

A GIS STUDY OF LANDSLIDES IN THE LOWER LOS AMIGOS FORELAND
OF PERU

By

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CHAPTER ONE

1.1 INTRODUCTION

Landslides involving rock, mud, and debris flow are dominant geomorphic processes in humid foreland environments worldwide. The environmental variables governing landslides, however, are not well known because most mass movement studies have been confined to areas influenced by human activities. By studying patterns of landslides in natural ecosystems, government officials, policy makers, engineers, geologists and others will become better informed about likely success of prevention or amelioration programs in risk-prone areas. My study area, the lower Los Amigos Basin in Peruvian Amazon, is an ideal place to study 'natural' landslide patterns and their causes.

Increased population and economic pressures have focused landslide research on those areas where landslides have the potential to affect human lives and infrastructure (Turner and Shuster, 1996). According to Cruden and Varnes (1996), various factors control landslides. These include geological, morphological, physical and human causes.

Geological causes include: material properties such as: weakness, sensitivity, degree of weathering, shear strength, jointing, bedding, schistosity, thrusts, faults, unconformities, contrast in permeability, and contrast in stiffness (Varnes, 1978). Morphological causes involve: tectonic or volcanic uplift, glacial rebound, fluvial, glacial or wave erosion of slope toe, erosion of lateral margin and deposition and vegetation removal. Similarly, physical causes involve: intense rainfall, rapid snow melt, prolonged exceptional precipitation, rapid drawdown, earthquake, volcanic eruptions, thawing, and shrink-and-

swell weathering. Although the human causes are negligible in this study area as there are no significant human activities, there are several human-induced landslides triggered all over the world. Human causes may be excavation of slope, loading of slope, drawdown or reservoirs, deforestation, irrigation, mining, artificial vibration, water leakage from utilities, etc.

According to Keller (2000) landslide causes can be grouped as external causes or internal causes. External causes include: loading of a slope by erosion or excavation, and earthquake shocks. Internal causes produce landslides without any recognized external changes and include such changes as increase in pore-water pressure or decrease in cohesion of the slope materials. Some causes of landslides are intermediate, having some attributes of both external and internal causes. For example, rapid groundwater draw-down involves an increase in the shear stress accompanied by decrease in shear strength caused by high pore water pressure.

The Andean Amazon foreland basin is prone to landslide activities. Indeed, the South American Andean Mountains have been subjected to a number of major landslide catastrophes. In 1962, Ancasa in Peru had a major landslide called Huscarac debris avalanche with a net volume of $13 \times 10^6 \text{m}^3$. It killed 4,000-5,000 people and much of Ranrahirca village was destroyed (Guadango and Zampelli, 2000). Although the triggering factor was unknown at the time, it is believed that the landslide was triggered by heavy rain. Similarly, in 1966 in Rio de Janeiro, Brazil a major landslide of avalanches debris and mud flows occurred. That too was triggered by heavy rainfall and

killed approximately 1000 people. The Nevados Huascara rock/debris avalanche in Peru, in 1970, was triggered by an earthquake of magnitude 7.7, killing 1,800 people and destroyed the town of Yungay (Guadango and Zampelli, 2000). These examples show that the tectonically active regions with high rainfall are prone to landslide activities. Several past and present landslides of San Francisco were also triggered either by heavy rain or by earthquakes resulting from tectonic activity (Griffiths, 2005).

Landslides range from simple rock/mud fall to complex slides and flows. According to Dikau et al. (1996) landslides are classified as fall, topple, slide, spread and flow. Fall and topple include detachment due to pre-existing discontinuities or tension failure surfaces. These landslides may be free fall, break up, bounce, slide or flow down slopes and may involve fluidization, liquefaction, cohesion less grain flow, heat generation or other secondary effects. Slide movement includes rotational or non-rotational and translational. In slides, the toe area may deform in a complex way. The ground can bulge, the slide may creep or even flow. Flow, bulge or slide can override existing failures. Failure might be retrogressive or progressive, and a graben often develops at the head of the landslide or it may include a toe failure. Spreads are lateral spreading of deformed ductile or soft material. Lateral spreading can develop sudden spreading failures in quick clays when the slope opens up in blocks and fissures followed by liquefaction. Sometimes, there might be a slow movement associated with denudational unloading. Flows are defined as debris movement by flow from unconfined and/or channeled failure surfaces. Flows involve a complex runout mechanism and these may be catastrophic in effect and may move in

sheets or lobes. The form of movement is a function of the rheological properties of the material (Dikau et al., 1996).

According to Varnes (1978), landslides can be classified according to type of movement and type of material (Table 1.1). Their diagrams are given in Fig. 1.1.

Table 1.1 : Types of landslides depending on type of movement and type of material (Varnes, 1978) as described by Roy and Hirotoka (2006)

TYPE OF MOVEMENT		TYPE OF MATERIAL		
		BEDROCK	ENGINEERING SOIL	
			Predominantly coarse	Predominantly fine
FALLS		Rock fall	Debris fall	Earth fall
TOPPLES		Rock topple	Debris topple	Earth topple
SLIDES	ROTATIONAL	Rock slide	Debris slide	Earth slide
	TRANSLATIONAL			
LATERAL SPREAD		Rock spread	Debris spread	Earth spread
FLOWS		Rock flow (deep creep)	Debris flow (Soil creep)	Earth flow
Complex		Combination of two or more principal types of movement		

The occurrence of different kinds of landslides depends on the causes behind them and the triggering factors. Brunsten (1993) explains how different factors trigger landslides. Physical, chemical and biological weathering cause changes in the physical and chemical properties in soil and rock. Triggering factors create changes in grading, cation exchange, and cementation. These changes cause formation of weak discontinuities and increased

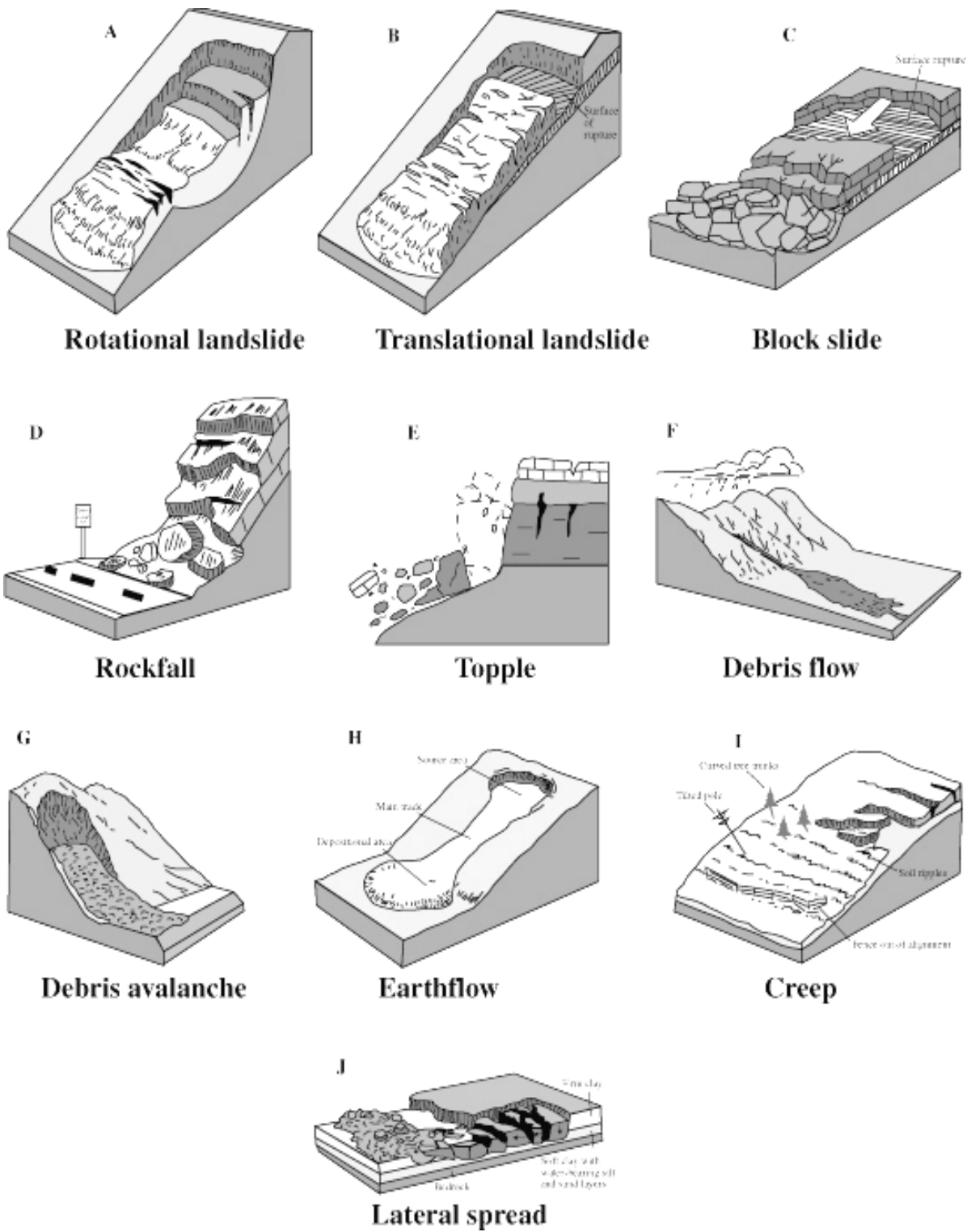


Fig. 1.1: Different types of landslides according to Varnes (1978).

depth of low strength materials. Eventually, there are changes in density, strength, permeability and pore water pressure in the soil and rock. Another type of weathering, which also changes the slope geometry, is associated with fluvial, glacial or coastal erosion. The changes in slope relief, slope height, length, angle and aspect results the changes in stress, strength and permeability along the slope and eventually triggers landslides.

Erosion and weathering can also undermine soils and rocks resulting in mechanical disintegration, solution, loss of cementing materials, leaching, and seepage. Undermining creates loss of support, consolidation of materials, changes in pore water pressure and loss of strength. Similarly, deposition of material by fluvial, glacial or mass movement processes creates long-term loading in drained areas and short-term loading in undrained areas, causing changes in relief, slope height, length, angle, and aspect of the terrain (Brunsden, 1993). Deposition of material eventually creates changes in permeability, strength and pore water pressure. Changes in water storage in groundwater can also trigger landslides. This change may cause rising or falling groundwater, development of perched water tables, surface saturation and flooding. The typical changes in this case could be floods, lake bursts, 'wet' years, intense precipitation, snow and ice melts and rapid drawdown. These changes in water storage also eventually create excess pore water pressure, changes in bulk densities and reduction in effective shear strength (Brunsden, 1993). Human interference causes similar changes in terrain.

The observation of air photos of the study area from different years shows that the majority of landslides in my study area are earth flows, and a few are rotational slides.

This observation is also supported by literature and historical landslide records. According to Chorley *et al.*, (1984) humid tropical rainforest areas undergo maximum chemical weathering, episodic mass wasting, moderate slope wash and erosion/sedimentation related fluvial processes and these areas have high dissolved and suspended loads in rivers. Morphologically, these areas contain low gradient rivers, wide, flat floodplains, and steep slopes arising abruptly from valleys, stabilized by vegetation and knife edge ridges. To identify the causes for landslide occurrences, different casual factors and triggering factors must be studied. According to Sower and Royster (1978), data for six parameters are necessary for any detailed landslide investigation: topography, geology, hydrology (groundwater and surface water), history of slope changes, weather, and vibration. Topographic data includes contour maps, surface drainage, slope profiles and data on topographic changes. Geological data includes lithology at the site, geological structure, and nature and depth of weathering. Hydrologic data include piezometric levels, variations in piezometric level, groundwater chemistry, nature and extent of surface water, seepage and data on water withdrawal. Data on history of slope changes means any information on slope changes due to natural processes (long term geological changes, erosion, and past movements), rate of movement, correlation of movement with other factors such as surface and groundwater, weather, and human activity. Weather data include precipitation, temperature and barometric changes. Similarly vibration data are seismic data, and any human induced vibration data such as blasting and heavy machinery. Site-specific landslide model which incorporates geology,

geomorphology, anthropology and the range of external process is also useful (Sower and Royster, 1978).

Collecting, storing, analyzing, and manipulating the above-mentioned data are important tasks in any landslide study. Development of GIS and spatial statistical techniques are recent technological developments in earth sciences. These tools are constantly being used to improve investigation techniques and mitigative measures for the landslides in populated regions. There is improvement of quantitative methods to assess the probability of future landslide occurrences (Clerici, 2002). Most GIS-based landslide studies are, so far, most effectively used in landslide susceptibility studies and landslide hazard/risk mapping. However, some research also focus on the future prediction of landslide and landslide distribution in natural terrain. Brenning (2005) used spatial statistics to develop a spatial prediction model for landslide hazards. Guthrie and Evans (2004), after analyzing landslide frequencies and characteristics in British Columbia, Canada, concluded that GIS landslide studies must focus on landslides in natural ecosystems.

Dai (2001) used GIS techniques to study and map landslide susceptibility on the natural terrain. Burton *et al.*, (1998) used spatial statistics to generate a landslide model, and later they field checked the model. Lan *et. al.*, (2004) analyzed the dynamic characteristics of landslides in response to rainfall and concluded that the water pressure distribution and slope stability can be used as landslide predictor in GIS. Some studies even compare the different methods. Suzen and Doyuran (2004) compare the GIS based landslide susceptibility assessment methods by using multivariate and bivariate approaches. My thesis also uses hydrologic modeling to observe the soil-water interactions to model

landslides. Hydrologic modeling is the quantification of hydrological processes using rainfall, soil, topography, and vegetation. In other words, hydrologic modeling solves many complex hydrological relationships/equations.

A terrain becomes unstable only when the shear stress exceeds the shear strength along some surface that becomes the failure surface. The methods used in this study are based on this principle of failure. In general, it is common for slope failures to occur during wet weather, because shear stress increases with increased weight of wetter slope materials (Fitts, 2002).

According to Mohr-Coulomb failure Criterion, for any slope:

$$\tau_f = c + \sigma_e \tan \phi . \quad (1.1)$$

Where, τ_f = shear strength (i.e, shear stress at failure),

c = Cohesion of material,

ϕ = Internal friction angle,

σ_e = Effective stress.

We have the relationship (Fitts, 2002):

$$\sigma_e = \sigma_t - P. \quad (1.2)$$

Where,

σ_t = Total stress and,

P = Pore water pressure.

So, Mohr-Coulomb failure Criterion becomes:

$$\tau_f = c + (\sigma_t - P) \tan \phi . \quad (1.3)$$

Equation (1.3) shows the stresses at failure depends on cohesion of soil (c), friction angle (Φ) and most importantly, total stress (σ_t) and pore water pressure (P).

The pore water pressure in soil and effective stress can be related to soil water content and pressure head. In other words, we can use a hydrologic model to determine these parameters by providing, rainfall data, evaporation data and soil properties data.

The hydrologic model used to observe the changes in water content and pressure head for high and low rainfall periods along with rainfall rate and evaporation rate in test sites. These observations were then used to explain the effective stress and the pore water pressure of the unsaturated soil in the area.

According to Fitts (2002), for a fixed weight at the bottom of soil column ($\sigma_t = \text{constant}$) thus:

$$d\sigma_e = -dP. \quad (1.4)$$

Where, $d\sigma_e$ = increase in effective stress and,

$-dP$ = decrease in pore water pressure.

For the unsaturated flow, according to Bishop and Blight (1963):

$$d\sigma_e = -\rho g \kappa dH. \quad (1.5)$$

Where, κ = a constant, depends on the degree of saturation, soil structure, and the wetting – drying history of the soil,

ρ = density of water,

H = pressure head.

For the unsaturated soil, $H > 0$, $\kappa = 1$,

$$H < 0, \kappa \leq 1,$$

$$H \ll 0, \kappa = 0.$$

Hence, pore water pressure, water content and effective stress must be analyzed carefully in order to understand the failure mechanism in any landslide prone region. The hydrologic modeling was used to observe the changes in soil-water pressure head (H) with time.

The term ‘landslides’ in my study refers to any soil/rock failures that can be mapped at the 1:100,000 scale from air photos. Identifying, mapping and analyzing different classes of landslides depicted in fig.1, on a pure GIS basis is not possible; thus, every time I refer to the term ‘landslide’, I mean one of possible: cut bank erosion, side cutting by rivers, debris flow, translational and rotational slides, mappable rill/gully erosions, mud slides/flows, rock/soil fall/topple, slumps and creeps (if mappable). I did not classify landslides according to type.

My thesis has 4 chapters and two appendices. The appendix includes all initial data, processed data and outputs. In Chapter 1, I introduce the occurrences, classification, and causes of landslides. I declare my objectives. In Chapter 2, I describe my materials and methods. Chapter 3 presents results and discussion, and I present a conceptual model of the landslide process for my study area. I conclude my research project in Chapter 4.

1.2 OBJECTIVES

My thesis has three objectives.

- 1) Check the distribution (*i.e.*, randomness) of landslides digitized in ArcGIS for spatial trends.

The randomness will show whether the distributions of landslides are just random or whether they are occurring due to a spatially correlated geomorphological process (*e.g.*, river meander). Such distribution can be described either qualitatively or quantitatively. Quantitative techniques are accurate, reliable, and scientifically sound.

- 2) Determine the relationships between environmental variables, and the occurrence of landslides.

Since environmental variables such as water pressure in soils contributes to landslides, the degree of their dependency with landslide occurrence can be determined.

- 3) Develop a conceptual model for channel cross-section to show influence of landslides on fluvial and foreland processes.

CHAPTER TWO

MATERIALS AND METHODS

2.1 Study area

Peru is located on the South American continent and is well known for its highly variable geography. Because of variation in relief, rain shadows, El Nino, Humboldt Current, and wind patterns, the country comprises a multitude of climates (Escobal and Torero, 2000). My study area (Fig 2.1) lies in the south-eastern part of the country, in the foothill of the Andes, in the Amazon basin. The study area is a small portion of the much larger Madre de Dios basin. The Madre de Dios basin contains 3 sub-basins, and has a total drainage area of 47,254 km². The Los Amigos sub-basin is one of the three sub-basins in the Madre de Dios foreland watershed. The lower Los Amigos sub-basin with a 1,634 km² study area, is located between 12⁰ -12.5⁰ latitude and 70⁰ – 71⁰ longitude. The area is characterized by heavy rainfall, dense vegetation, meandering streams, and homogeneous soil types. Many swamps and oxbow lakes are common due to the sinuosity of the river. Many small and large landslides, predominantly mud flows, debris flows and mud slides are common. Sandy and silty loamy soils are the major soil types; bamboo commonly grows on exposed soils.

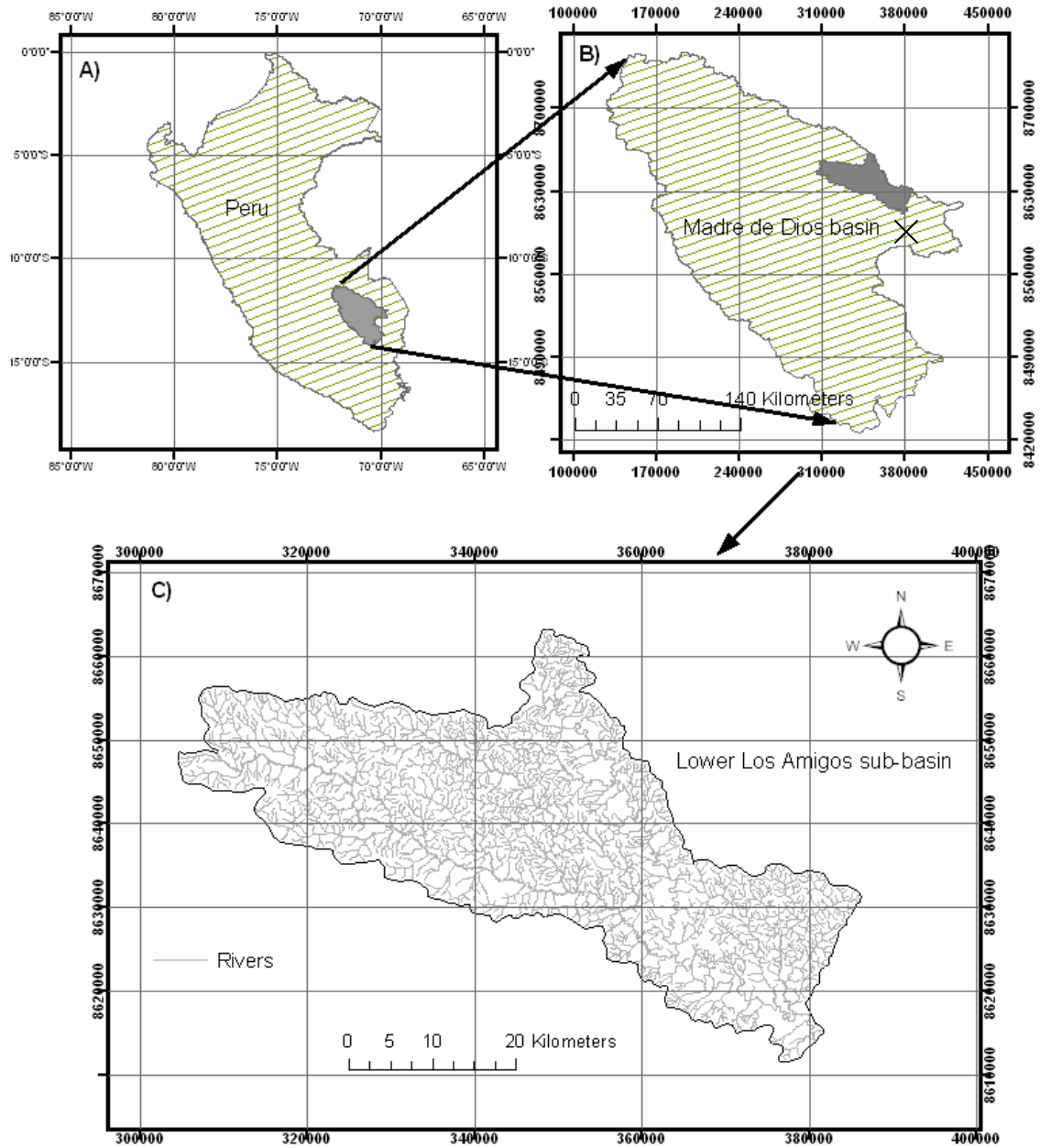


Fig. 2.1: A) Map showing Peru and Madre de Dios basin, B) Study area within Madre de Dios basin, C) My Study area. The coordinate system for map A is Lat Long and the coordinate system for other two maps B and C is Universal Transverse Mercator (UTM). The X, marks the approximate location of the Los Amigos Biological Station.

2.2 Geological and geo-morphological setting:

The Nazca Plate is moving east to north-east and is subsiding beneath the South American Plate (Jaillard *et al.*, 2000). Various studies have been conducted on the subduction of the Nazca plate and foreland basin evolution. Meschede and Barckhausen (1998), paleogeographically reconstructed the oceanic crust formed by the Cocos- Nazca spreading center and its precursors. Spreading performed in steps of 0.5 million years. During subduction, very large lithospheric plates subside beneath the crust producing a strong seismic wave. These waves travel to the surface and in many case are detected as strong earthquake and may serve as external cause of landslides

A foreland basin starts in the foothills of a mountain, and is relatively flat. It is defined as an elongate region of potential sediment accommodation that forms on continental crust between a contractional orogenic belt and the adjacent craton (Brazilian Craton for the Amazon), mainly in response to the geodynamics processes related to subduction and the resulting peripheral thrust belt (DeCelles and Giles, 1996). The Andean foreland basin in Peru receives a huge amount of water and loose sediments from the mountains, making the basin more prone to erosion.

This foreland basin is also a part of great Amazonian basin. The Amazonian basin is the world's largest Cenozoic (Neogene) fluvial sedimentary basin. The study area is still deforming due to active orogenic movement which has been affecting the fluvial depositional environments in the Amazonian foreland basin throughout the Neogene-

Quaternary time (23 to 1.8 million years ago) (Rasanen *et al.*, 1991). The continuous deformation is affecting sediment transportation, deposition, and water storage. That storage sometimes explodes in the form of voluminous floods and these floods may be responsible for many landslides.

Fig. 2.2 shows the paleogeographical reconstruction of the Nazca plate subducting beneath the South American plate.

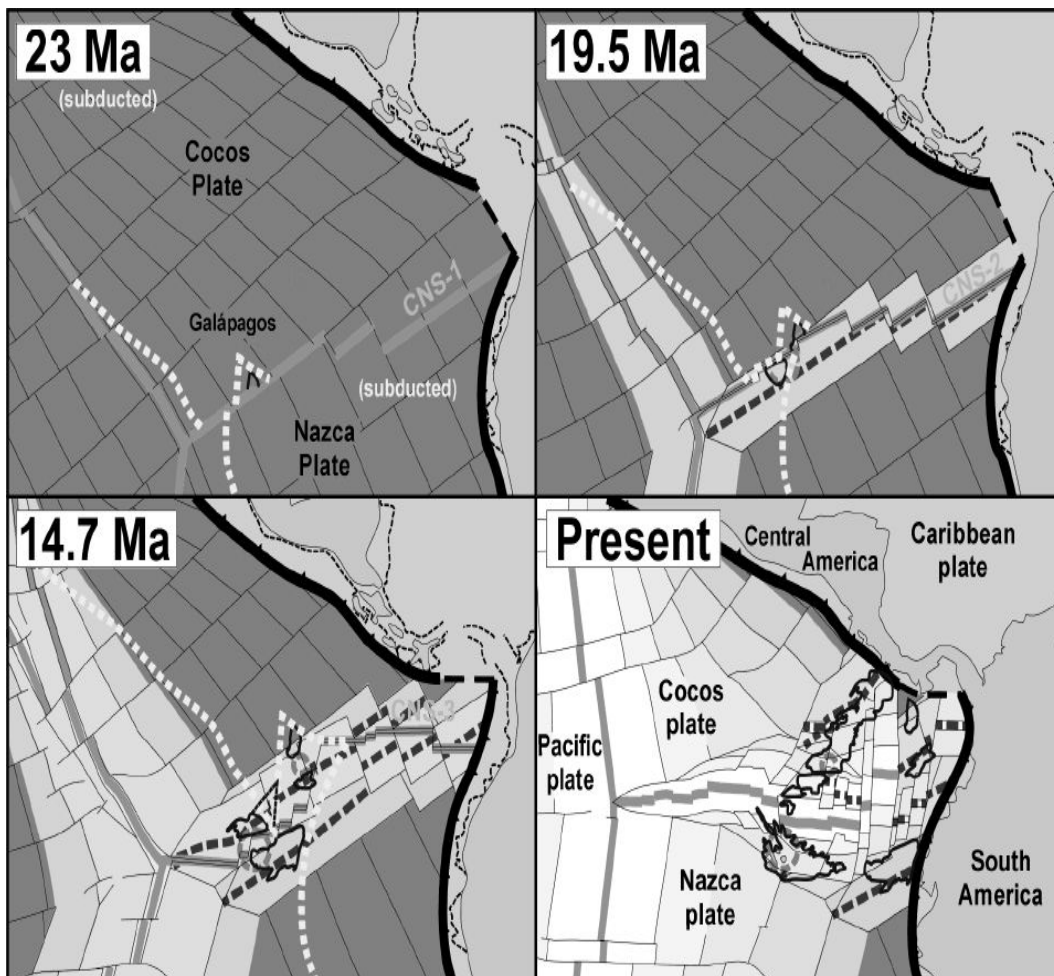


Fig. 2.2: Plates and plate boundaries. This figure shows Subduction of Nazca oceanic plate into the South American plate. This paleogeographical reconstruction was done by Meschede and Barckhausen (1998).

2.3 Rainfall:

Rainforests obviously receive more rainfall than any other part of a continent. Observing the monthly rainfall for seven years (from 1998 to 2004) by NASA's TRMM (TRMM, 2005), the recorded highest monthly accumulated rainfall was around 700mm.

December-January is a generally high rainfall period and June-July is a low rainfall period. TRMM data were first obtained in ASCII (American Standard Code for Information Interchange) format from NASA's (National Aeronautics and Space Administration) TRMM website for each month of this seven year period. Data tabulation, average calculation and plotting were done by using EXCEL[®] (Microsoft Corporation) spreadsheet application. Fig. 2.3 shows average monthly rainfall plot for seven years. Detail data for each month are presented in appendix.

For hydrologic modeling, I used the 30 minute rainfall data for 2004 and 2005 from the Los Amigos Biological Station provided by John Janovec, Botanical Research Institute of Texas, Fort Worth. Detailed use of rainfall data is given in section 2.7.2.

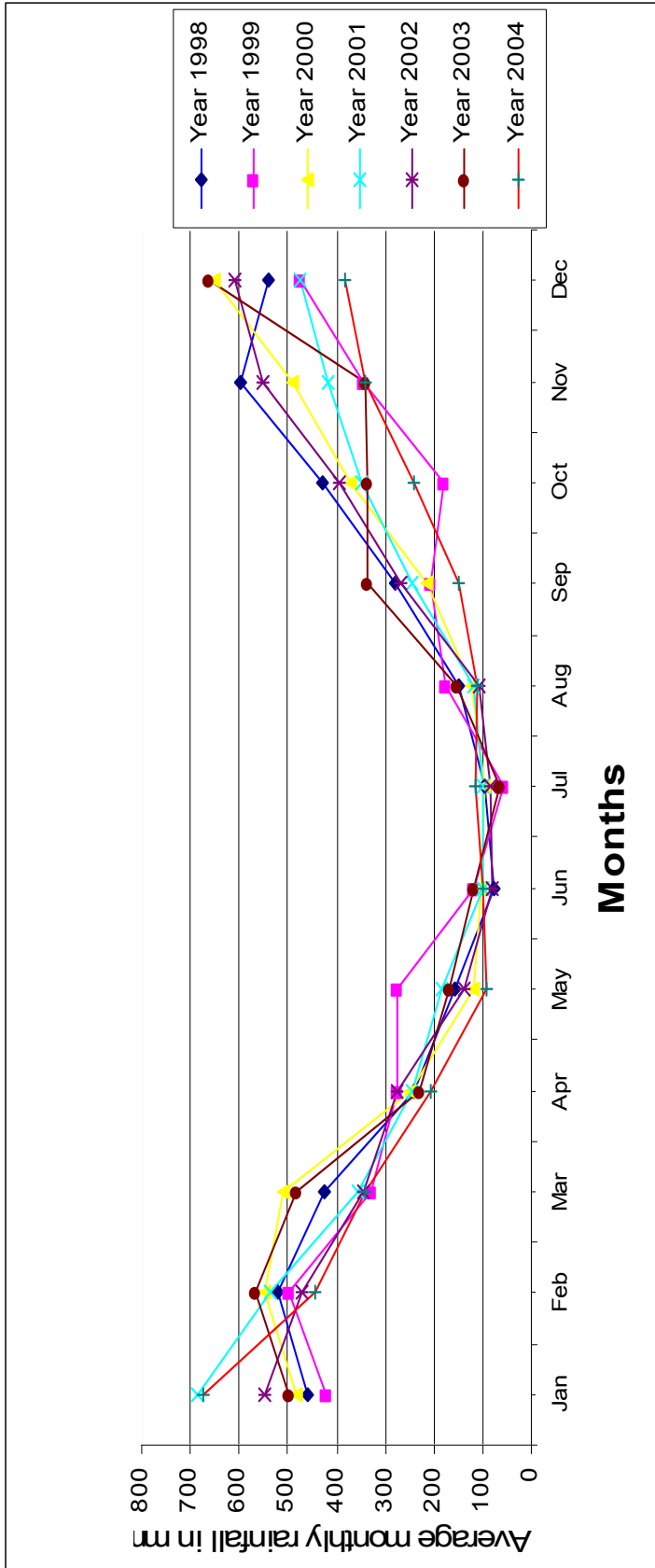
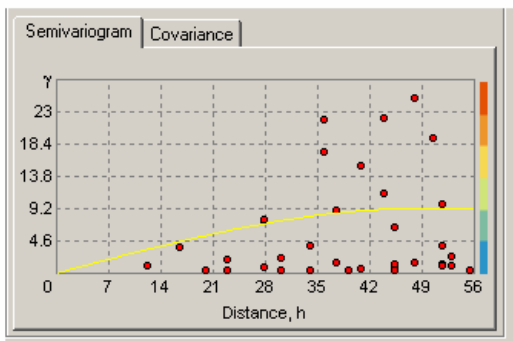
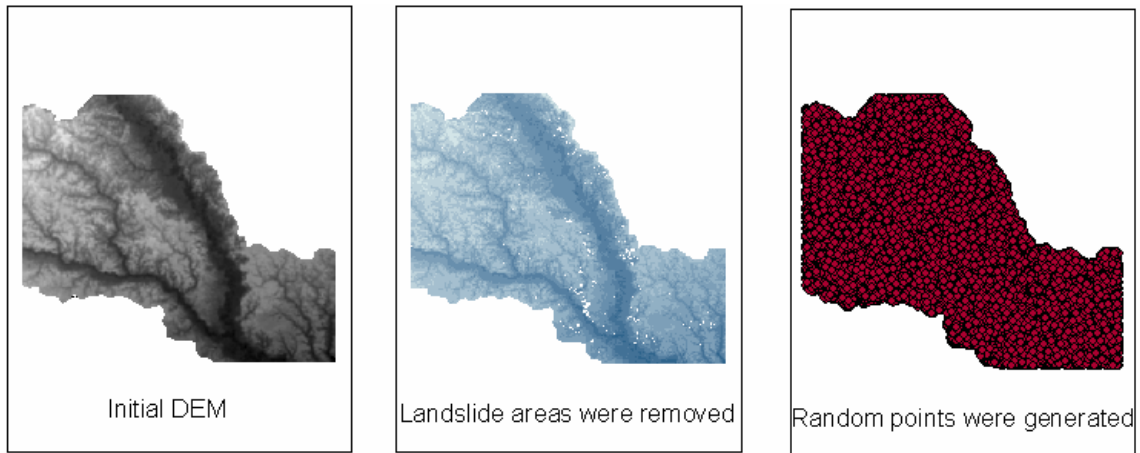


Fig. 2.3: Average monthly rainfall in mm. This plot was created by using NASA's TRMM rainfall data. January 2001 has highest rainfall recorded in these seven years period. Each year December and January receives high rainfall while June and July are relatively dry months.

2.4 Hydrology

2.4.1 Elevation and Slope

Compared to the entire Madre de Dios basin, the terrain in the lower Los Amigos sub-basin is relatively flat. The highest elevation is 422m above mean sea level and the lowest elevation is 226m above mean sea level. ASTER (Advanced Spaceborne Thermal Emission and Reflection Radiometer) DEM (Digital Elevation Model) of 30m resolution was collected and extracted for the study area. However the ASTER DEM did not cover the whole area. SRTM (Shuttle Radar Thematic Mapper) DEM with 80m resolution was used to extract the elevation for the remaining areas (SRTM, 2006). The areas with landslides were masked out from both DEMs and the random points were generated. Randomly sampled elevation points for the Los Amigos were then extracted using Hawth's analysis tool for ESRI (Environmental System Research Industries, Redlands, California) ArcGIS® 9.1. Then those points were interpolated by kriging operation using Geostatistical Analyst extension of ArcGIS® 9.1. The maps used to krig a DEM are given in fig. 2.4.1a.. Since there is little elevation variation (Fig. 2.4.1b), the slopes were relatively low (Fig. 2.4.1c): the maximum slope was 16° . The slope was calculated using spatial analyst extension of ArcGIS® 9.1.



A Semi-variogram was fitted to the elevation points

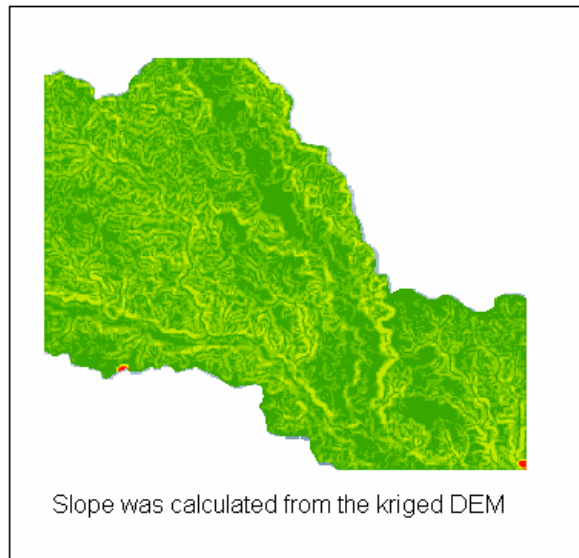
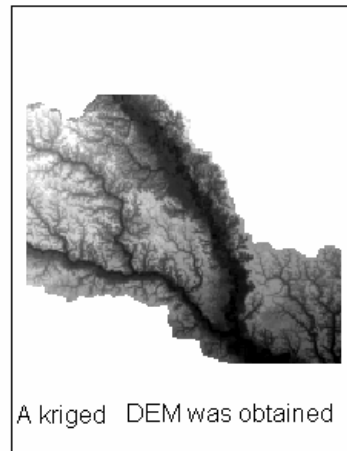


Fig.2.4.1a: re-kriging of DEM to get the slopes around landslides. Elevation generation started off from the top left corner.

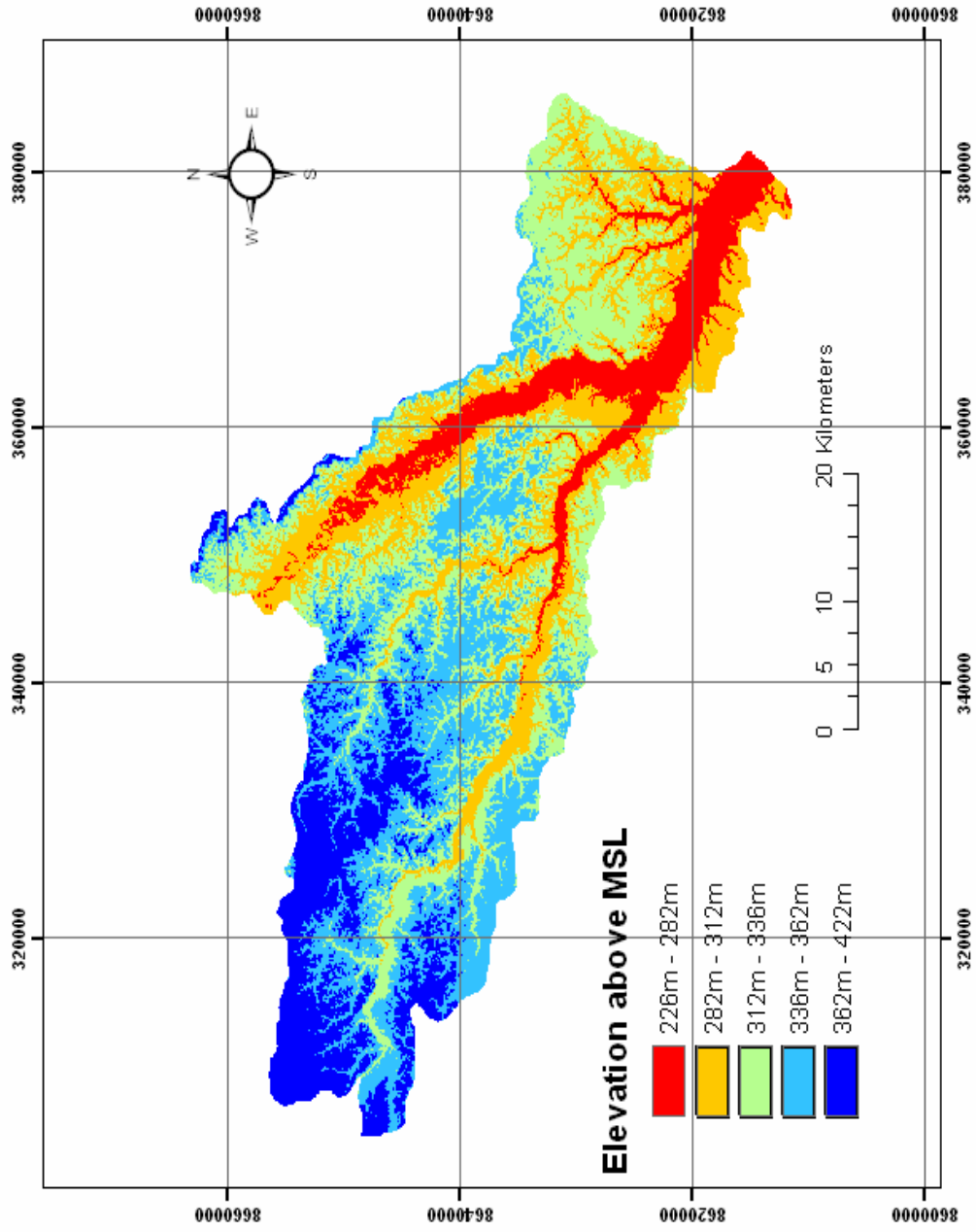


Fig. 2.4.1b.: The elevation map for the Lower Los Amigos sub-basin. The highest elevation is 422m and the lowest elevation is 226m above MSL. The coordinate system is in UTM.

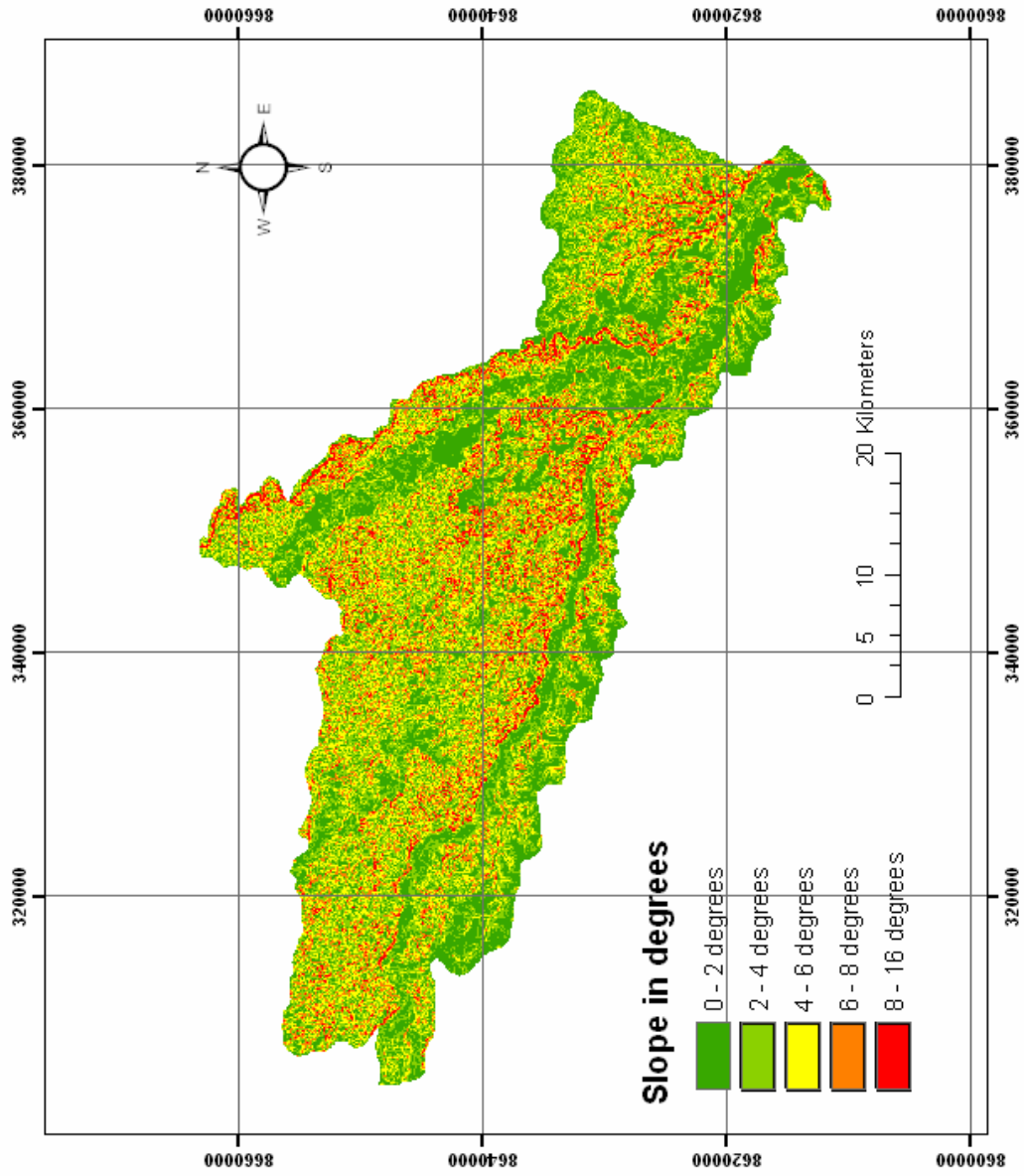


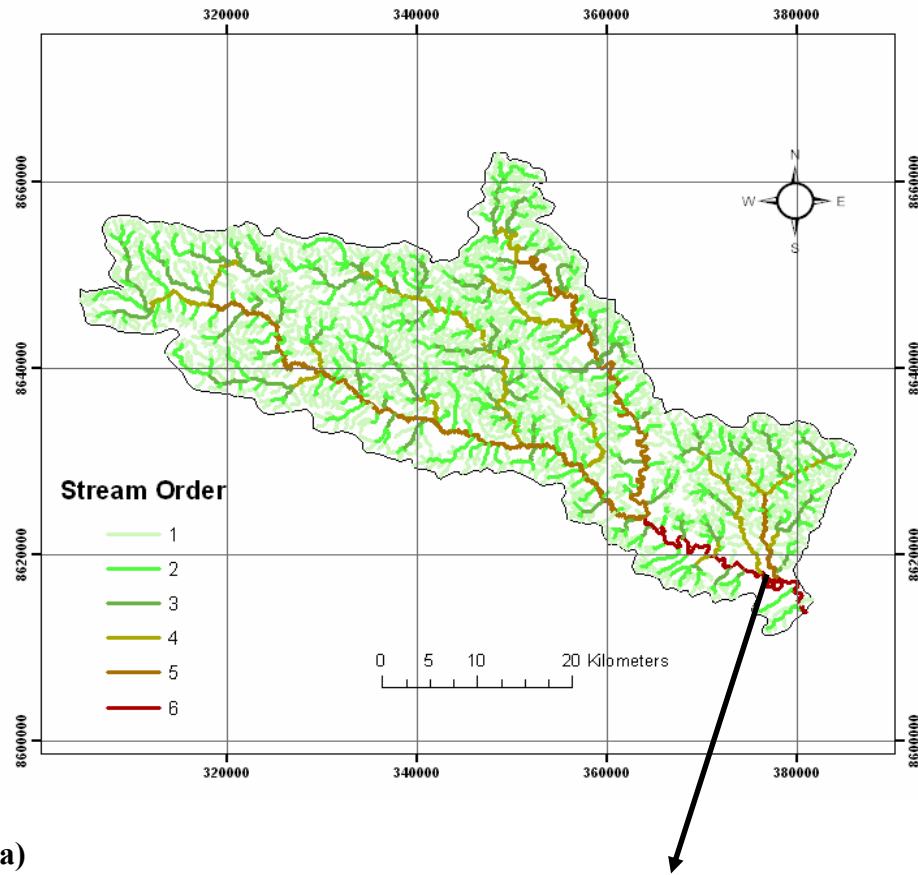
Fig. 2.4.1c.: Slope distribution in the study area. The coordinate system is UTM.

2.4.2 Drainage

The drainage pattern in the study area is mostly dendritic. Dendritic drainage patterns are recognized by their branching tree-like structure. Drainage delineation took three major steps:

- 1) Slicing of DEM: DEM for entire region did not show distinct drainage because of the greater variation in elevation values so the DEM was sliced into 14 smaller sections to make the drainage visible for digitizing.
- 2) River digitizing in 'From node' to 'To node' direction: When all visible DEM sections were loaded into Arc GIS 9.1, the digitization was carried out down river direction.
- 3) Network geometry and stream ordering: Network geometry was maintained and streams were ordered according to Strahler (1952) by using the RivEx extension for ArcGIS[®] (Duncan's RivEx Extension for ArcGIS, <http://www.rivex.co.uk>, accessed on December, 2005). River ordering helped identify the major streams. The study area contains six stream orders (Fig. 2.4.2 (a)).

The main stream in the sub-basin is Los Amigos River. Los Amigos meets Madre de Dios River a few kilometers south-east from the south-eastern boundary of the study area. The highly meandering rivers continuously change their paths over time. Fig. 2.4.2 (b) shows an example meander that I commonly observed.



a)

b)

Fig. 2.4.2: Drainage map. a) Drainage map with river order. b) A meandering river has changed its path. The coordinate system for the stream order map is UTM.

2.4.3 Watershed

The watershed was delineated using the drainage map. To draw the precise and accurate watershed, a hillshade was created from the DEM. Hillshade along with drainage network helped to identify the ridge and watershed divide. Hillshade and river network were overlaid in ArcGIS® 9.1, and the watershed shown in Fig. 2.4.3 was digitized. Since the study area is a part of the larger Madre de Dios basin, the first 7 digits of its label came from the watershed label for Madre de Dios basin. The label has 9 digits. First digit '3' means that this area is the third sub basin of the Madre de Dios basin. The Following 3 digits represent the number of upstream sub watersheds. Among the remaining 5 digits, the first three represent the watershed number for the larger Madre de Dios basin and the last 2 digits are watershed number for the study area. the watershed boundary was used to delineate my area.

2.5 Soils

A soil map obtained from government of Peru through BRIT (Botanical Research Institute of Texas) contained taxonomically classified soil polygons. I reclassified the soils by soil texture using the USDA (United States Department of Agriculture) textural soil classification triangle. To do that: I extracted the percent of silt, clay and sand from the taxonomically classified soil, and then I re-classified the soil texturally using the USDA triangle. The majority of soils were silty clay loam, sand, and silt loam. Silt loam is confined along the main river banks (Fig. 2.5).

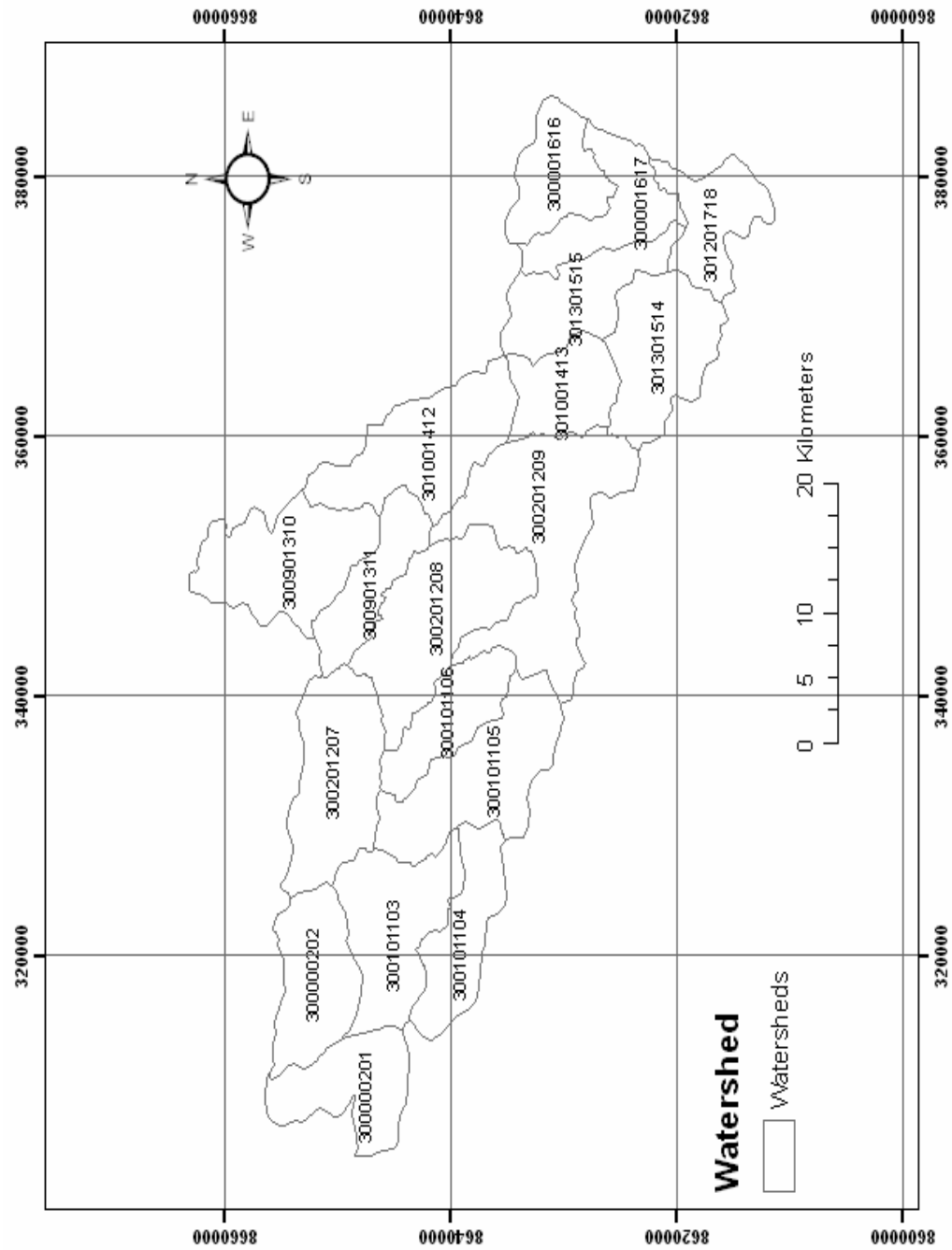


Fig. 2.4.3: Watershed map of the study area. Since this is a part of Madre de Dios basin, the first digit in this watershed corresponds to sub-basin no 3 of Madre de Dios basin. The coordinate system is in UTM.

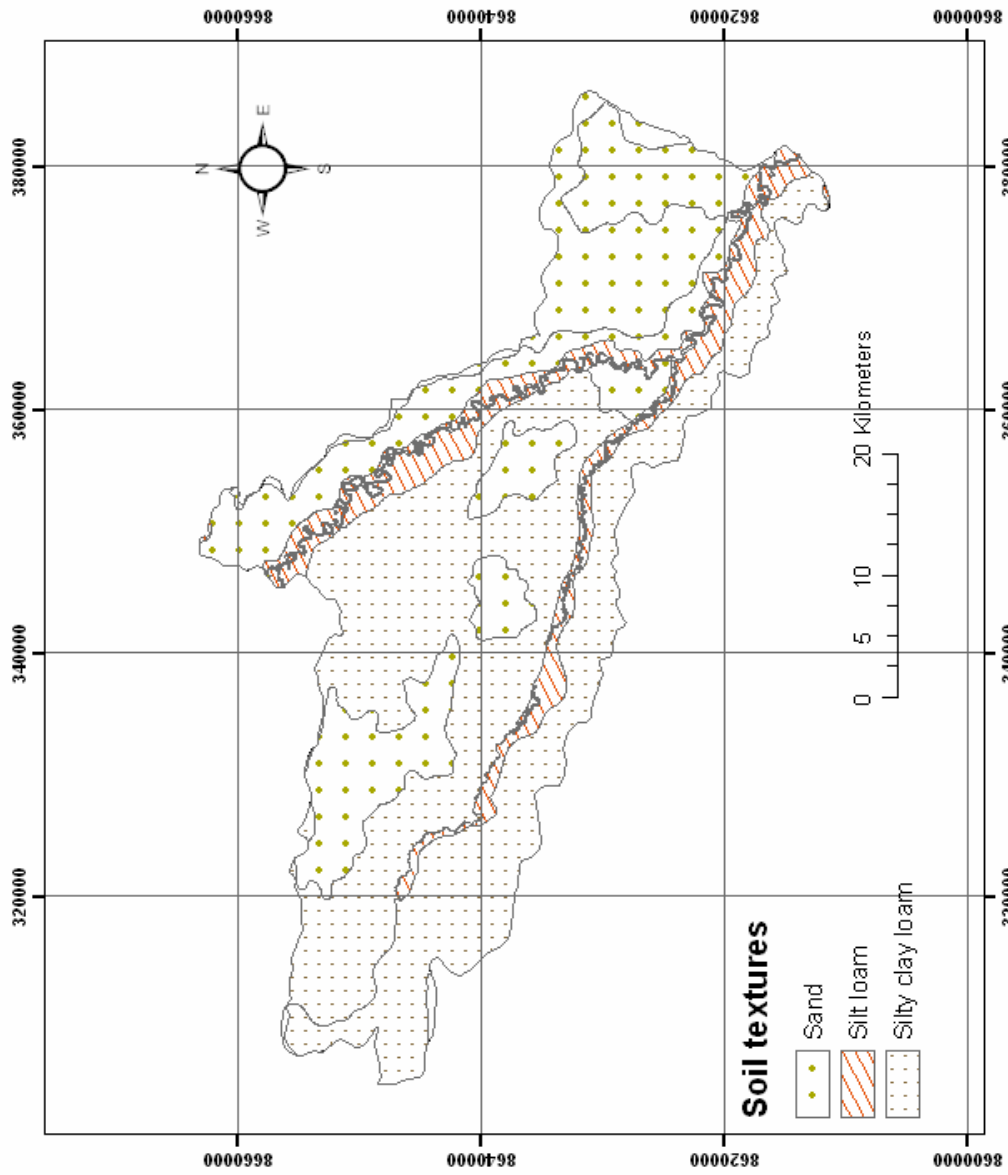


Fig 2.5: Soil distribution in study area. The classification scheme shown in this map is based on soil texture i.e., classification based on percentage of sand, silt and clay. The coordinate system is in UTM.

2.6 Landslides

Lower Los Amigos basin has hundreds of landslides confined mainly on either side of the Los Amigos river(Fig.2.6.1). Almost all the landslides are located on the sandy soil and silty loam soils. Recent landslides were identified from 5cm resolution air photos taken by Winrock International in 2003. Air photos were loaded into ArcGIS[®] 9.1, and landslides were digitized. A total of 381 landslides with a mean area of 2,4081 m² weere digitized. The total area of landslides was 8.7 km². The largest landslide identified had an area of 400,000 m². Fig. 2.6.1 - Fig 2.6.8, show example landslides photographed by Ethan Householder, a TCU Environmental Science graduate student working in Los Amigos. The purpose in presenting these photographs is to show some common types of failures and mass movements.

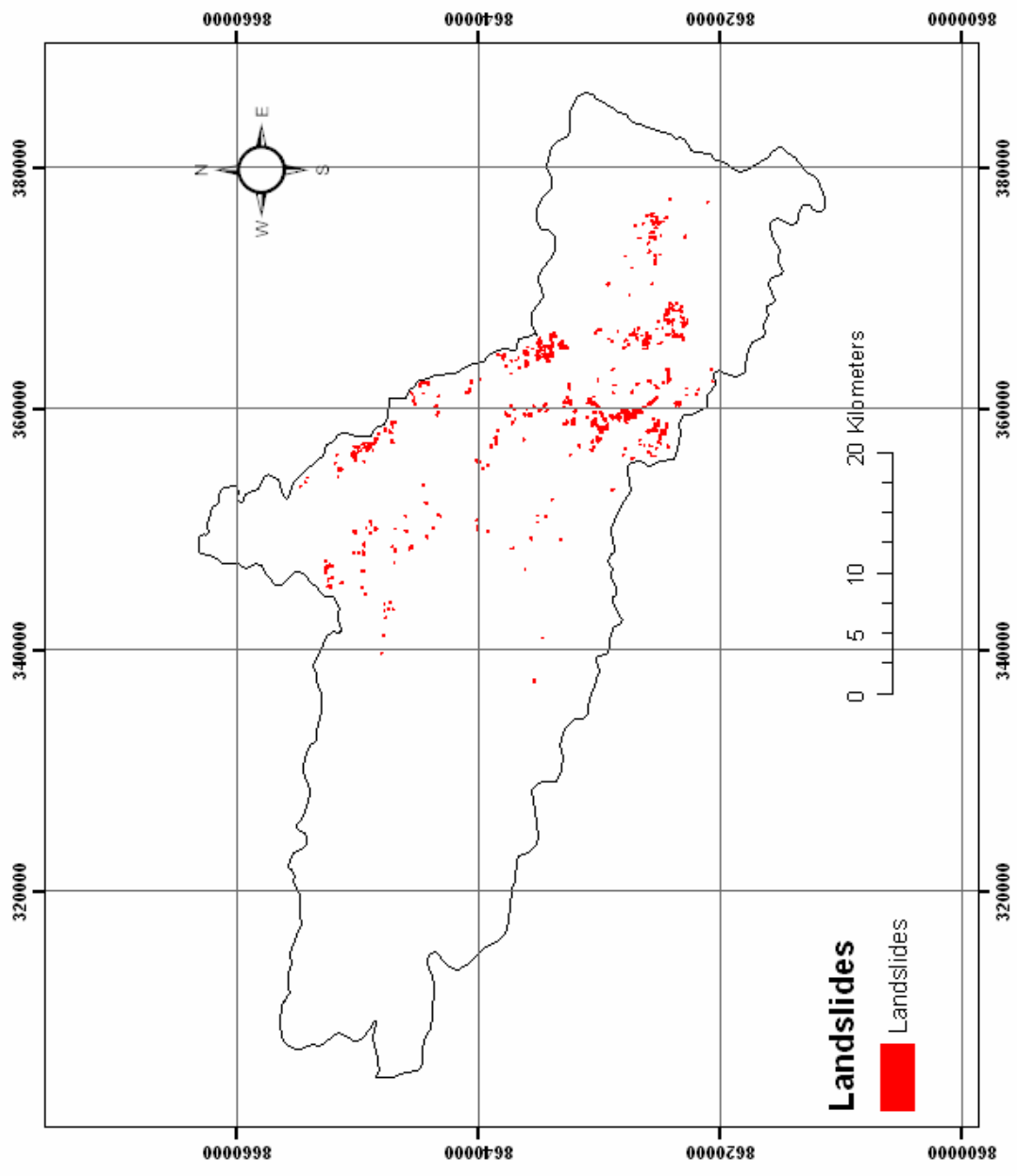


Fig. 2.6.1: Landslide distribution in the study area. Red patches are landslides. The coordinate system is in UTM.



Fig 2.6.2: Erosion at a river bank. Many river banks in the study area are unstable. Note the shallow rooting depth. The breaks (shown in white line) running along the soil profile suggest historical soil deposition. The breaks may be attenuated by wet/dry cycling of soils.



Fig 2.6.3: Another failure along the river bank. The debris deposit and landslide slopes are rapidly covered by pioneer species, bamboo.



Fig. 2.6.4: Loose sandy soils are easily eroded away by intermittent rivers and overland flow after the rainfall.



Fig. 2.6.5: Silty soils showing water erosion in exposed areas.



Fig. 2.6.6: Bamboo is a Pioneer species that rapidly colonizes landslides.



Fig. 2.6.7: A landslide: Typical example of water induced failure. Ethan is standing right on the channel.



Fig. 2.6.8: Riverside failure. This is a small translational slide. Note the second order failure from the upper scarp. The lower scarp (B) is the older one with dark colored organic lining on the surface. The upper scarp (A) is fresh.

2.7 Hydrologic modeling

The pore water pressure can internally cause soil failure. I determined pore water pressure for my study area from soil-water pressure. Soil-water pressures were obtained from hydrologic model called MIKE-SHE (DHI Inc., Denmark). MIKE-SHE is an advanced integrated hydrological modeling system. It simulates water flow in the entire land based phase of the hydrological cycle from rainfall to river flow, via various flow processes such as, overland flow, infiltration into soils, evapotranspiration from vegetation, and groundwater flow (MIKE-SHE, 2006).

2.7.1 Model essentials

To observe and explain the changes in pressure head and soil water content, hydrologic modeling was carried out. The model was run for two different months: September, 2004 and March 2005; defining ‘dry’ and ‘wet’ periods, respectively. Observing results from both periods helped me observe and explain the difference in soil water interaction in these two different time periods. The hydrologic model was MIKE-SHE (DHI Inc, Denmark). The whole modeling process involved three main steps (Fig.2.7.1).

- Input
- Running model and,
- Output

The input data for the modeling consisted of rainfall, evaporation, soil water retention parameters, hydraulic conductivity, elevation and groundwater table. Input details are

presented in the next section (2.7.2). To run the MIKE-SHE model, MIKE-ZERO framework was used. While MIKE-SHE is a dynamic modeling system for integrated groundwater and surface resources, MIKE-ZERO is a framework that gives access to MIKE-SHE modeling system. MIKE-ZERO gave many important facilities (data editing, charting, preprocessing, running and analysis tool) for me to model the hydrology. The simulation was run at three hourly time steps. The output from the model was obtained in gridded data format. Outputs include water content in unsaturated zone, pressure head in unsaturated zone, rainfall rate in unsaturated zone and actual evaporation rate in unsaturated zone.

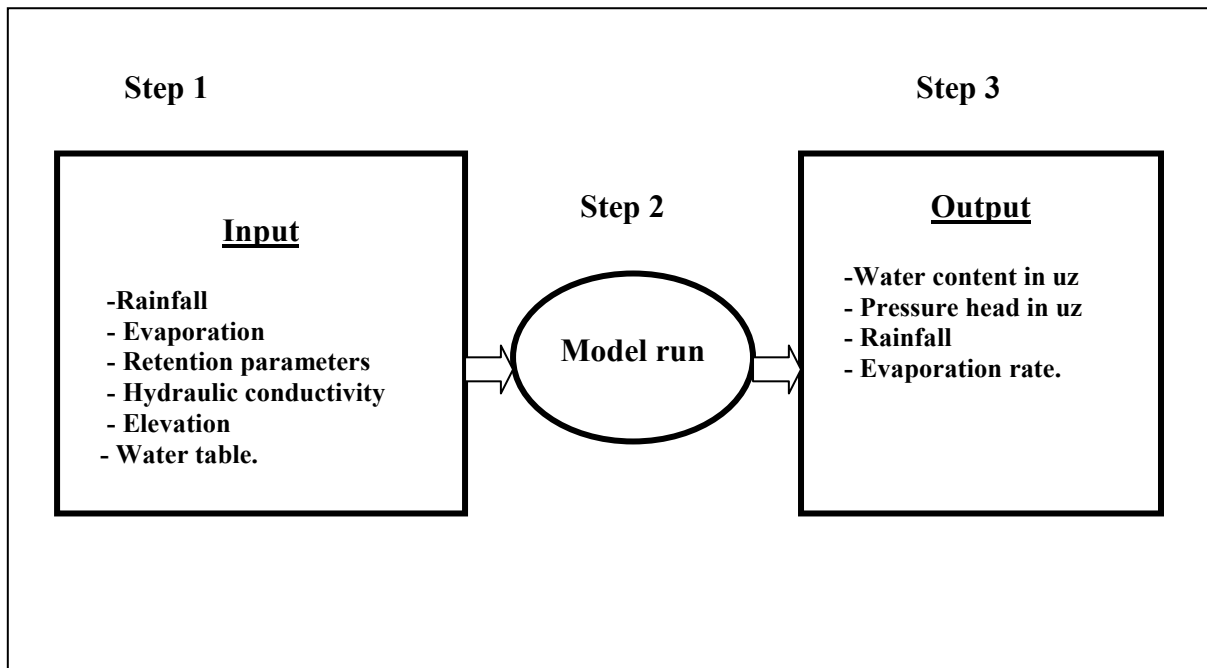


Fig. 2.7.1: General flow chart of the modeling showing different steps involved to run the model (uz refers to unsaturated zone).

2.7.2 Model Input

As stated in section 2.7.1, six input parameters were collected and used. None of the initial GIS data were in a format required by MIKE-SHE. A series of calculations and data manipulations were done before loading the data into MIKE-SHE environment. The calculation of rainfall was simple, while the calculation of evaporation, soil water retention parameters and hydraulic conductivities were more involved.

2.7.2.1 Calculation of rainfall and evaporation

Measured 30- minute weather data provided by John Janovec from BRIT (Botanical Research Institute of Texas), were used to generate evapotranspiration and rainfall data for MIKE-SHE. The initial data consisted of 30 minute measurement of rainfall, solar radiation, relative humidity, temperature and wind speed. The 30 minute measurement data were converted into three-hourly measurements using Microsoft Excel because the modeling time step was 3 hours. The flow chart in fig. 2.7.2 illustrates the steps used for the calculation of rainfall and evaporation.

The procedure for calculation of evaporation from the Penman-Monteith equation is shown in fig. 2.7.2 (Shuttleworth, 1993). The required parameters were net radiation, latent heat, wind speed, and temperature gradient. They were calculated at 3 hourly time steps. The psychrometric constant was assumed to be constant at $0.067 \text{ kPa } ^\circ\text{C}^{-1}$ at an average temperature of 25°C .

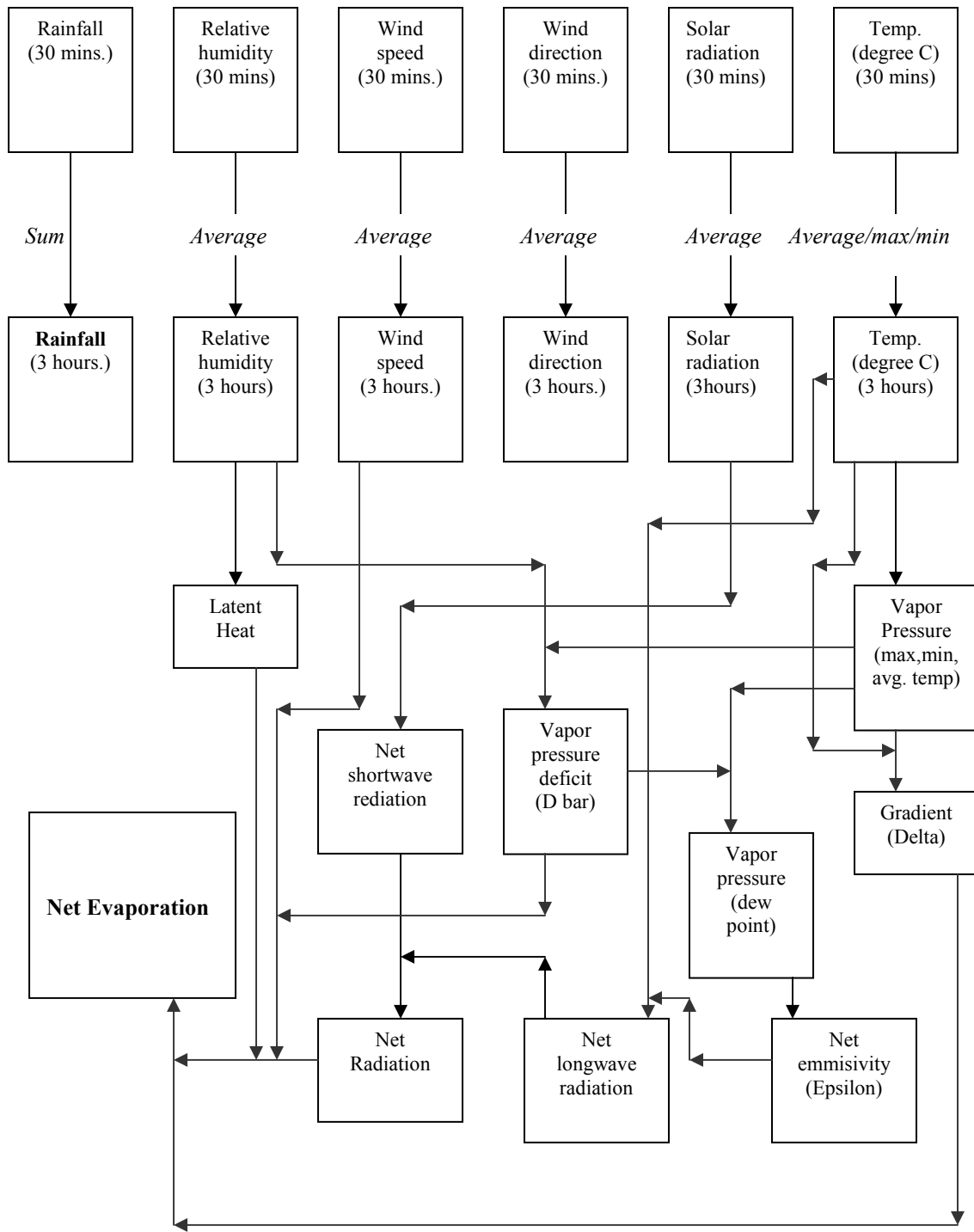


Fig. 2.7.2: Flow chart showing calculation of rainfall and evaporation. Starting from the top of the figure, the arrowheads start from the data and point towards the calculated results. Follow the arrowheads to get the parameters required to calculate the specific terms. The final result of all these calculations is rainfall and net evaporation shown in bold letters.

I used the Penman-Monteith equation (Shuttleworth, 1993)

$$E_p = \frac{\nabla}{\nabla + \gamma} (R_n + A_h) + \frac{\gamma}{\Delta + \gamma} \frac{6.43(1 + 0.536U_2)\bar{D}}{\lambda} \quad (2.7.1)$$

Where,

E_p = Potential evaporation/ net evaporation, mm day⁻¹,

R_n = net radiation exchange for the free water surface, mm day⁻¹,

A_h = energy advected to the water body, mm day⁻¹, if significant,

U_2 = wind speed measured at 2m, ms⁻¹, \bar{D} = vapor pressure deficit,

γ = psychrometric constant, kPa⁰C⁻¹, λ = latent heat, MJkg⁻¹,

∇ = gradient defined by temperature.

As mentioned earlier, γ was assumed to be constant. Also, A_h was ignored. R_n was obtained by the sum of net shortwave radiation and net longwave radiation (Fig. 2.7.1).

Net shortwave radiation was obtained from solar radiation data and net longwave radiation was obtained from net emissivity and temperature (Shuttleworth, 1993). Net emissivity was calculated from vapor pressure and vapor pressure was actually obtained from temperature data. Similarly, \bar{D} was also calculated from vapor pressure and saturated vapor pressure. The evaporation calculations were performed in Microsoft Excel. The 3 hourly evaporation data were then loaded as a .dfs0 file into MIKE-SHE.

2.7.2.2 Calculation of soil water retention and hydraulic conductivity

Rawls *et al.*, (1993) suggested three types of soil water retention and hydraulic conductivity relationships for the modeling: Brooks and Corey relationship, Campbell relationship and Van Genuchten relationship. MIKE-SHE supports only two of them: Brooks and Corey and Van genuchten relationships. I used Van Genuchten methods because, in my case, I found this method provided better retention curves.

Van Genuchten relationship for soil water retention is given by (Rawls *et al.*, 1993):

$$\frac{\theta - \theta_r}{\phi - \theta_r} = \left[\frac{1}{1 + (\alpha h)^n} \right]^m \quad (2.7.2)$$

Where, ϕ = porosity,

θ = water content,

θ_r = residual water,

α = constant given by $\alpha = (h_b)^{-1}$, where h_b = bubbling capillary pressure, kPa,

n = constant given by $n = \lambda + 1$, where λ = pore size index,

m = constant given by $m = \frac{\lambda}{\lambda + 1}$.

Similarly, Van Genuchten relationship for hydraulic conductivity is given by (Rawls *et al.*, 1993):

$$\frac{K(\theta)}{K_s} = \left(\frac{\theta - \theta_r}{\phi - \theta_r} \right)^{\frac{1}{2}} \left\{ 1 - \left(\left[\frac{\theta - \theta_r}{\phi - \theta_r} \right]^{\frac{1}{m}} \right)^m \right\}^2 \quad (2.7.3)$$

Where, $K(\theta)$ = hydraulic conductivity for given water content, cm h^{-1} ,

K_s = fully saturated conductivity, cm h^{-1} when $\theta = \phi$.

As noted in section 2.5 of this chapter, the soil data was initially taxonomically classified. There were four major soil types: Entisols, Inceptisols, Alfisols and Ultisols. Since the data did not contain any information on soil water retention and hydraulic conductivity parameters, these soils were reclassified texturally in terms of sand, silt and clay percentages based on Nordt (2000), Wayne (2000), Hallmark (2000), and West (2000). Three textural soils were identified: sand, silt loam and silty clay loam. Once the soils were classified texturally, the water retention properties were determined from Rawls *et al.* (1982, 1993). The soil water retention and hydraulic conductivity parameters for three soils are presented in following table (Table 2.7.1).

Table 2.7.1 Soil parameters required by the unsaturated soil component of MIKE-SHE.

	<i>Silty loam</i>	<i>Silty clay loam</i>	<i>Sand</i>
Silt%	65.8	7	6
Sand%	20.4	65	87
Clay%	13.8	28	7
Porosity (ϕ)	0.50	0.471	0.52
Moisture at -33kPa	0.33	0.366	0.14
Moisture at -1.5MPa	0.133	0.208	0.01
K_s (cm/h)	1	0.05	20
Pore-Size index, λ	0.234	0.177	0.694
α	0.048169557	0.030712531	0.137741047
θ_r	0.015	0.04	0.02
h_b , cm	20.76	32.56	7.26
K_s , mm/h	0.1	0.005	2.0

2.7.3 Model Runs

After data input, the specifications required to run the model in MIKE-SHE were determined. The simulation was specified as unsaturated zone flow (UZ) dependent on rainfall and evapotranspiration. The unsaturated flow simulation was performed using the full Richard's equation (Ross, 1990). The simulation period was one month: one month each for wet (March, 2005) and dry (September 2004) periods. The time step was 3-hourly, and the grid specified was 1km X 1km. The topography was obtained from the contour shape file. The spatial distribution of precipitation was assumed to be uniform because the 30 minute rainfall data was available at the Los Amigos Biological Station. Similarly, the spatial distribution of vegetation was assumed to be uniform with a Leaf Area Index (LAI) value of 5 to represent the dense canopies. The rooting depth (RD) was specified as 1.5 m (assuming shallow tree rooting depth).

The spatial distribution of evapotranspiration was also assumed to be uniform for two reasons: 1). the entire study area has dense vegetation cover and, 2). no vegetation classification was available. The spatial distribution of soil profiles was specified as spatially non-uniform (spatially-distributed) by providing polygon data with the X and Y axes in UTM meter coordinates.

The groundwater table depth was specified as spatially-distributed, and a water table map was provided with water table depth ranging from zero meters to 15 meters from the ground surface (Fig.2.7.3): the groundwater table data for the study area could not be

obtained because no piezometric instruments were installed in the study area. Thus, the groundwater table was assumed at zero meter depth to the ground at the mouth of the Los Amigos River and up to 15 meter depth from the ground surface along the first order streams in river source areas and it was also assumed that the groundwater table follows the topography. The groundwater table elevation map was obtained using the Raster Calculator of Spatial Analyst extension in ArcGIS® 9.1. The water table elevation raster map created in ArcGIS® 9.1 was not recognized by MIKE-SHE , so a contour map was created from this water table elevation map in ArcGIS® 9.1 and imported into MIKE-SHE. The actual water table elevation map was then produced in MIKE-SHE using water table contour map. This contour map was interpolated into a grid inside MIKE-SHE by bilinear interpolation.

2.7.3 Model Output:

Detailed time series output were obtained from the model. The time series outputs that I selected were pressure head in unsaturated zone, soil water content in unsaturated zone, rainfall rate, and actual soil evaporation. These outputs were obtained in MIKE-SHE in the form of gridded data which were later exported into ASCII formats to plot the data in Microsoft Excel.

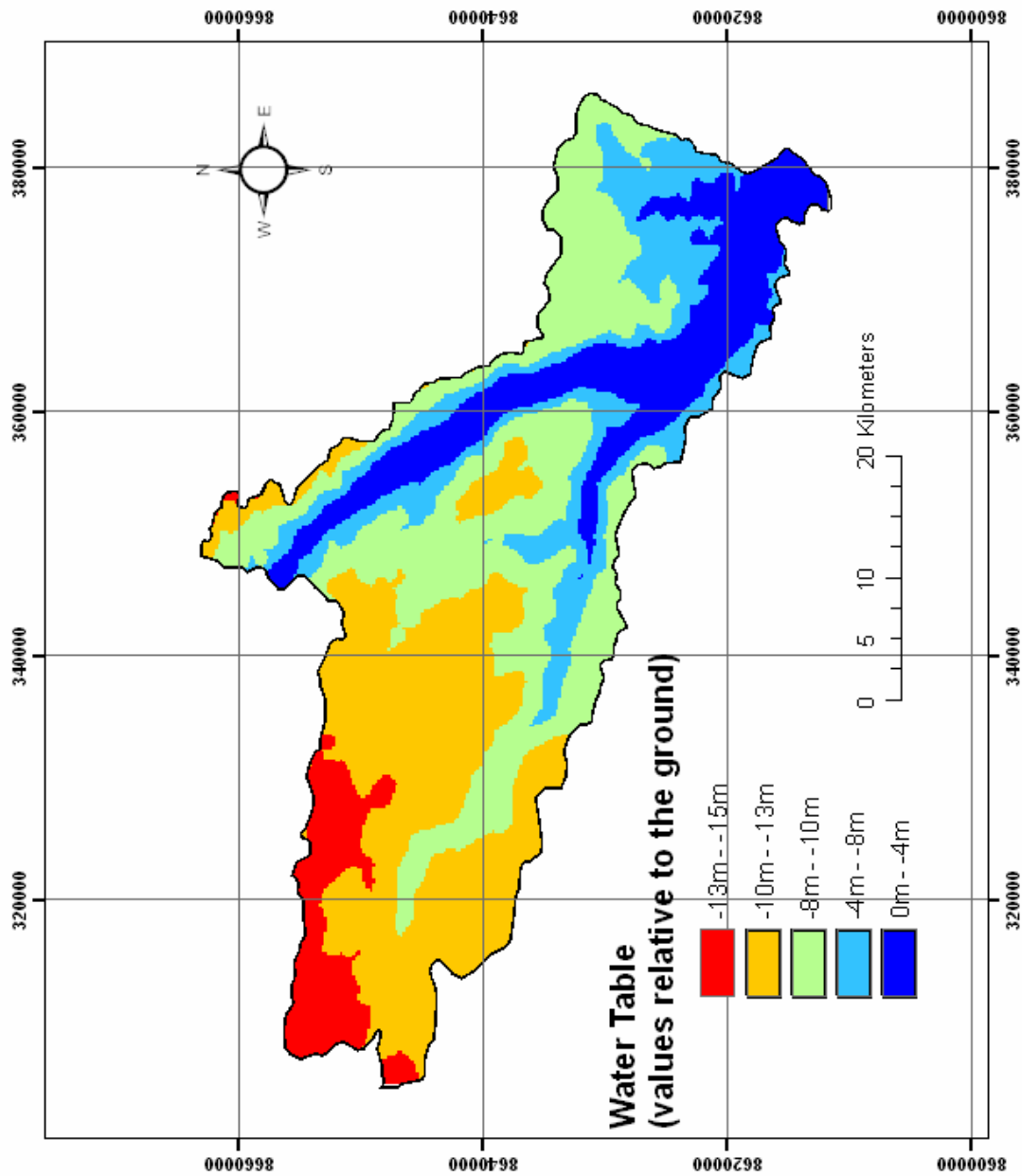


Fig. 2.7.3: Groundwater table map of the study area. The coordinate system is in UTM.

2.8 Randomness

Randomness explains the spatial trends of events. An event may be a single phenomena, object, occurrence or existence at any spatial location (Landslides occurrences are events in my study). Events are regular, clustered or random. From among several statistical methods, I used Ripley's K-function to check the randomness of landslide distribution (Ripley, 1976; Ripley, 1979; Bailey and Guttrel, 1995; Ripley, 1977). K-function is a tool for analyzing spatial point process data *i.e.*, it analyzes the spatial event points for spatial trends (Dixon, 2002). Ripley's K-function provides a test of randomness between specified area limits (Levine, 2004). Randomness is tested by comparing Ripley's K-function with Complete Spatial Randomness (CSR) where CSR represents a baseline hypothesis against which the observed patterns are compared to see whether observed patterns are regular, clustered or random (Bailey and Gatrell, 1995).

2.8.1 K-function

The theory description given by Levine (2004) is simplified and presented here.

Let us consider a spatially random distribution of N points. Suppose, the circles of radius d_s , are drawn around each points, where s represents the order of radii from the smallest radius to the largest radius. Then the number of points within the circle is counted and then summed over all points. Now, the expected numbers of points within that radius are:

$$E(\text{number of points within distance } d_i) = \frac{N}{A} K(d_s). \quad (2.8.1)$$

Where, N= sample size,

A= Total study area,

$K(d_s)$ = area of circle defined by radius d_s .

In the case of CSR, the expected number of points within distance d_s is given by:

$$E(\text{number of points under CSR}) = \frac{N}{A} \pi d_s^2. \quad (2.8.2)$$

Now, if the average number of points found within a circle of a particular radius over each point is greater than $\frac{N}{A} \pi d_s^2$ (i.e., number of points under CSR), then the points are clustered. On the other hand, if the average number of points found within a circle of a particular radius over each point is less than number of points under CSR, the points are dispersed or random.

In general, K-statistics indicates the non-randomness by counting the number of total event points within a particular radius and comparing it to the number expected on the basis of CSR. Based on this assumption, K-statistics is defined as:

$$K(d_s) = \frac{A}{N^2} \sum_i \sum_{i \neq j} I(d_{ij}). \quad (2.8.3)$$

Where,

$I(d_{ij})$ = Number of other points, j, found within distance d_s , summed over all points, i.

After completing this process, the radius of the circle is increased and the entire process is repeated. In my study, 100 intervals were used by using:

$$d_s = \frac{R}{100} . \quad (2.8.4)$$

Where, R= radius of a circle whose area is equal to the study area,

d_s = radius distance.

Since, $K(d_s)$ is non linear, it is transformed into a square root function $L(d_s)$ to make it linear. The square root function is defined by

$$L(d_s) = \sqrt{\frac{K(d_s)}{\pi}} - d_s . \quad (2.8.5)$$

In practice, L statistics are plotted, even though the name of the statistic K is based on the K derivation given by equation (2.8.3).

The software I used was Crimestat[®] III (Ned Levine & Associates, Houston, TX, and the National Institute of Justice, Washington, DC). I used 1000 simulations for CSR, and I specified the circular edge correction. Edge correction was necessary because the K-function is biased near edges.

2.9 Spatial heterogeneity

To test whether landslides had spatial dependencies, I used spatial regression.

Environmental variables such as slope classes, aspect, closeness to the river, soil properties, and vegetation play a role in the occurrences of landslides. Spatial regression helped with the final and the most important objective of this thesis: determining the main causes for landslides in tropical rain forests.

2.9.1 Spatial Regression

The spatial regression analysis involved a series of significance tests for regression coefficients. This was necessary to identify and confirm the spatial dependencies, and significance between landslides and environmental variables. The following paragraphs explain 2 main steps I carried out in spatial regression.

2.9.1.1. Standard linear regression or Ordinary Least Squares model (OLS)

This model finds a linear relationship between a dependent variable and a set of explanatory variables:

$$y = X\beta + \varepsilon . \tag{2.9.1}$$

Where, β = regression coefficient (intercept),

X= Explanatory variable,

y= Dependent variable and,

ε = Error term.

Equation (2.9.1) is for the linear relationship when, dependent variable is y and single explanatory variable is X.

The OLS estimation is called Best Linear Unbiased Estimator (BLUE) because OLS minimizes error variances. It estimates β by minimizing the sum of squared prediction errors so the term least squares is used. In order to obtain the BLUE property, certain assumptions about the random error of the regression equations are made:

- i) The random error has a mean of zero
- ii) The random errors are uncorrelated and they have a constant variance. Having constant variance in random errors is called homoscedastic. A test called heteroscedasticity checks for the variable variance in errors.
- iii) The random errors follow a normal distribution.

2.9.1.2 Spatial dependency

If the assumptions made for BLUE are true, then there won't be any spatial dependence, but in practice this is not always true. If a value observed in one location depends on the values observed at neighboring locations, then there is spatial dependence.

2.9.1.2.1. Spatial error

In spatial error, the error terms across different spatial units are correlated i.e., the error term ε_i from spatial unit y_i and ε_j from spatial unit y_j for example, are correlated. The spatial error coefficient λ is observed for the significance in spatial error model.

2.9.1.2.2 Spatial lag

In spatial lag, the dependent variable in one place is affected by the independent variables both in that place and another place. In the spatial lag model, the lag coefficient ρ will show presence of spatial dependence.

All regression analysis was carried out using GeoDa[®] (Spatial Analysis Laboratory, Department of Geography, University of Illinois). The selection of a dependent variable for landslides was a major challenge. I digitized the outline of landslides as polygons using 5cm air photos (Fig. 2.6.1 from section 2.6). In order to quantify landslides as a dependent variable, I counted the number of individual landslides within a 1km X 1 km grid (Fig. 2.9.1). The landslides were counted within 1km X 1km grid because the hydrologic modeling was also run at 1km X 1km grids (Section 2.7.3), and any output obtained from hydrologic modeling would be applicable for 1km X 1km grid. I counted the number of landslides within each grid using Hawth's analysis tool 3.24 for ArcGIS[®] 9.1. Then each 1km X 1km grid containing landslides was assigned the number of landslides (Fig. 2.9.2).

I extracted the slope and aspect for each grid from the slope map and aspect map, respectively. At this stage, I had two independent variables which might be responsible for the landslides in the area. Another drainage dependent variable (Pressure head fluctuation) was obtained from MIKE-SHE for each landslide grid. The standard deviation in pressure head at each grid was extracted from MIKE-SHE in ASCII format to get another independent variable, H_{σ} . The distance from the nearest river for the each grid was determined from Hwath's analysis tool for ArcGIS® 9.1. In this way, I used landslide count as a dependent variable and slope, aspect, distance from river, and standard deviation in pressure head (H_{σ}) as explanatory independent variables.

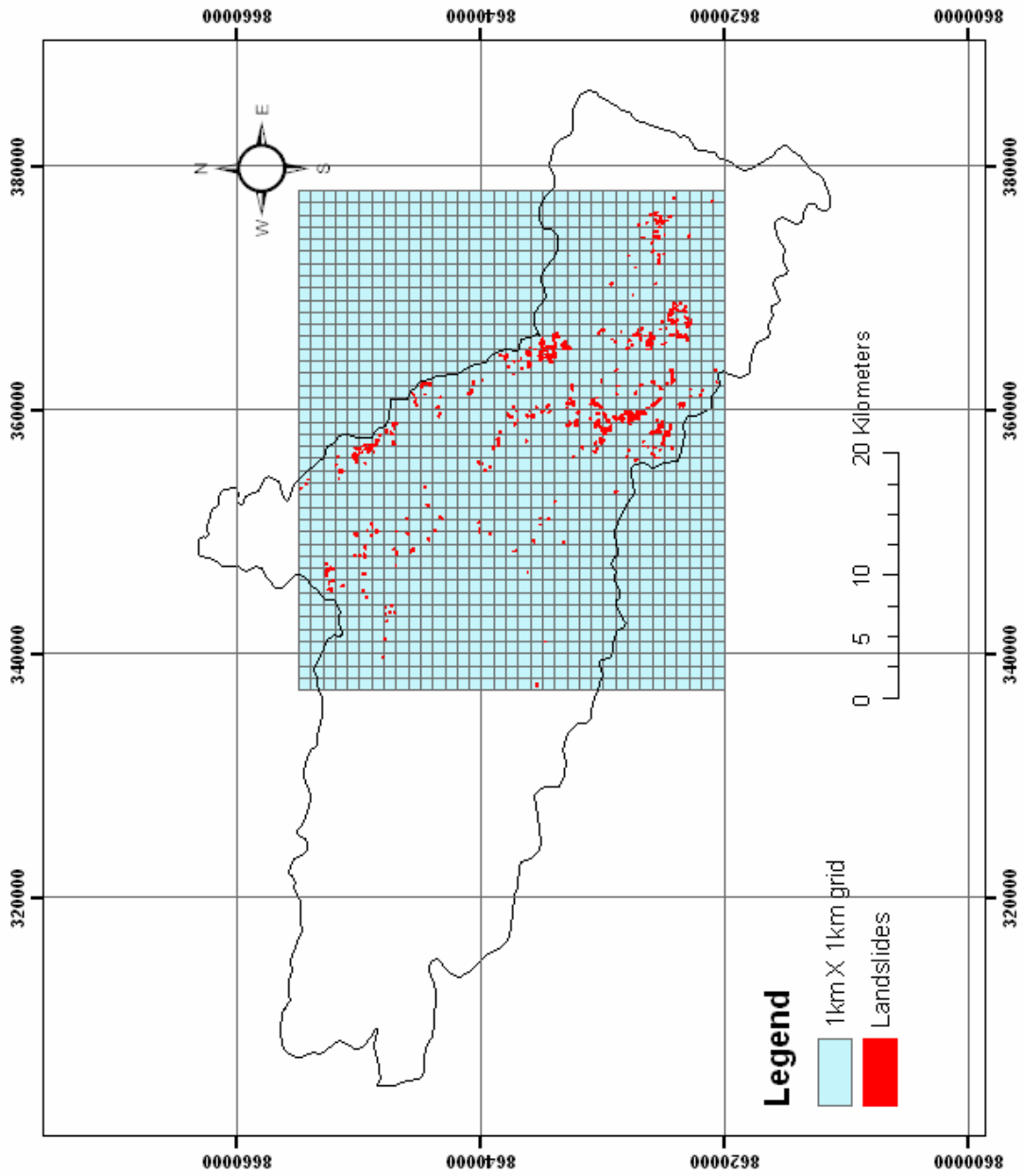


Fig. 2.9.1: 1km by 1km grid was created and overlaid on the landslide distribution. The coordinate system is UTM.

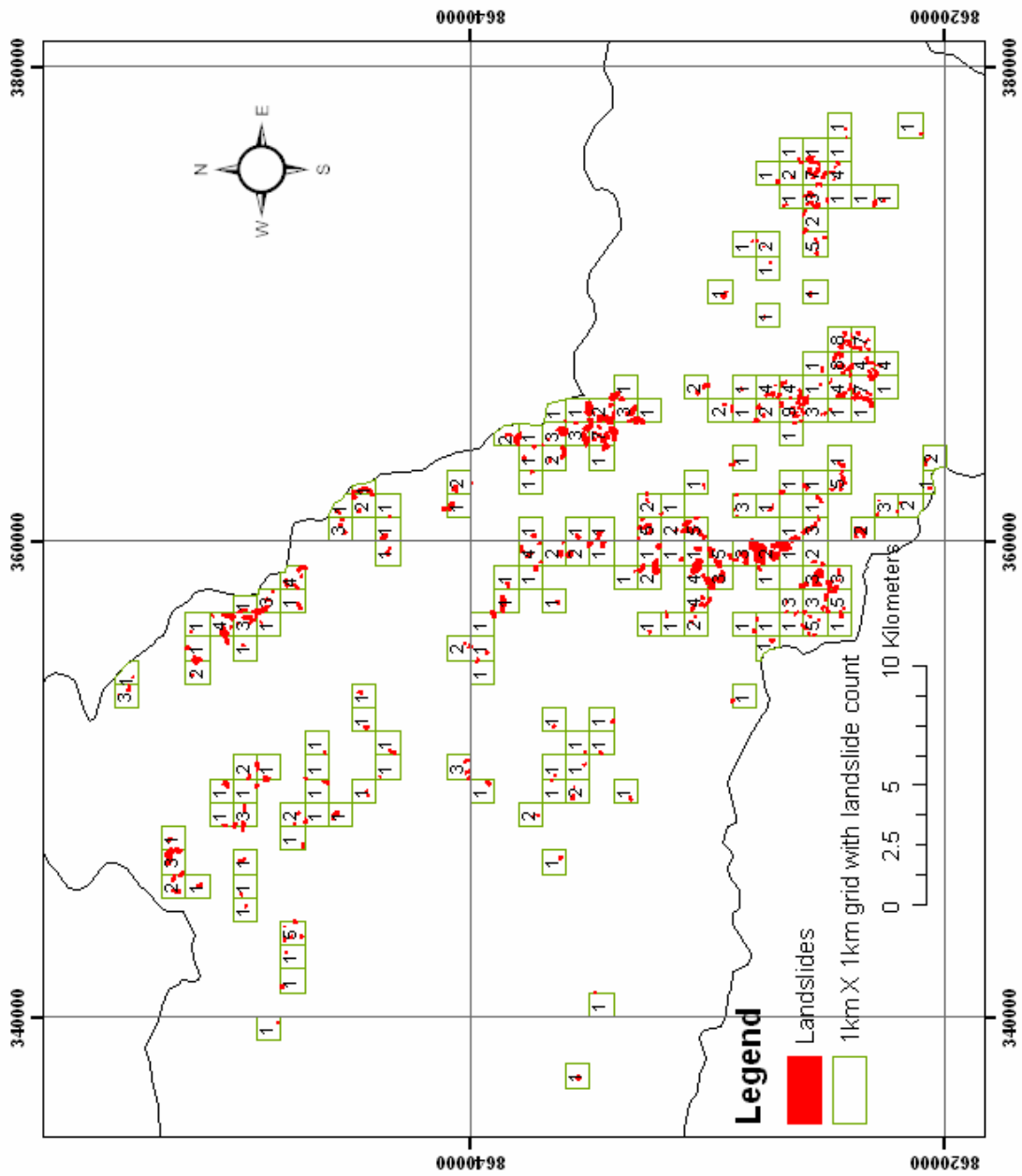


Fig. 2.9.2: Landslide count within 1km X 1km grid. The number inside each grid represents the number of landslides.

CHAPTER THREE

Results and discussion

In natural ecosystems, where accurate data on landslide are sparse or unavailable, the results from spatial analysis using GIS is a reasonable approach to understand causes of landslides. My study covers three important aspects of landslide study: landslide trend assessment, soil-water modeling using MIKE-SHE, and spatial regression. The result from the randomness checked whether there was a spatial trend. The internal cause for landslides was identified by spatial regression analysis.

3.1 Randomness

Fig. 3.1 shows the Ripley's K-function from the 381 individual landslides (before aggregating to 1km X 1km grids). The solid thick black line represents the L(d) (observed K-statistic); the grey dotted and dashed lines are 100 Monte Carlo simulation envelopes representing maximum and minimum L(d), respectively. The black dashed line at zero L(d) is the CSR line.

The K function showed clustering at 2km, and overall regional clustering up to the 13 km which was the maximum specified distance. The L(d) line is greater than both the random envelopes, suggesting non-randomness.

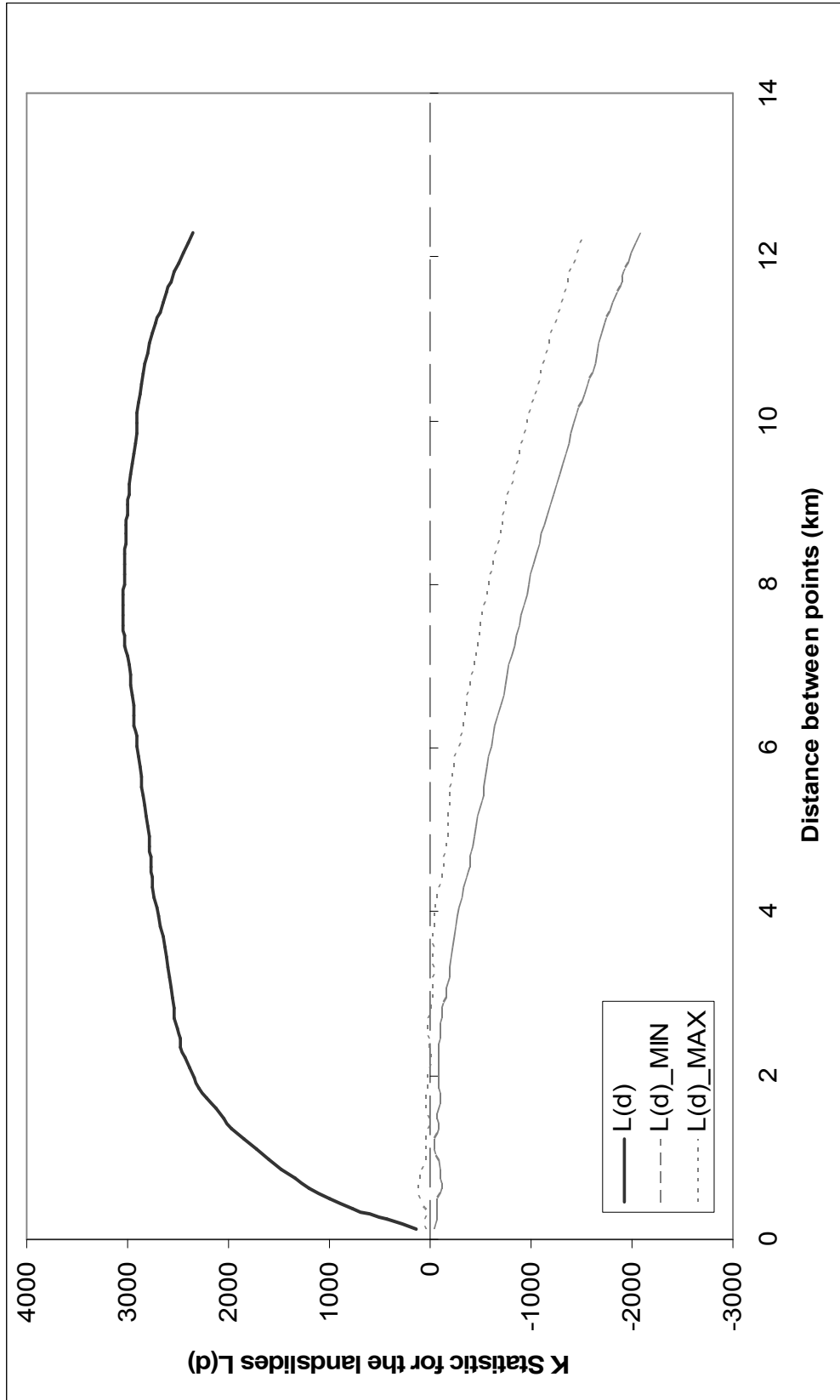


Fig. 3.1: Ripley's K-function plot for landslides. The solid black line is observed K-Statistic and the grey dotted and dashed line represents the 1000 simulation envelope. Black dashed line at zero is CSR (Complete spatial randomness) line. A clustering can be seen up to 2 km.

I propose the following possibilities for the 2km clustering: the basic soil properties at one location may not vary much within 2km radius or the similar soil water interactions may be assumed over 2 kilometer circle; The general fluvial processes on meander cutbanks can be correlated up to 2km distance from a point. These includes: cut bank erosion, failure due to chute cut off, erosion and failure due to crevasse splays, and reworking of sediments on point bars. The measurement of general meander length for the Los Amigos river suggested that the distances between meander bend was about 1 kilometer (see table 3.1). Since two meander lengths are involved in creating a cutoff, the average distance between cutoff points is close to 2km. Fig. 3.2 shows the Los Amigos meandering in 1960, 1980 and 2003. A loop length is the distance along A to B. A chute cutoff form between loops A to B and B to C; and thus, two loops are involved. Notice that in 2003, a chute cutoff had formed isolating loop B. The point bar areas of the isolated loop B are likely to contain weakened soils where landslides are more prone to occur.

3.2 Hydrologic Modeling

The variation of soil moisture content, changes in pressure head, variation in rainfall and evaporation when modeled, could give a clearer understanding of the effect of soil water contribution to landslides. Both wet and dry months have fluctuations in soil moisture content and pressure head. The changes in water content and pressure head along with rainfall rate and actual evaporation rate in two major soil types (sand and silty loam) are presented in two sections: one for wet period, and the other for dry period.

Table 3.1: River meander lengths for Los Amigos River. Distance denotes the straight distance between two adjacent apex of the meander.

Major meanders	Loop length (m)	Distance (m)
1	2433	889
2	3343	1018
3	2396	746
4	1616	918
5	2444	1017
6	1518	782
7	2158	1012
8	2245	1251
9	1565	606
10	1531	516
11	1781	869
12	2607	799
13	1160	1257
15	1837	927
16	1647	1386
17	1123	858
18	889	1216
19	3038	919
20	1199	1178
21	2970	1184
22	3427	754
23	2562	539
Average	2068	938

3.2.1 Soil water interaction in wet period

Soil water pressure frequently increases during high rainfall. There are many instances when unsaturated pressure head (suction head) approaches to zero (less than 1m or 9.8 kPa) during wet period (Fig. 3.2.1). Also, there is rapid decrease of pressure head with time when rainfall intensity is very low (Fig 3.2.2).

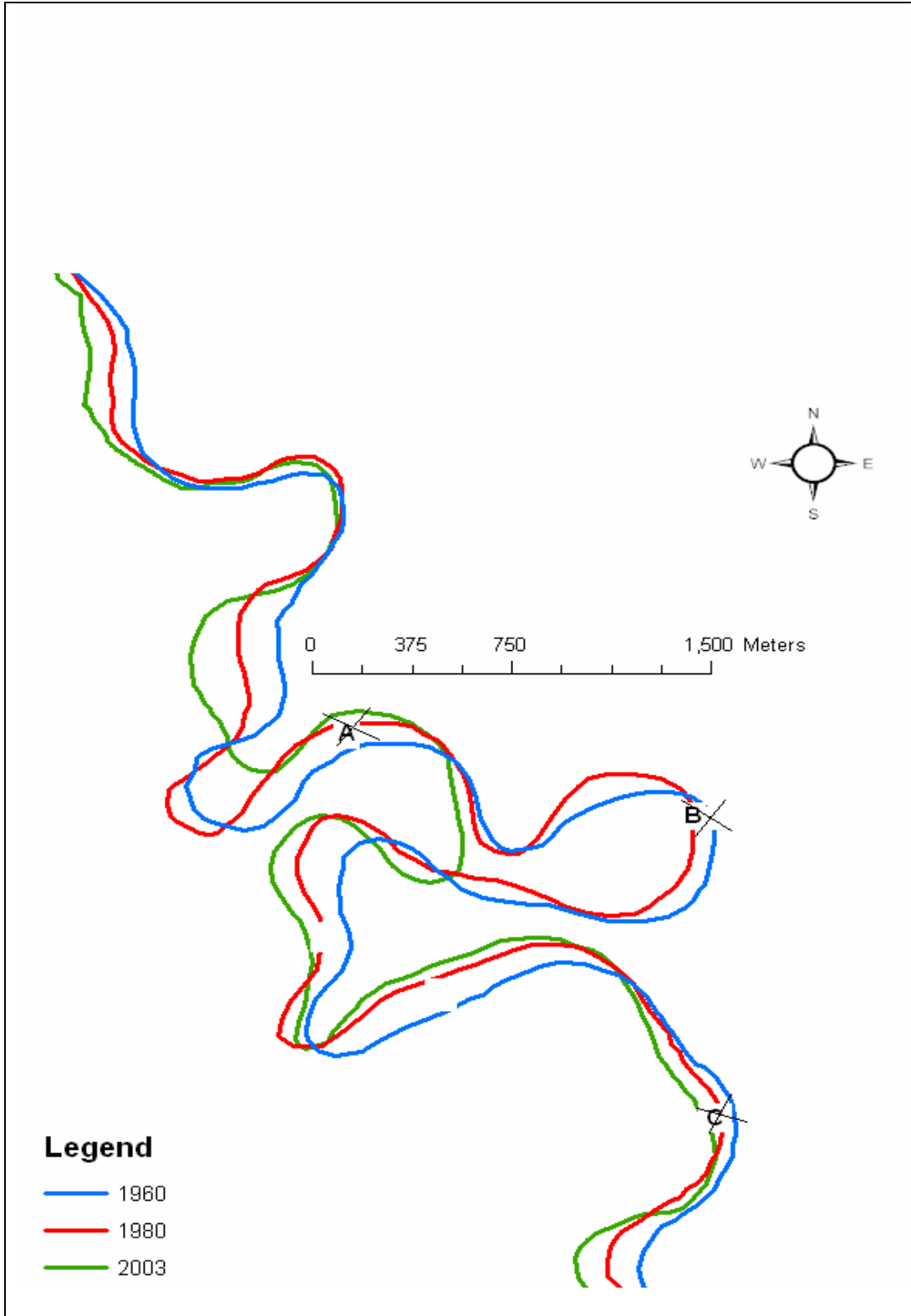


Fig. 3.2: A meandering part of Los Amigos River in 1960, 1980 and 2003. The average meander length is 1km. The loop length is the length following the river curve (eg. A - B or B - C).

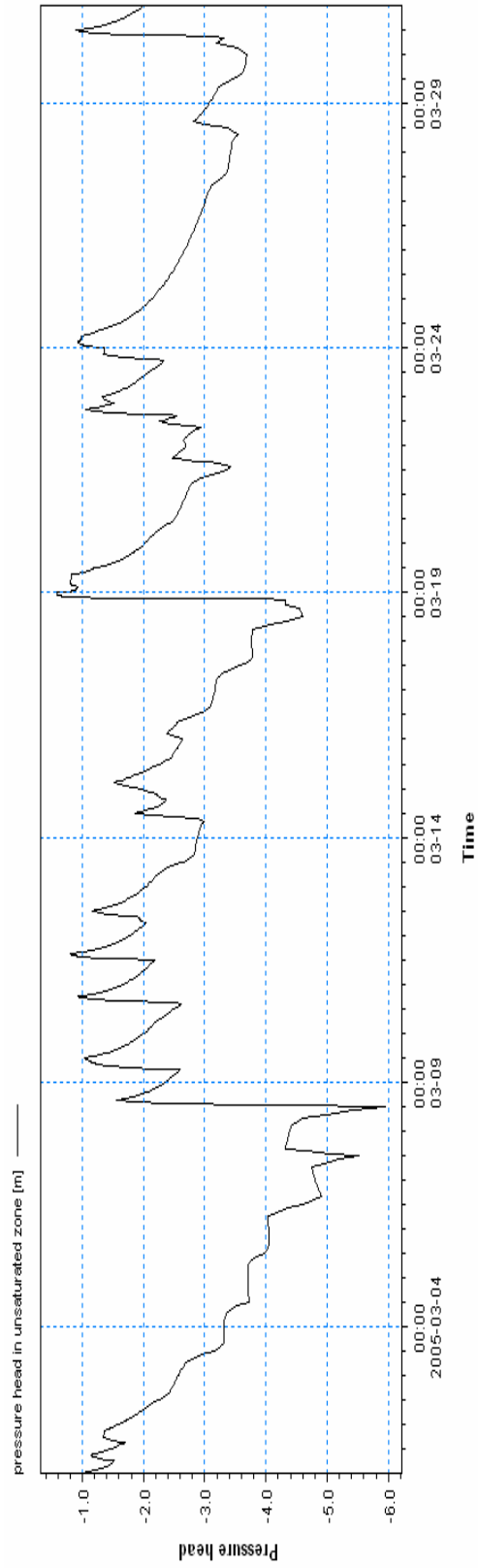


Fig. 3.2.1: pressure head in sand during wet period. Drop off in pressure head suggests rapid wetting and drying cycle of soils.

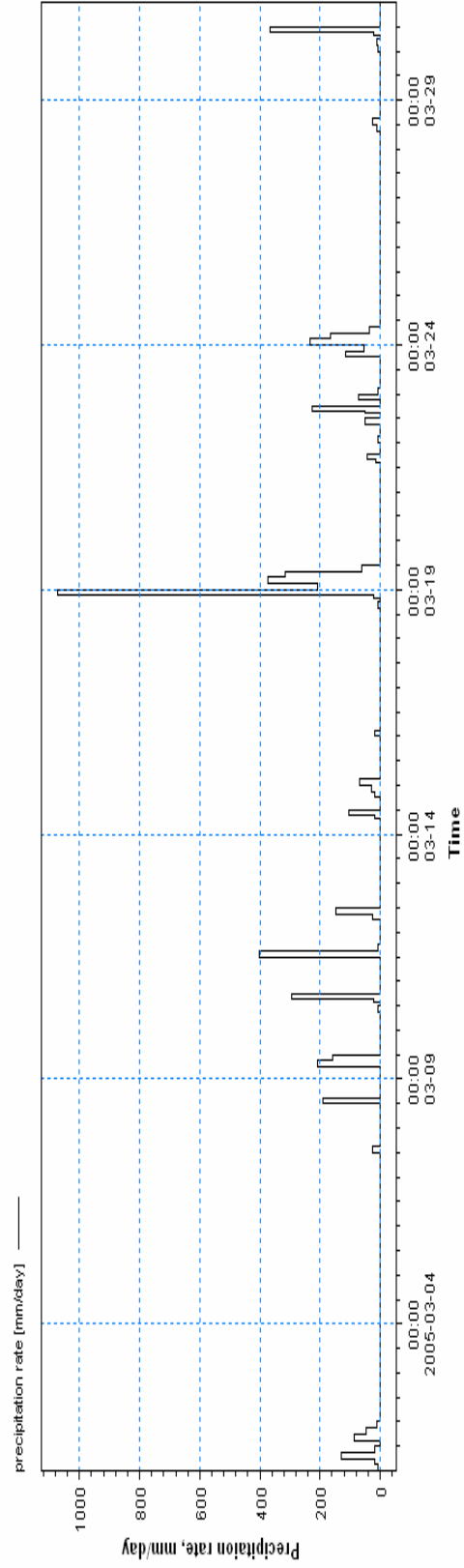


Fig. 3.2.2: Precipitation rate during wet period.

Even a very short 'no rainfall' period (3-5 days) created an appreciable drop in pressure head. Two factors might be responsible for decrease in pressure head. The first is dense vegetation which takes water from the soil. Since Amazonian forests have shallow rooting depth, the second responsible factor is soil water evaporation. If we look at soil-water evaporation (Fig. 3.2.4.) and rainfall (Fig. 3.2.2), the plots show the high evaporation rate following rainfall. The change in pressure head was similar overall silty loam (Fig. 3.2.4), but the pressure head fluctuations were noticeably reduced compared to the sandy soils.

3.2.2 Soil water interaction in dry period

There were no noticeable differences in the magnitude of pressure head change between wet period and dry period (Fig. 3.2.1 and 3.2.4). The only difference is low and infrequent rainfall during dry period (Fig. 3.2.6), and the more frequent soil drying cycles for the wetter period. In the dry period, the silty loam soil exhibited the similar changes in pressure head (Fig. 3.2.7).

So, for the soil texture (sandy soil and silty loam) for these example sites, it is clear that there is rapid up and down fluctuation in pressure head in the unsaturated soil zone before and following rainfall events. The change in unsaturated soil-water pressure indicates a decrease in effective stress (Since $d\sigma_e = -dP$).

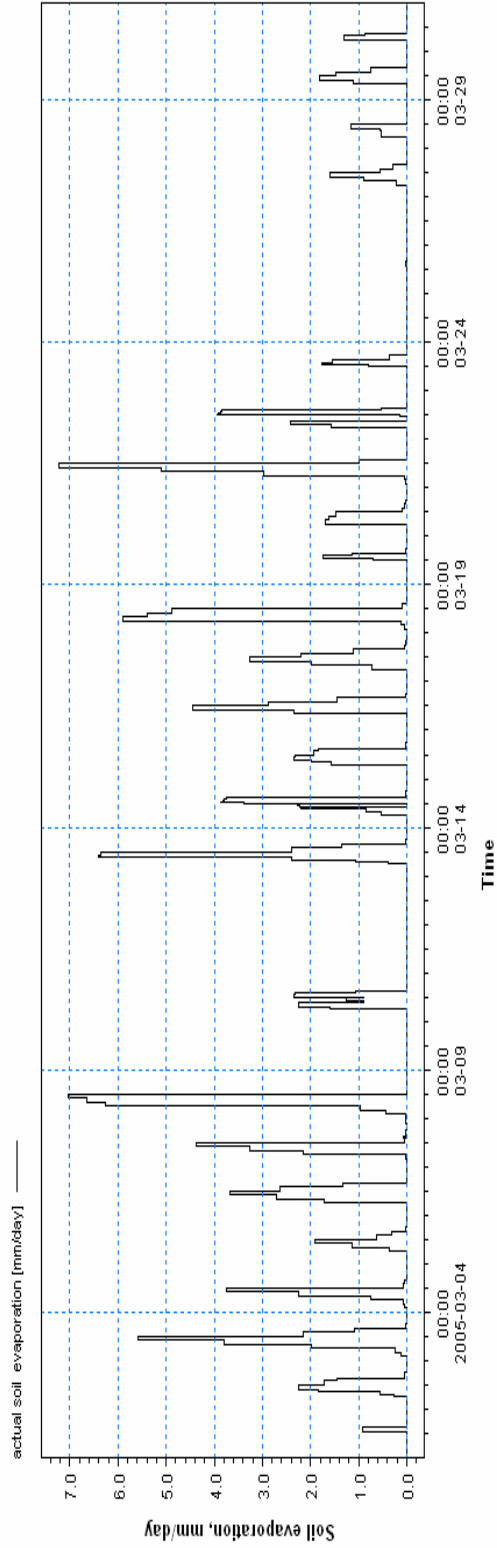


Fig. 3.2.3: Soil evaporation during wet period.

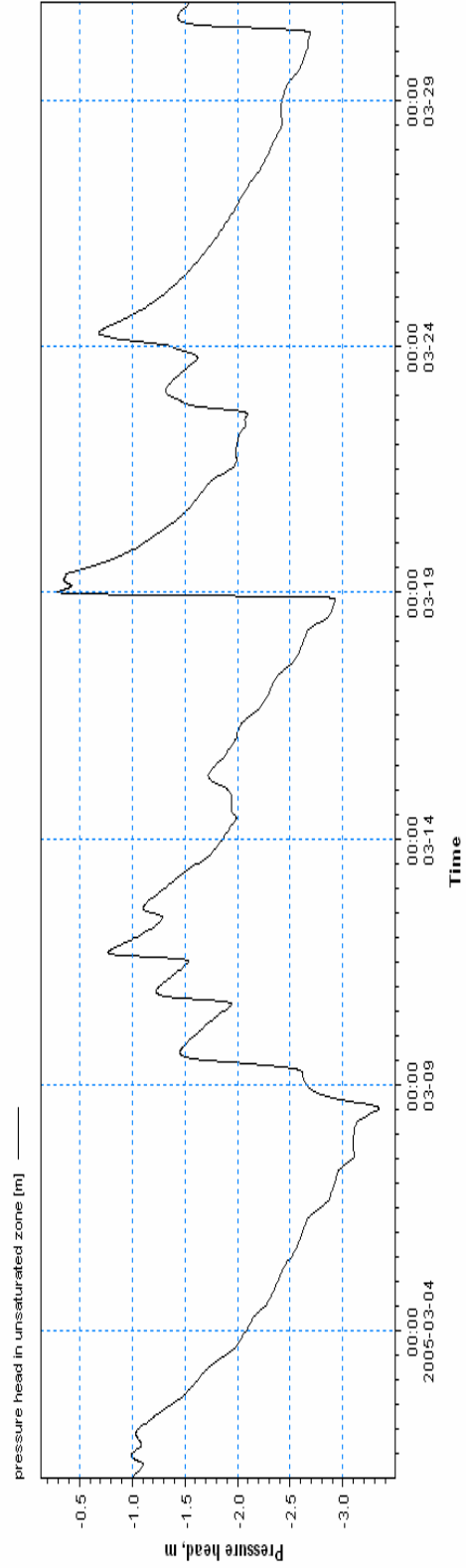


Fig. 3.2.4: Pressure head in silty loam soil during wet period.

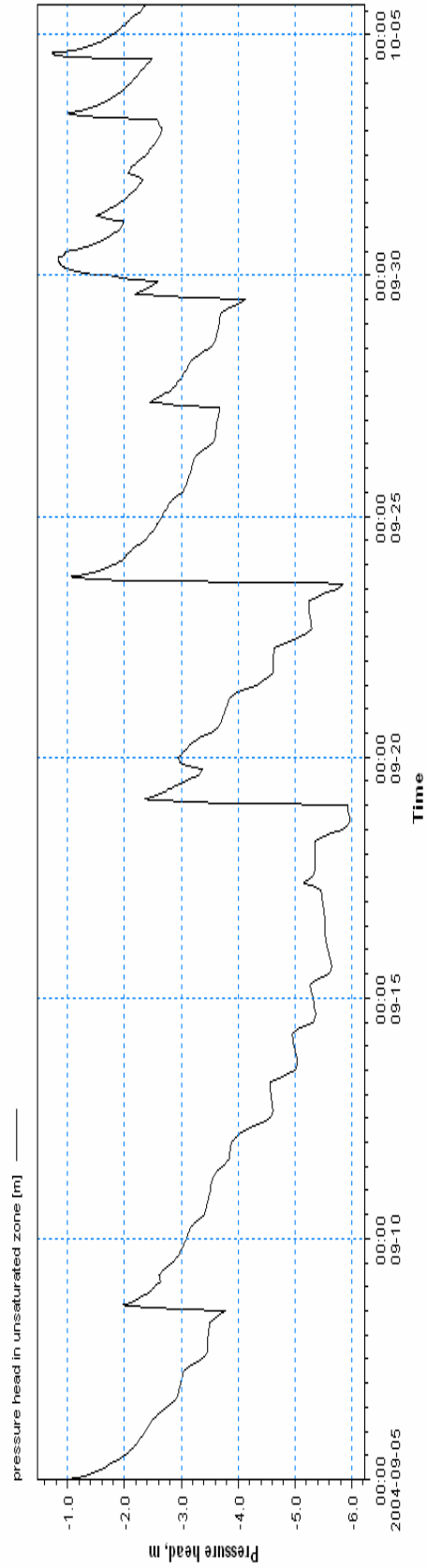


Fig. 3.2.5: Pressure head in sandy soil during dry period.

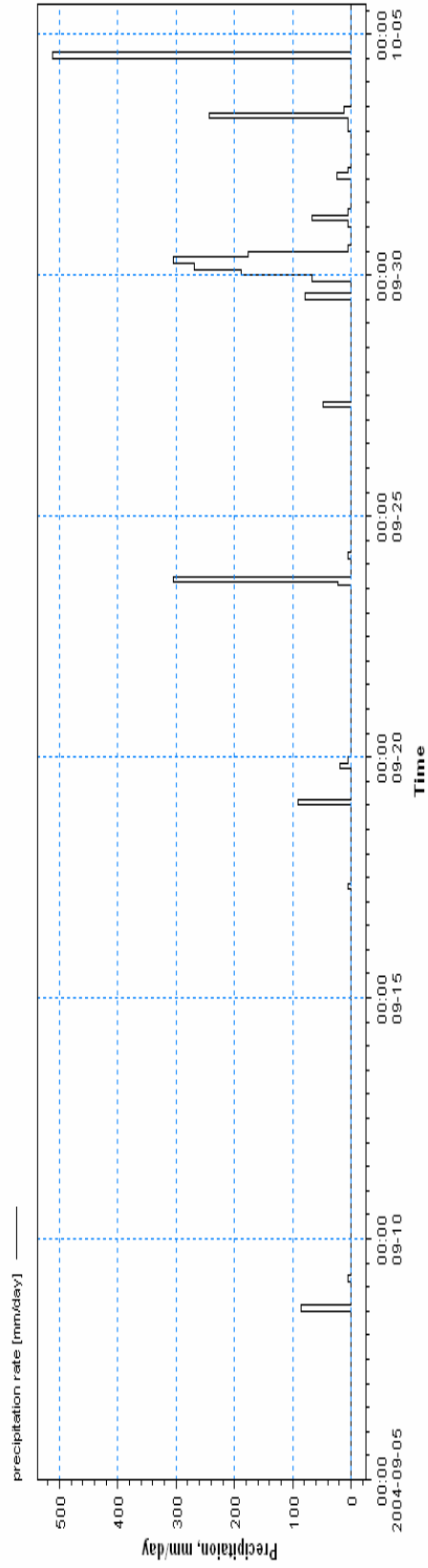


Fig. 3.2.6: Precipitation during dry period.

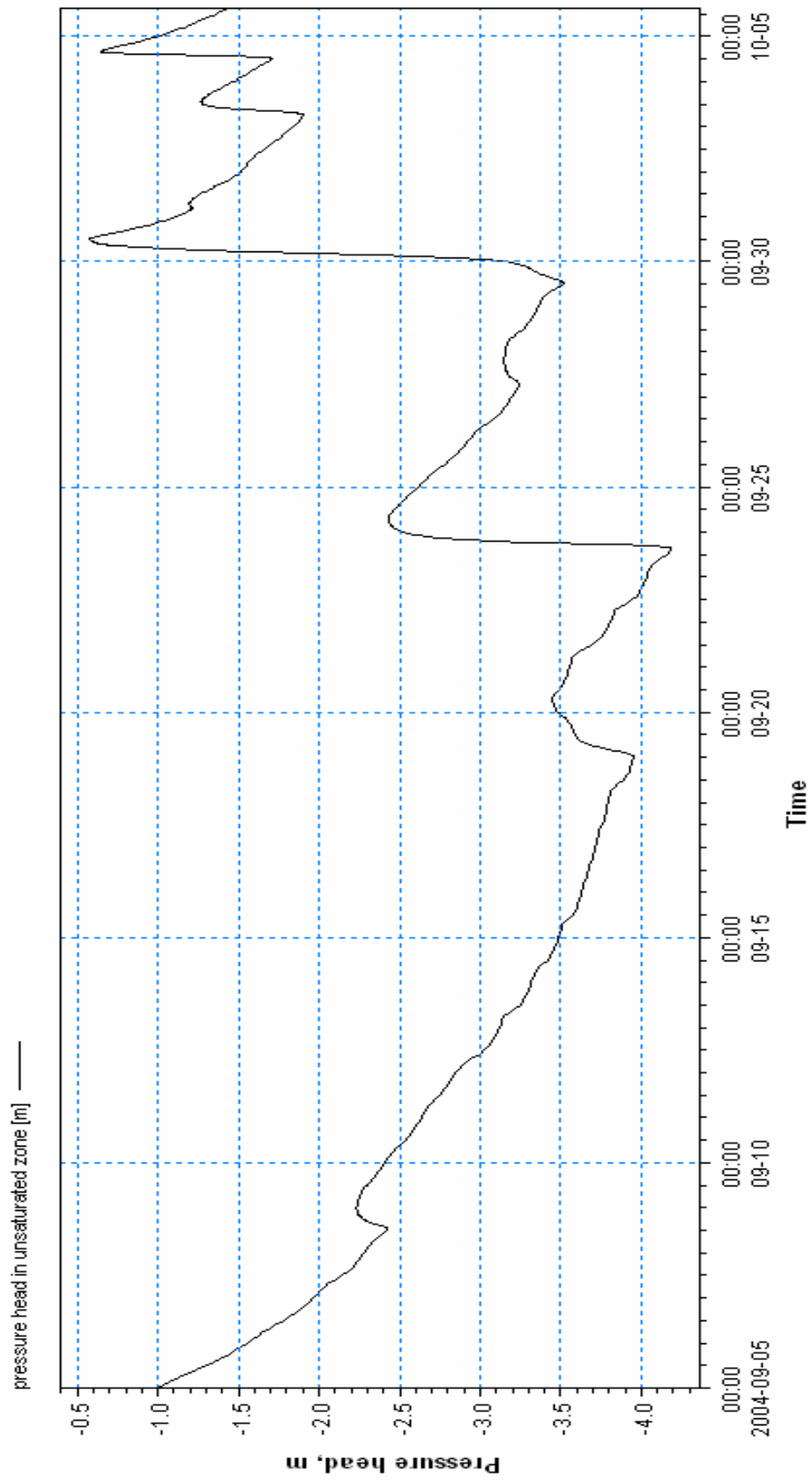


Fig. 3.2.7: Pressure head in silty loam during dry period.

Going back to Mohr-coulomb failure criterion, soil failure occurs when there is significant reduction in effective stress from change in pore water pressure, according to:

$$d\sigma_e = -\rho g \kappa dH . \quad (3.2.1)$$

Comparing unsaturated flow zone output for sandy soil and silty loam, in both cases the maximum changes in water content and pressure head occurs after the rainfall. Almost all changing patterns are the same for both soil types except that for the silty loam is smoother than that for sand. In sandy soil, a number of instances of drying and wetting cycles can be observed. Interestingly, most of the landslides are located on sandy soils (see fig. 3.2.8).

Along cutbanks and stream banks, the changes in pressure head are also dependent on changes in stream depth. So indirectly, all soil failures in the study area can be explained as rainfall-induced failures. In other words hydrologic modeling suggested that these landslides are the result of continuous input of rainfall, evaporation, root water uptake and variations in water table. The following section (section 3.3) used statistical significance tests for environmental variables.

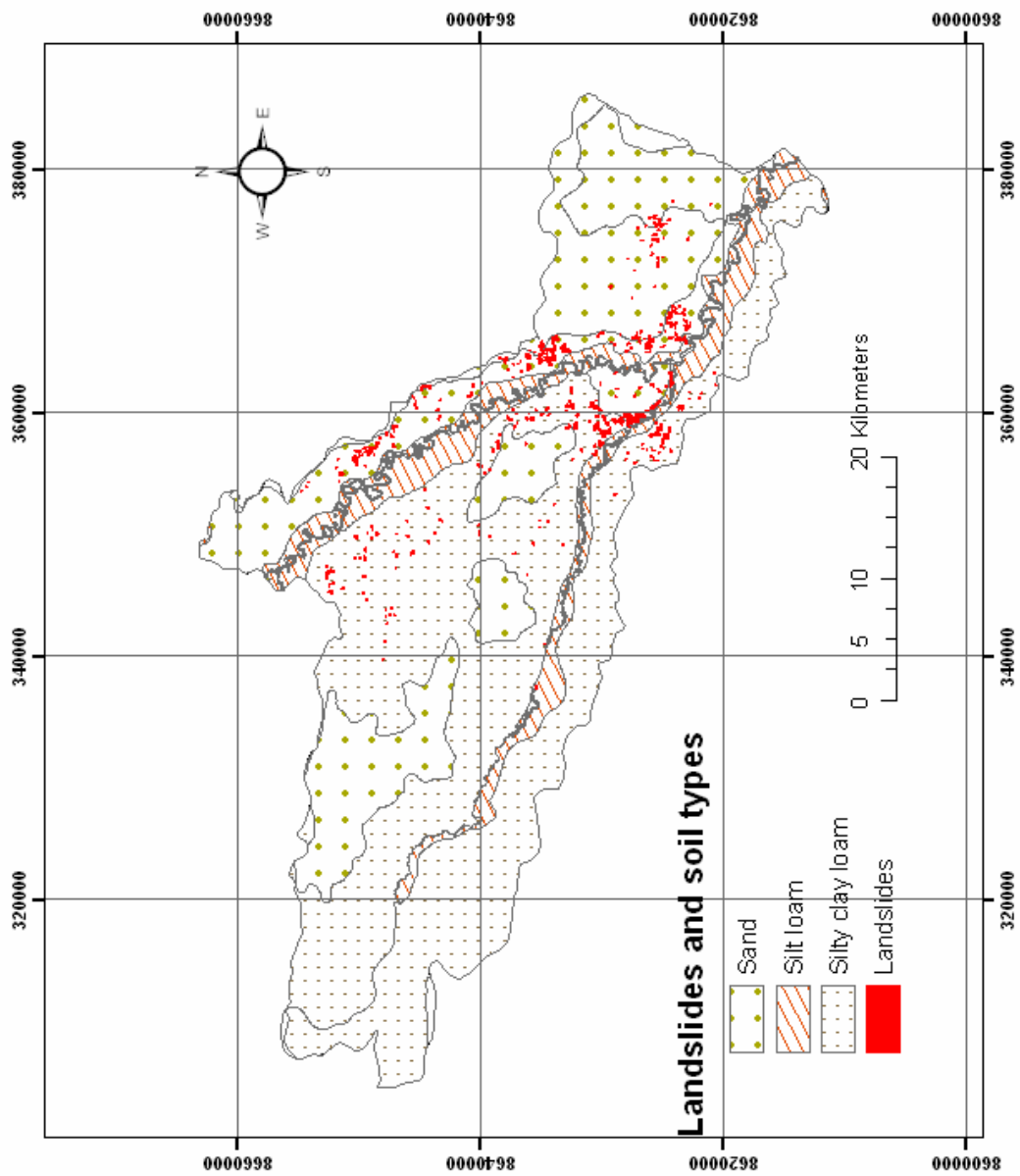


Fig. 3.2.8.: Distribution of landslides over different soil types. Majority of landslides are distributed along the sandy soil. The coordinate system is UTM.

3.3 Spatial heterogeneity

3.3.1 Result from OLS (ordinary least square estimation)

The following table (Table 3.3.1) shows the summary of output and coefficients for variables from ordinary least square estimation. The dependent variable was landslide count and the independent variables were slope, aspect, Standard deviation in pressure head for wet period (H_σ), and distance of landslide from the nearest river. The R^2 was 0.063182 for 190 observations with 185 degrees of freedom. Among the four variables: slope, aspect, distance from river and H_σ , only H_σ is positively related to landslide counts. The acceptable hypothesis here at $\alpha = 0.01$, is that the regression coefficients are zero except for H_σ .

Table 3.3.1: Environmental variables and corresponding regression coefficients

Independent Variable	Probability	Coefficient
Slope	0.5850986	-0.04168618
Distance from river	0.6712689	-0.000384877
H_σ , Standard deviation of pressure head	0.0058243	0.134671
Aspect	0.5308285	0.001032487

3.3.2 Spatial lag model

The spatial dependency was then re-estimated with maximum likelihood approach. The spatial lag model uses maximum likelihood method to determine the spatial dependency of the dependent variable. The following table (Table 3.3.2) shows the summary of output and variable coefficients from the spatial lag model. The R^2 was estimated as 0.131491 at 184 degree of freedom (higher than for the OLS model). The lag coefficient ρ was 0.262648. The landslide count (weight) is a new independent variable based on the weight matrix and is known as the “spatial lag term.” The weight matrix is estimated after Thiessen polygon segmentation of the study area.

Table 3.3.2: Environmental variables and their corresponding regression coefficients for spatial lag model.

Variable	Probability	Coefficient
landslide count (weight)	0.0024930	0.2626478
Slope	0.9054525	-0.008601649
Distance from river	0.4324563	-0.000675276
H_σ	0.0102254	0.1189587
Aspect	0.7517502	0.0004962102

Table 3.3.2 shows that H_σ is a significant variable at $\alpha = 0.05$ (since

Probability=0.01022 < 0.05). All other variables have no significance at $\alpha = 0.05$.

Now, let us see how in spatial lag model, the tests of heteroscedasticity and spatial dependence appear. The result of the heteroscedasticity test gave a probability value of 0.0000027 suggesting significant spatial dependence for landslide counts. A more refined spatial regression model does not assume equal variance for error (heteroscedasticity).

3.3.3 Spatial error model (heteroscedasticity)

The following table (Table 3.3.3) shows output summary and the variable's coefficients obtained from the spatial error model. Comparing this model with the spatial lag model, we can see a coefficient λ is added as another variable; λ is a coefficient representing spatially correlated errors. The R^2 value of 0.152374 was higher than for the spatial lag model. Thus the spatial error model is a refinement over the original OLS and spatial lag model. At significance levels, $\alpha = 0.05$, table 3.3.3, shows that the error coefficient λ and H_σ have non-zero coefficients. The environmental variables such as slope, aspect, and distance from river have no effect in the model.

Table 3.3.3: Environmental variables and their corresponding regression coefficients for spatial error model.

Variable	Probability	Coefficient
Slope	0.5835414	0.04207117
Distance from river	0.2541708	-0.000959969
H_σ	0.0036824	0.1465408
Aspect	0.8003094	0.0004697591
λ	0.0002831	0.30932

The three regression tests: OLS, spatial lag model, and the spatial error model, respectively, provide improved regression models (higher R^2 values). This suggests adopting the spatial error model to explain the spatial heterogeneity of landslide distribution is best. Although the spatial error model seems better in this case, all three models show correlations of landslide counts only exists with the standard deviation in pressure head (H_σ).

I now explain why there is significance only for H_σ in the models.

From equation (1.3):

$$\tau_f = c + (\sigma_t - P).Tan\phi. \quad (3.3.1)$$

Equation (3.3.1) can be written as:

$$\tau_f = c + \sigma_t.Tan\phi - P.Tan\phi \quad (3.3.2)$$

For a fixed weight at the bottom of a column, $\sigma_t = \text{constant}$. Thus, assuming constant cohesion c and friction angle ϕ :

$$d\tau_f = dP.Tan\phi \quad (3.3.3)$$

Equation (3.3.3) shows that the decrease (due to negative sign) in shear strength is equal to change in pore water pressure. During the wetting and drying cycles of soil, the pore water pressure changes with soil-water pressure. The effective stress (σ_e) is reduced by this change in pore pressure by dP (equation 3.3.6). Since the effective stress represents the pressure felt between the soil particles, the soil particles get compressed and the soil pore spacing gets reduced, compacting the soil. Over many wetting and drying cycles, the soil will get more and more compact. Eventually, the pore pressure required to fail the soil will become small (assuming equilibrium conditions).

3.4 Conceptual model for landscape development and landslides

Based on results obtained from, Ripley's K-function, hydrologic modeling, and spatial regression analysis, I am ready to explain the influence of landslides on landscape development. My study area contains meandering rivers. I chose a representative cross-section of Los Amigos River (Fig. 3.4.1). The initial stage is described by normal fluvial processes: a meandering river with no landslides. Upland drainage areas receive rainfall; stream bank soils get wet. Some of the bank soils could be point bars. When rainfall fluctuates between wet and dry day, the shear strength is reduced with changes to pore water pressure (Fig. 3.4.2) resulting in a landslides on terraces (*e.g.*, X and Y were previously terraced). As a result of looser sediments in landslides, the weak soil along river banks can be eroded away by river flow.

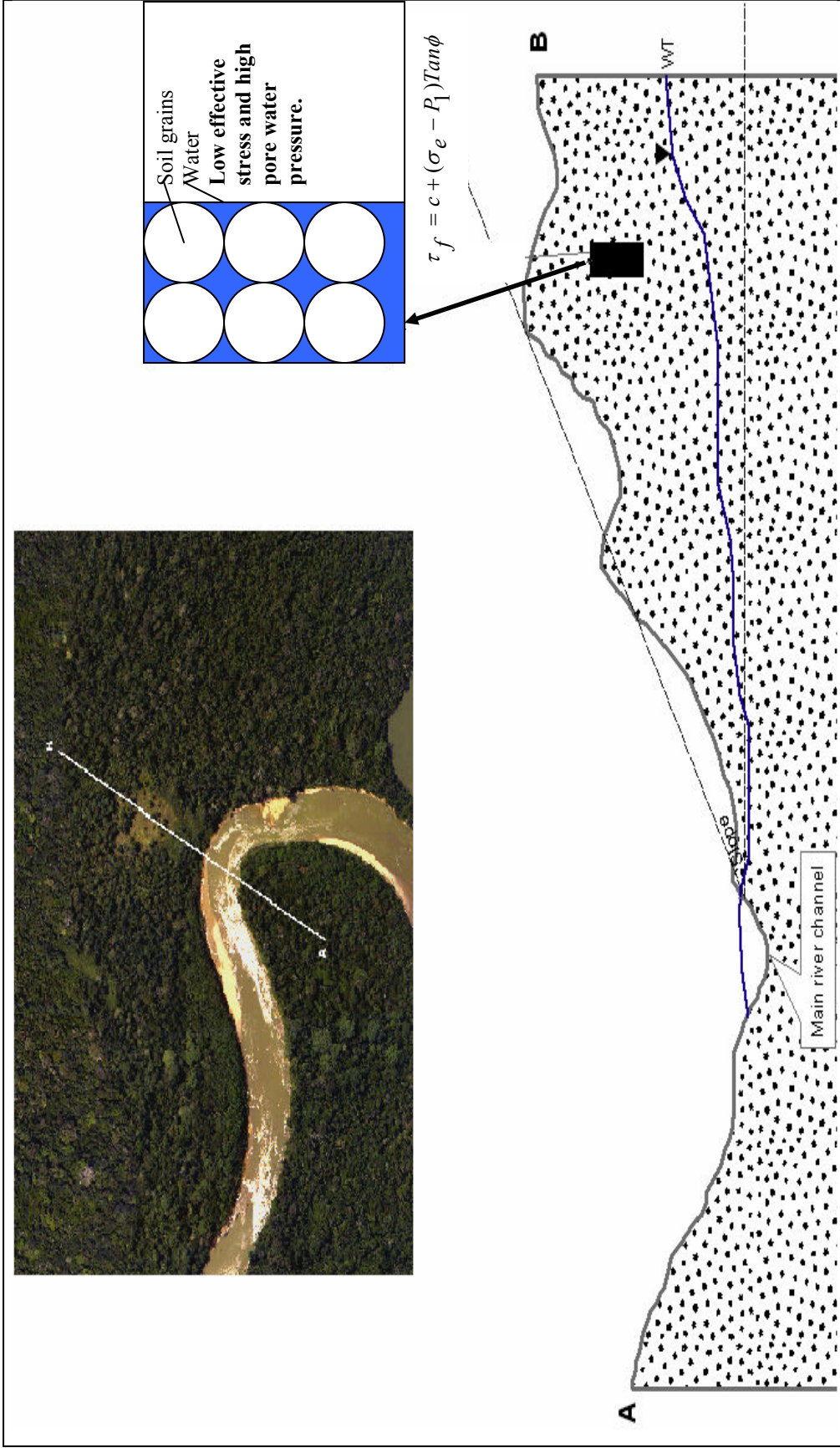


Fig. 3.4.1: Cross-sectional diagram for a meander on the Los Amigos River. This conceptual diagram shows the soil condition in absence of wet/dry cycling.

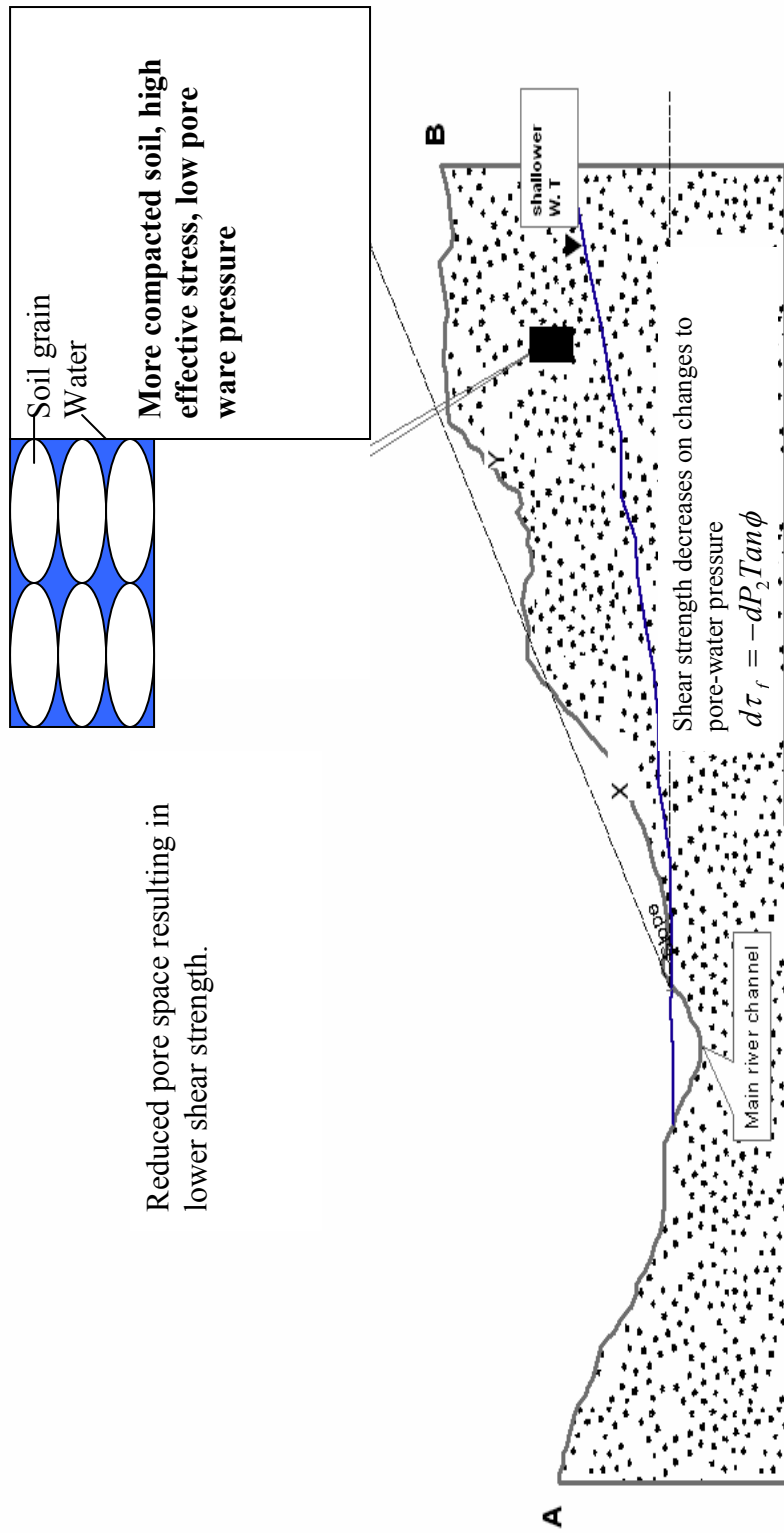


Fig. 3.4.2: Second stage cross-sectional diagram shows more compacted soils with reduced pore space. The shallower water table further reduces shear strength. Points X, and Y, represents observed landslides.

CHAPTER FOUR

Conclusions

My GIS study suggests that for terraced flood plains, a single environmental variable, variation in soil-water pressure (H_σ), is sufficient to explain landslide occurrences. H_σ is related to failure of the soil profile through $d\tau_f$.

I conclude the following:

- 1) The pattern of landslide distribution in lower Los Amigos sub-basin is non-random and spatially correlated at a distance of about 2km.
- 2) Landslide counts (within 1X1 km grids) are independent of slope, aspect, and distance from nearest river, but dependent on variation of pressure head in the soils.

It was surprising the slope was not related to landslide occurrence. My study suggests that soil failure on flat terraces due to soil moisture cycling is fundamentally sculpting the foreland basin. In watersheds with steeped slopes (*e.g.* Himalays), the loss of soil shear strength due to soil moisture cycling (which controls H_σ) is probably reducing the resistive force to soil weight along inclines.

APPENDIX – I

Monthly rainfall data for seven years:

1998

Latitude	Longitude	jan	feb	mar	apr	may	jun	jul	aug	sep	oct	nov	dec
-12.75	-71.00	493.894	585.435	458.584	267.231	200.464	98.2525	92.7855	110.69	267.581	459.732	595.646	558.797
-12.75	-70.75	475.512	594.028	468.941	274.654	204.037	102.959	100.958	126.782	270.089	431.521	699.56	665.641
-12.75	-70.50	525.778	577.328	462.281	306.402	215.255	104.296	112.033	143.337	310.111	460.59	647.881	627.774
-12.75	-70.25	543.731	588.368	457.073	286.748	205.026	106.384	115.307	162.346	316.029	513.476	736.598	633.452
-12.75	-70.00	546.341	590.469	478.358	315.195	201.197	94.6198	116.648	203.939	338.849	538.012	723.276	553.393
-12.50	-71.00	462.372	573.408	453.953	202.641	139.855	81.7568	85.8195	127.004	255.448	376.483	513.45	504.883
-12.50	-70.75	444.782	536.268	414.209	251.728	191.582	83.8249	93.6566	135.611	302.596	426.827	622.374	598.63
-12.50	-70.50	458.597	530.208	436.812	266.218	184.514	88.7592	99.6072	149.762	295.419	426.601	619.622	572.045
-12.50	-70.25	495.846	532.744	446.082	274.224	183.951	98.6021	107.798	155.415	295.844	503.693	674.237	537.962
-12.50	-70.00	506.21	543.292	447.74	289.162	171.718	87.2394	124.155	202.884	306.107	479.303	688.14	545.171
-12.25	-71.00	434.875	534.718	432.668	178.429	115.247	77.4834	86.7226	121.663	253.911	381.466	483.686	485.657
-12.25	-70.75	432.543	512.223	418.956	200.999	130.886	78.5727	92.606	136.649	257.655	413.088	548.603	491.958
-12.25	-70.50	439.359	503.19	428.776	237.086	154.188	84.9865	108.119	160.418	276.411	427.323	573.892	501.227
-12.25	-70.25	469.597	497.961	433.457	263.036	164.141	92.9627	107.691	157.904	290.292	468.275	595.695	493.726
-12.25	-70.00	468.127	514.715	440.074	281.336	155.877	79.7072	121.375	202.752	307.331	455.487	668.269	573.409
-12.00	-71.00	404.361	434.959	342.8	171.693	102.128	42.5009	51.5245	102.146	220.617	338.181	447.927	432.119
-12.00	-70.75	394.449	458.381	373.738	173.274	98.1801	30.5698	61.2538	120.157	225.267	354.439	467.518	445.673
-12.00	-70.50	401.491	439.872	359.505	190.176	108.484	35.8957	61.293	119.255	231.903	352.274	503.261	489.646
-12.00	-70.25	394.741	421.828	341.582	186.055	112.918	42.3911	66.1418	133.23	243.269	351.093	544.011	547.503
-12.00	-70.00	417.28	447.483	397.806	244.08	103.498	39.6348	103.601	213.708	318.83	452.548	587.68	531.418

Monthly rainfall data for seven years (con.)

1999

Latitude	Longitude	jan	feb	mar	apr	may	jun	jul	aug	sep	oct	nov	dec
-12.75	-71.00	528.297	693.432	436.693	241.867	246.281	126.866	80.1191	163.037	186.508	147.069	322.391	482.501
-12.75	-70.75	487.49	654.337	422.076	231.633	236.279	124.014	71.0091	158.49	182.49	149.445	341.215	489.413
-12.75	-70.50	458.098	530.945	353.06	229.588	229.366	122.243	64.7803	162.996	185.212	157.686	337.897	475.774
-12.75	-70.25	432.75	507.605	324.186	226.591	244.646	135.507	70.9685	193.043	212.821	169.704	347.406	472.783
-12.75	-70.00	406.017	483.374	284.481	186.421	226.949	135.479	47.7912	185.918	227.32	200.664	320.814	465.048
-12.50	-71.00	446.442	565.416	360.795	259.48	261.933	105.786	59.5715	148.358	176.226	155.934	312.248	460.305
-12.50	-70.75	421.928	535.274	348.619	248.478	256.994	118.434	64.4515	166.727	195.5	156.819	314.67	460.351
-12.50	-70.50	403.016	529.068	368.062	245.447	247.414	127.081	73.1979	178.454	193.448	161.995	333.576	468.958
-12.50	-70.25	379.901	456.32	314.063	266.108	282.914	150.812	82.5667	199.333	203.756	170.245	351.397	472.039
-12.50	-70.00	363.381	424.687	259.891	214.762	250.583	132.947	50.0096	197.479	235.035	217.918	342.014	439.195
-12.25	-71.00	437.271	506.522	333.013	342.443	337.641	107.851	59.155	197.218	228.247	156.759	317.56	495.707
-12.25	-70.75	407.804	491.457	324.56	315.22	327.424	126.439	64.1204	219.952	243.036	159.967	319.377	478.88
-12.25	-70.50	392.93	477.959	333.7	294.497	294.586	135.839	77.6946	188.501	201.057	174.72	335.151	459.788
-12.25	-70.25	383.06	453.774	325.154	308.823	317.136	148.039	68.9185	179.732	206.328	181.993	354.028	477.027
-12.25	-70.00	377.215	414.052	263.363	223.583	247.666	121.822	48.2144	187.404	247.146	231.44	361.574	462.412
-12.00	-71.00	414.646	514.443	374.193	386.33	329.544	78.8513	43.5078	202.618	230.971	172.944	329.895	442.513
-12.00	-70.75	389.606	446.547	323.915	398.308	356.114	79.186	38.2962	186.138	214.676	178.525	348.667	447.421
-12.00	-70.50	395.814	425.292	303.839	359.53	314.581	80.6418	38.0693	143.485	172.939	191.53	372.478	483.903
-12.00	-70.25	423.942	442.3	303.524	332.257	290.825	82.1929	40.609	133.006	182.591	227.328	424.635	535.189
-12.00	-70.00	435.171	411.503	262.118	231.208	216.423	96.883	37.2359	151.359	205.596	232.18	405.228	526.504

Monthly rainfall data for seven years (con.)

2000

Latitude	Longitude	jan	feb	mar	apr	may	jun	jul	aug	sep	oct	nov	dec
-12.75	-71.00	489.386	585.716	560.57	244.898	102.695	87.7569	93.3415	157.537	270.446	485.638	692.726	878.206
-12.75	-70.75	493.268	593.357	517.044	202.833	96.0365	90.1745	93.3563	147.041	274.002	521.367	724.684	823.999
-12.75	-70.50	497.849	596.549	593.596	286.343	105.669	104.634	102.251	152.517	249.814	458.538	668.244	797.299
-12.75	-70.25	510.446	638.649	653.222	330.785	124.026	129.377	117.378	184.307	258.275	367.121	540.759	753.89
-12.75	-70.00	541.083	685.225	656.734	310.805	149.07	131.661	112.93	146.801	219.052	357.885	486.874	759.672
-12.50	-71.00	439.067	499.185	495.883	219.348	98.4663	87.2486	77.11	131.562	222.076	459.143	716.745	776.607
-12.50	-70.75	465.81	538.9	487.642	209.958	106.422	94.1751	74.5631	131.099	222.347	397.039	536.751	661.938
-12.50	-70.50	511.525	582.841	501.238	232.625	112.75	98.192	86.2048	148.7	234.559	339.376	488.18	671.354
-12.50	-70.25	522.415	604.577	550.52	270.237	106.086	94.0086	90.752	151.073	235.155	328.766	464.361	677.165
-12.50	-70.00	486.77	598.885	540.7	248.672	131.824	100.097	99.6047	149.875	221.071	335.561	452.591	711.999
-12.25	-71.00	484.966	497.03	468.002	231.026	118.859	93.944	69.6518	98.9634	200.373	449.576	545.805	577.854
-12.25	-70.75	483.809	506.666	471.87	237.131	125.974	114.846	82.8588	103.362	207.363	378.206	437.282	546.88
-12.25	-70.50	493.836	544.445	479.214	233.694	121.608	110.062	89.4086	118.836	202.697	305.633	388.251	581.992
-12.25	-70.25	496.942	573.626	501.715	237.746	134.675	121.94	104.728	119.048	186.604	300.618	403.39	602.921
-12.25	-70.00	468.117	545.12	457.761	194.221	118.396	114.645	113.191	113.885	204.362	351.746	445.542	622.021
-12.00	-71.00	428.083	456.757	463.62	269.744	112.258	87.8866	81.4192	77.8493	192.62	396.181	390.326	484.138
-12.00	-70.75	446.951	477.74	445.802	286.33	147.842	83.0658	70.8888	70.6024	162.648	291.816	326.413	500.261
-12.00	-70.50	490.24	505.316	481.473	307.014	143.977	93.4617	83.8685	78.7107	158.641	274.223	346.5	535.154
-12.00	-70.25	451.434	468.601	441.26	228.474	127.891	117.044	111.904	85.3915	171.117	288.433	357.604	539.444
-12.00	-70.00	448.921	474.084	437.602	187.004	116.854	107.854	120.415	117.193	198.06	340.764	397.257	521.913

Monthly rainfall data for seven years (con.)

2001

Latitude	Longitude	jan	feb	mar	apr	may	jun	jul	aug	sep	oct	nov	dec
-12.75	-71.00	869.906	643.161	383.695	211.149	138.429	107.095	111.323	116.548	270.735	343.34	382.155	503.003
-12.75	-70.75	830.801	661.636	380.769	221.473	159.382	114.597	117.989	119.362	253.306	326.788	387.341	520.062
-12.75	-70.50	840.35	652.482	344.142	240.694	193.688	119.733	132.739	125.416	223.491	330.507	431.031	513.957
-12.75	-70.25	848.788	628.81	327.273	220.644	185.326	137.494	124.004	111.79	263.777	391.17	446.723	483
-12.75	-70.00	865.816	567.369	312.078	226.865	185.274	140.801	134.882	111.148	259.918	413.226	488.711	543.014
-12.50	-71.00	736.887	630.384	397.094	256.712	177.783	93.4864	97.0224	114.473	286.467	358.335	359.865	420.138
-12.50	-70.75	782.267	683.283	404.859	254.64	192.32	87.3694	77.4175	101.614	233.682	314.26	393.904	483.442
-12.50	-70.50	730.192	605.639	359.517	225.227	191.533	104.806	87.5739	105.415	219.927	337.71	454.631	503.628
-12.50	-70.25	696.267	532.643	344.268	216.758	170.32	100.688	87.1891	113.408	274.621	403.724	448.903	475.286
-12.50	-70.00	756.828	498.743	326.032	241.048	175.226	105.042	113.984	123.694	247.243	385.888	487.027	574.356
-12.25	-71.00	639.595	519.929	331.274	209.529	138.406	75.2932	68.1727	82.105	218.302	312.038	343.561	372.044
-12.25	-70.75	641.455	532.479	339.575	249.903	201.257	87.9214	73.4587	96.7163	204.764	318.64	401.899	438.443
-12.25	-70.50	618.848	518.259	370.922	247.518	219.261	112.56	86.9852	120.876	227.182	346.436	439.953	469.338
-12.25	-70.25	597.56	472.849	374.629	277.615	206.325	101.101	92.459	113.125	244.872	362.017	423.879	511.471
-12.25	-70.00	600.374	446.068	371.875	341.388	242.439	93.9191	87.0606	107.747	252.223	365.66	454.551	609.181
-12.00	-71.00	571.274	473.626	376.662	226.461	142.022	71.8043	82.5057	129.88	190.972	288.941	363.356	390.566
-12.00	-70.75	566.107	438.457	327.724	230.59	184.338	92.5976	94.4833	169.43	234.583	310.142	372.687	394.145
-12.00	-70.50	510.783	428.391	381.568	232.158	165.021	74.5917	107.04	173.374	232.343	350.8	423.989	380.802
-12.00	-70.25	509.638	374.11	322.718	278.3	218.87	88.4094	98.855	143.081	235.523	347.502	391.626	385.028
-12.00	-70.00	522.182	442.901	372.66	274.117	208.183	98.0359	81.1053	128.206	293.145	397.067	434.421	491.755

Monthly rainfall data for seven years (con.)

2002

Latitude	Longitude	jan	feb	mar	apr	may	jun	jul	aug	sep	oct	nov	dec
-12.75	-71.00	597.599	554.506	415.38	279.637	128.281	91.2841	90.2976	85.4664	331.063	439.717	606.407	698.349
-12.75	-70.75	633.914	552.599	399.31	295.848	145.425	90.5556	91.8578	107.737	380.773	499.22	504.553	619.189
-12.75	-70.50	658.045	595.082	397.37	303.767	163.563	101.766	97.8509	135.429	353.194	473.542	499.669	624.384
-12.75	-70.25	617.99	569.884	376.28	318.126	182.716	95.6648	92.4983	137.492	302.873	410.72	533.911	616.223
-12.75	-70.00	610.64	529.244	316.674	282.639	199.26	81.1862	71.6167	117.069	265.53	465.298	708.203	707.879
-12.50	-71.00	499.784	492.313	391.466	252.986	94.0777	67.975	81.1581	90.3105	285.077	385.364	527.133	560.807
-12.50	-70.75	583.819	510.074	357.347	250.635	111.691	96.9848	95.8182	109.547	317.052	419.135	550.594	619.655
-12.50	-70.50	599.394	521.946	347.423	264.722	134.68	98.9385	98.8705	119.544	326.911	461.746	593.225	672.366
-12.50	-70.25	579.315	493.283	302.285	261.383	158.376	96.8699	94.5015	127.406	288.759	431.343	652.454	714.583
-12.50	-70.00	626.402	498.662	281.7	256.361	182.436	76.449	72.819	112.702	280.667	400.568	679.948	754.081
-12.25	-71.00	453.361	425.594	346.474	253.951	93.1665	66.737	70.8666	71.387	235.355	326.484	593.855	660.36
-12.25	-70.75	513.847	434.97	340.554	257.87	96.2519	81.9529	92.1298	95.539	248.29	366.076	553.594	628.141
-12.25	-70.50	502.038	406.004	340.129	282.315	118.078	84.4421	102.25	106.466	244.334	387.034	611.806	673.144
-12.25	-70.25	573.5	428.328	301.341	263.007	138.208	78.1495	102.049	124.559	215.889	339.27	565.11	606.599
-12.25	-70.00	603.863	441.893	303.361	252.447	167.265	67.3	85.0832	116.937	255.506	439.033	594.416	577.518
-12.00	-71.00	449.504	379.402	329.645	278.84	111.347	67.8797	69.0008	77.8955	215.268	345.3	460.668	500.184
-12.00	-70.75	467.784	393.213	350.86	299.342	109.608	86.1453	99.8531	106.854	222.918	317.89	451.704	508.896
-12.00	-70.50	427.62	387.873	347.988	313.251	131.701	73.4534	82.7568	105.142	217.679	326.083	457.294	504.771
-12.00	-70.25	444.717	416.917	336.011	297.621	146.224	59.6238	70.7109	100.302	179.674	276.452	409.128	462.128
-12.00	-70.00	486.824	390.374	292.223	250.214	129.447	49.8541	55.969	82.5796	205.998	359.61	469.452	479.257

Monthly rainfall data for seven years (con.)

2003

Latitude	Longitude	jan	feb	mar	apr	may	jun	jul	aug	sep	oct	nov	dec
-12.75	-71.00	590.64	675.849	546.988	278.524	203.454	153.704	59.0033	175.376	348.823	287.47	285.125	753.024
-12.75	-70.75	527.023	587.941	558.177	252.185	181.797	150.925	74.0664	168.819	351.248	320.271	312.777	811.287
-12.75	-70.50	538.015	568.108	535.397	237.939	197.04	153.794	53.5378	150.539	359.183	337.089	346.636	811.721
-12.75	-70.25	488.228	553.083	534.113	241.321	146.537	112.069	52.5141	152.17	366.012	363.534	393.336	800.05
-12.75	-70.00	519.624	553.763	496.407	223.324	156.998	127.344	55.7224	154.271	392.412	399.13	342.001	574.67
-12.50	-71.00	418.061	471.459	428.989	246.256	165.212	121	57.7133	152.212	301.028	262.81	267.337	727.44
-12.50	-70.75	452.387	533.983	492.911	244.067	168.07	110.934	67.8155	166.049	332.587	314.378	311.063	724.104
-12.50	-70.50	521.906	626.754	550.915	238.742	169.78	108.103	54.9212	168.519	379.025	355.638	330.932	722.255
-12.50	-70.25	541.164	668.114	590.217	231.799	151.109	116.05	61.5092	190.665	422.422	396.222	367.675	760.423
-12.50	-70.00	528.282	581.399	492.219	220.167	177.411	137.796	75.5906	188.803	424.852	422.067	357.469	618.026
-12.25	-71.00	426.593	462.645	391.63	230.411	152.773	90.3743	65.9743	138.094	283.695	291.303	292.666	670.177
-12.25	-70.75	503.273	496.751	385.272	216.55	141.06	83.4947	70.9664	163.085	328.284	331.402	334.378	658.409
-12.25	-70.50	504.164	559.434	466.06	215.934	146.365	99.7745	62.2818	154.482	327.423	330.994	352.343	663.154
-12.25	-70.25	493.968	610.503	520.834	236.559	162.129	111.735	49.7339	137.055	328.711	359.19	366.112	644.441
-12.25	-70.00	479.471	603.427	517.304	218.046	171.807	126.179	59.7274	149.33	334.791	353.759	343.609	568.991
-12.00	-71.00	431.953	436.947	361.228	209.414	162.577	97.8158	77.3731	129.076	260.084	305.017	343.481	554.356
-12.00	-70.75	464.58	511.67	400.35	224.467	169.676	92.9438	89.0029	143.204	264.329	321.032	371.752	574.393
-12.00	-70.50	494.251	602.099	477.378	220.984	179.389	123.044	93.51	146.355	286.775	352.497	392.136	570.742
-12.00	-70.25	505.735	644.097	496.004	218.807	189.924	131.454	56.8785	133.752	314.638	344.676	364.979	514.116
-12.00	-70.00	496.792	571.041	427.642	186.812	160.821	119.795	48.7637	136.633	299.777	326.157	356.358	535.602

Monthly rainfall data for seven years (con.)

2004

Latitude	Longitude	jan	feb	mar	apr	may	jun	jul	aug	sep	oct	nov	dec
-12.75	-71.00	790.426	427.032	339.049	220.281	85.7689	144.7	149.103	94.9134	138.06	230.254	346.768	384.385
-12.75	-70.75	865.923	491.856	351.896	227.752	124.323	154.954	139.567	102.766	139.368	208.71	350.83	435.171
-12.75	-70.50	886.605	551.821	380.548	270.526	136.992	116.405	121.604	111.45	152.661	241.062	429.494	509.68
-12.75	-70.25	847.438	593.359	405.576	236.17	127.292	131.993	133.992	97.8219	155.889	287.98	418.742	476.233
-12.75	-70.00	654.524	551.727	414.677	284.882	162.245	145.87	141	89.9237	161.652	287.597	415.117	493.71
-12.50	-71.00	804.117	439.674	255.94	155.62	84.5404	106.413	114.719	98.5868	119.161	180.162	281.026	341.185
-12.50	-70.75	772.504	435.379	281.496	171.769	76.6679	95.3094	117.688	111.297	132.22	186.497	292.417	359.942
-12.50	-70.50	749.656	454.244	344.866	217.193	93.639	105.121	120.077	111.123	150.622	244.598	341.269	373.085
-12.50	-70.25	742.058	442.22	391.583	238.773	83.7924	102.598	123.434	116.209	151.005	262.623	356.72	371.064
-12.50	-70.00	614.976	430.749	408.012	292.017	122.321	126.071	126.052	88.7831	171.344	298.71	356.368	427
-12.25	-71.00	700.245	405.375	248.51	135.238	79.722	68.6346	84.2721	105.298	127.751	181.686	243.97	289.197
-12.25	-70.75	627.47	372.443	301.683	173.37	64.33	66.0766	92.9572	124.072	148.786	202.927	279.929	320.657
-12.25	-70.50	601.844	362.908	367.237	230.735	66.8222	93.7207	113.156	120.298	158.688	215.889	360.745	412.454
-12.25	-70.25	618.664	412.962	372.058	208.994	74.5106	107.333	111.845	104.481	139.387	220.752	354.626	384.496
-12.25	-70.00	567.781	420.259	373.711	213.152	66.8061	101.823	111.807	101.454	158.503	262.378	370.277	405.213
-12.00	-71.00	523.9	422.184	287.267	129.716	71.6636	49.5579	83.0727	128.173	156.312	233.609	249.936	271.609
-12.00	-70.75	501.321	385.933	310.948	153.057	68.7689	57.1365	85.006	139.121	168.545	280.247	348.805	325.023
-12.00	-70.50	511.572	379.504	323.245	201.967	76.3283	71.8725	107.788	132.108	175.866	313.623	405.653	370.511
-12.00	-70.25	523.263	446.534	332.877	196.408	76.9956	72.7985	114.64	140.949	164.425	215.702	284.961	334.896
-12.00	-70.00	551.66	459.921	344.551	181.864	68.6869	79.7518	105.999	102.487	149.679	250.307	336.077	373.823

APPENDIX – II

Weather data for wet period

Date/ Time	T M P (° C)	TMP max (°C)	TMP min (°C)	RH	RH (%)	solar radia- tion watt/ m ²	St. solar radian- MJ/m ² 2/3hr	W ND (Deg)	Rai- ntall (m)	Win spe- d, km/ hr	U2, Win spe- d m/s	Lam- da MJ/ kg	e* k P a	e* m kPa	e* mi kPa	Delt a kPa/ °C	Dbai- r kPa	e*d, point vapor pres- sure, kPa	Epsilon net emis- ivity	Gamma Psycho- metric constan- t	Sn, net shortw- ave radiati- on, MJ/m ² 2/3hr	Ln, Long wave radiatio- n, MJ/m ² 2/3hr	Rn, net radiatio- n, MJ/m ² 2/3hr	Rn, net radiatio- n mm/3hr	Ep, net evapor- ation, mm/3hr
3/1/0 5 0.00	23 .7	24.4	23.7	1	10 0	0	0	21 3.8	0.25	0	0	2.44 504	2. 93	3.0 56	2.93 061	0.17 591	0	2.9306 07375	0.1003 33764	0.067	0	0.5255 96528	0.5255 96528	0.0002 14964	0.0001 55672
3/1/0 5 3.00	23 .7	24	23.7	1	10 0	0	0	21 3.8	0.25	0	0	2.44 504	2. 93	2.9 84	2.93 061	0.17 591	0	2.9306 07375	0.1003 33764	0.067	0	0.5255 96528	0.5255 96528	0.0002 14964	0.0001 55672
3/1/0 5 6.00	25	25.2	23.7	0.9 75	97. 47	64.7	0.0291 15	17 1.6	0.75	0	0	2.44 15	3. 21	3.2 06	2.93 061	0.19 023	0.00 078	3.2049 34976	0.0893 67349	0.067	0.0250 389	0.4776 81854	0.5027 20754	0.0002 05906	0.0010 10393
3/1/0 5 9.00	24 .8	28	24.8	0.6 85	68. 45	193 1333	0.0869 1	14 3.9	5.33	0.26 667	17. 778	2.44 245	3. 13	3.7 8	3.13 024	0.18 632	0.01 09	3.1193 34433	0.0927 37073	0.067	0.0747 426	0.4930 40998	0.5677 83598	0.0002 32485	0.1290 67995
3/1/0 5 12.00	25 .2	25.2	24	0.5 4	53. 98	99.0 3333	0.0445 65	15 6.6	0.75	0.26 667	17. 778	2.44 15	3. 21	3.2 06	2.98 392	0.19 023	0.01 424	3.1914 70937	0.0898 94362	0.067	0.0383 259	0.4804 98813	0.5188 24713	0.0002 12502	0.1656 99621
3/1/0 5 15.00	24 .4	26	24.4	0.5 09	50. 9	110. 7833	0.0498 525	12 9.4	0	0.26 667	17. 778	2.44 339	3. 06	3.3 61	3.05 631	0.18 248	0.01 576	3.0405 57071	0.0958 79295	0.067	0.0428 7315	0.5070 15377	0.5498 86527	0.0002 25051	0.1897 01982
3/1/0 5 18.00	21 .3	24	21.3	0.8 72	87. 22	0	0	26 2.7	3.55	1.06 667	71. 111	2.45 071	2. 53	2.9 84	2.53 32	0.15 489	0.00 353	2.5296 7862	0.1173 30512	0.067	0	0.5949 99709	0.5949 99709	0.0002 42787	0.1809 62279
3/1/0 5 21.00	21 .3	21.3	21	0.9 13	91. 32	0	0	12 1.9	2.02	0	0	2.45 142	2. 49	2.5 33	2.48 701	0.15 242	0.00 218	2.4848 25789	0.1193 13377	0.067	0	0.6025 93446	0.6025 93446	0.0002 45814	0.0030 6685
3/2/0 5 0.00	21 .3	21.3	21	0.9 28	92. 8	0	0	26 4.2	0.5	0	0	2.45 071	2. 53	2.5 33	2.48 701	0.15 489	0.00 181	2.5313 97706	0.1172 54865	0.067	0	0.5946 16094	0.5946 16094	0.0002 4263	0.0025 38173
3/2/0 5 3.00	21 .3	21.3	21	0.9 95	93. 53	0	0	71 27	0	0	0	2.45 142	2. 49	2.5 33	2.48 701	0.15 242	0.00 012	2.4868 88259	0.1192 21808	0.067	0	0.6021 30977	0.6021 30977	0.0002 45625	0.0003 26268
3/2/0 5 6.00	23 .3	23.3	21	0.9 58	95. 75	137. 2333	0.0617 55	11 2.8	0	0.8	53. 333	2.44 599	2. 86	2.8 61	2.48 701	0.17 225	0.00 114	2.8596 84717	0.1032 51567	0.067	0.0531 093	0.5379 72448	0.5910 81748	0.0002 41654	0.0404 75816
3/2/0 5 9.00	25 .6	25.6	24	0.6 71	67. 05	238. 2333	0.1072 05	20 7	0	0.26 667	17. 778	2.44 056	3. 28	3.2 83	2.98 392	0.19 421	0.01 032	3.2724 468	0.0867 41323	0.067	0.0921 963	0.4661 36389	0.5683 32689	0.0002 28773	0.1181 60749
3/2/0 5 12.00	30 .4	30.8	26	0.5 57	55. 7	971. 5667	0.4372 05	14 2.7	0	0.8	53. 333	2.42 923	4. 34	4.4 42	3.36 144	0.24 771	0.01 728	4.3241 06703	0.0488 77189	0.067	0.3759 963	0.2799 48327	0.6559 44627	0.0002 70022	0.4570 08379

Date/ Time	T M P P (° C)	T M P max (°C)	T M P min (°C)	RH	RH (%)	solar radia tion watt/ m ²	St. solar radian MJ/m ² 2/3hr	W ND (D deg)	Rai nfall (m)	Win d spe ed, km/ hr	U2, Win d spe ed m/s	Lam da MJ/ kg	e ^t k P a	e ^m ax, kPa	e ^m n, kPa	Delt a kPa/ °C	Db a f, kPa	e ^d , dew point vapor pressur e, kPa	Epsilon net emissi vity	Gamma Psycho metric constan t	Sh, net shortw ave radiati on, MJ/m ² 2/3hr	Ln, Long wave radiatio n, MJ/m ² 2/3hr	Rn, net radiatio n, MJ/m ² 2/3hr	Rn, net radiatio n mm/3hr	Ep, net evapor ation, mm/3hr
3/2/0 5 15.00	26	29.9	26	0.5 66	57	271. 5667	0.1222 05	10 6.2	0	0.53 333	35. 556	2.43 961	3. 36	4.2 19	3.36 144	0.19 826	0.01 646	3.3449 781	0.0839 50062	0.067	0.1050 963	0.4535 571	0.5586 534	0.0002 28993	0.3525 69759
3/2/0 5 18.00	23 .7	24.4	23.7	0.7 74	38	0	0	13 3.1	0	0	0	2.44 504	3.0 56	2.93 061	0.17 591	0.00 677	0.00 677	2.9238 37166	0.1006 1076	0.067	0	0.5270 47563	0.5270 47563	0.0002 15557	0.0081 30207
3/2/0 5 21.00	22 .5	23.3	22.5	0.9 78	75	0	0	13 5	0	0	0	2.44 786	2.8 61	2.72 559	0.16 512	0.00 063	0.00 063	2.7249 59136	0.1088 95697	0.067	0	0.5612 81343	0.5612 81343	0.0002 29293	0.0009 43573
3/3/0 5 3.00	22 .1	22.5	22.1	0.9 97	67	0	0	13 5	0	0	0	2.44 882	2.7 26	2.66 009	0.16 165	0.05 05	0.05 05	2.6599 99574	0.1116 66928	0.067	0	0.5724 57104	0.5724 57104	0.0002 33768	0.0002 78748
3/3/0 5 6.00	21 .7	22.5	21.7	1	0	0	0	13 9.7	0	0	0	2.44 977	2.7 26	2.59 597	0.15 824	0	0	2.5859 69994	0.1144 31802	0.067	0	0.5834 59102	0.5834 59102	0.0002 38169	0.0001 67323
3/3/0 5 9.00	29 .5	29.5	21.7	0.9 47	72	294. 45	0.1323 45	18 5.9	0	0.8	53. 333	2.43 135	4.1 23	4.1 23	2.59 597	0.23 684	0.00 177	4.1211 10572	0.0557 92739	0.067	0.1138 167	0.3157 85335	0.4296 02035	0.0001 76693	0.0487 30623
3/3/0 5 12.00	32 .2	33.2	30.4	0.6 35	53	720. 5833	0.3242 625	21 4.2	0	0.8	53. 333	2.42 356	4. 97	5.0 87	4.34 139	0.27 879	0.01 719	4.9568 01162	0.0283 05754	0.067	0.2788 6575	0.1673 11206	0.4461 76956	0.0001 841	0.4148 64013
3/3/0 5 15.00	33 .2	34.1	32.8	0.5 18	77	700. 9833	0.3154 425	12 1.4	0	1.6	106 67	2.42 261	5. 09	5.3 49	4.97 399	0.28 427	0.02 49	5.0619 57649	0.0250 16874	0.067	0.2712 8055	0.1486 45809	0.4199 26359	0.0001 73336	1.1636 52124
3/3/0 5 18.00	26 .8	33.2	26.8	0.4 95	5	262. 75	0.1182 375	12 9.6	0	0.53 333	35. 556	2.43 773	3. 52	5.0 87	3.52 372	0.20 658	0.02 174	3.5019 77897	0.0780 09987	0.067	0.1016 8425	0.4259 90405	0.5276 74655	0.0002 16462	0.4503 06557
3/4/0 5 21.00	23 .7	25.6	23.7	0.8 45	5	0	0	18 9.4	0	0	0	2.44 504	2. 93	2.93 061	0.17 591	0.00 482	0.00 482	2.9257 92006	0.1005 30747	0.067	0	0.5266 28417	0.5266 28417	0.0002 15386	0.0058 27628
3/3/0 5 3.00	22 .9	23.3	22.9	0.9 65	53	0	0	27 4.2	0	0	0	2.44 693	2.8 61	2.79 249	0.16 865	0.08 098	0.08 098	2.7915 09859	0.1060 9063	0.067	0	0.5497 87993	0.5497 87993	0.0002 24685	0.0013 56277
3/4/0 5 6.00	22 .5	22.9	22.5	0.9 96	62	0	0	27 4.2	0	0	0	2.44 788	2. 92	2.72 559	0.16 512	0.00 011	0.00 011	2.7254 81843	0.1088 73532	0.067	0	0.5611 67101	0.5611 67101	0.0002 29246	0.0002 94417
3/4/0 5 9.00	22 .9	22.9	22.1	1	0	0	0	26 6.5	0	0	0	2.44 788	2. 92	2.66 009	0.16 512	0	0	2.7255 87607	0.1088 69048	0.067	0	0.5611 43987	0.5611 43987	0.0002 29237	0.0001 63069
3/4/0 5 12.00	29 .1	29.1	22.5	0.9 51	07	310. 375	0.1398 375	21 8.9	0	0.26 667	17. 778	2.43 229	4. 03	4.0 29	2.72 559	0.23 213	0.00 167	4.0272 1832	0.0590 48974	0.067	0.1202 6025	0.3324 52448	0.4527 12698	0.0001 86126	0.0166 36593
3/4/0 5 15.00	33 .6	33.6	31.2	0.6 16	55	926. 4833	0.4169 175	18 2.3	0	0.26 667	17. 778	2.42 167	5. 02	5.2 46	4.54 4	0.28 984	0.01 874	5.1831 93906	0.0212 67196	0.067	0.3585 4905	0.1270 27058	0.4855 76108	0.0002 00513	0.1563 39592
3/4/0 5 18.00	35 .3	35.3	34.5	0.5 21	05	912. 375	0.4107 375	22 9.5	0	1.06 667	71. 111	2.41 766	5. 72	5.7 915	0.31 456	0.02 682	0.02 682	5.6897 67183	0.0060 5474	0.067	0.3532 3425	0.0369 72665	0.3902 06915	0.0001 61389	0.7812 95995
3/4/0 5 21.00	27 .2	34.5	27.2	0.6 28	77	275. 5	0.1239 75	21 1.6	0	0	0	2.43 678	3. 61	3.60 739	0.21 084	0.01 69	0.01 69	3.5904 90821	0.0747 19733	0.067	0.1066 185	0.4102 0374	0.5168 2224	0.0002 12092	0.0173 17119

Date/ Time	T M P (°C)	TMP max (°C)	TMP min (°C)	RH	RH (%)	solar radia- tion watt/ m ²	St. solar radian- MJ/m ² 2/3hr	W ND (D deg)	Rai- ntail (m)	Win- d spe- d. km/ hr	U2 Win- d spe- d. m/s sec	Lam- da MJ/ kg	e ^t k P a	e ^m ax kPa	e ^m n kPa	Delt a kPa/ °C	Db a f. kPa	e ^d dew point vapor pressur- e, kPa	Epsilon net emissi- vity	Gamma Psycho- metric constan- t	Sh, net shortw- ave radiati- on, MJ/m ² 2/3hr	Ln, Long wave radiatio- n, MJ/m ² 2/3hr	Rn, net radiatio- n, MJ/m ² 2/3hr	Rn, net radiatio- n mm/3hr	Ep, net evapor- ation, mm/3hr	
3/4/0 5 18:00	24	26	24	0.9 74 35	0	0	0	8.4	0	0	0	2.44 434	2.44 98	3.3 61	2.98 392	0.17 87	0.00 084	2.9830 76717	0.0981 97801	0.067	0	0.5164 8959	0.5164 8959	0.0002 11301	0.0002 11301	0.0011 31087
3/4/0 5 21:00	23	23.7	23.3	0.9 99 92	0	0	0	8.4	0	0	0	2.44 599	2.44 86	2.9 31	2.86 082	0.17 225	2.4E -05	2.8607 96999	0.1032 0553	0.067	0	0.5377 32579	0.5377 32579	0.0002 19843	0.0002 19843	0.0001 87202
3/5/0 5 0:00	22	23.3	22.9	1 10	0	0	0	8.4	0	0	0	2.44 693	2.44 79	2.8 61	2.79 249	0.16 865	0	2.7924 89766	0.1080 49579	0.067	0	0.5495 75255	0.5495 75255	0.0002 24598	0.0002 24598	0.0001 60741
3/5/0 5 3:00	21	22.5	21.7	0.9 99 92	0	0	0	8.4	0	0	0	2.44 977	2.44 6	2.7 26	2.59 597	0.15 824	2.2E -05	2.5959 47821	0.1144 32765	0.067	0	0.5834 64014	0.5834 64014	0.0002 38171	0.0002 38171	0.0001 95866
3/5/0 5 6:00	30	30.4	22.1	0.9 69 9	0	0	0	93	0	0	0	2.42 923	4.4 34	4.3 41	2.66 009	0.24 771	0.00 109	4.3403 05408	0.0483 32405	0.067	0.1172 352	0.2768 28032	0.3840 63232	0.0001 62218	0.0010 97087	
3/5/0 5 9:00	33	33.2	31.2	0.8 16 6	0	0	0	23	0	0.26 667	17. 778	2.42 261	5.0 87	4.54 4	0.28 427	0.00 886	0.00 886	5.0779 92759	0.0245 18371	0.067	0.3509 574	0.1456 83797	0.4966 41197	0.0002 05002	0.0751 14109	
3/5/0 5 12:00	34	34.5	33.2	0.7 5 97	0	0	0	15	0	1.06 667	71. 111	2.41 955	5.4 69	5.08 685	0.30 272	0.01 321	0.01 321	5.4559 33311	0.0129 88849	0.067	0.3281 8245	0.0784 95587	0.4066 78037	0.0001 6808	0.3961 43916	
3/5/0 5 15:00	27	33.6	27.2	0.7 23 27	0	0	0	31	0	0.26 667	17. 778	2.43 678	5.2 02	3.60 739	0.21 084	0.01 222	0.01 222	3.5951 72714	0.0745 46831	0.067	0.0796 833	0.4092 54523	0.4889 37823	0.0002 00649	0.1307 37881	
3/5/0 5 18:00	25	26.4	25.2	0.8 5	0	0	0	32	0	0	0	2.44 15	3.4 21	3.2 42	3.20 571	0.19 023	0.00 499	3.2007 26649	0.0895 31953	0.067	0	0.4785 61687	0.4785 61687	0.0001 96011	0.0001 96011	0.0056 49154
3/5/0 5 21:00	24	25.2	24.8	0.9 65 5	0	0	0	32	0	0	0	2.44 245	3.2 13	3.13 024	0.18 632	0.00 111	0.00 111	3.1291 26429	0.0923 49282	0.067	0	0.4909 79288	0.4909 79288	0.0002 01019	0.0002 01019	0.0013 9309
3/6/0 5 0:00	24	24.8	24.8	0.9 99 92	0	0	0	32	0	0	0	2.44 245	3.1 3	3.13 024	0.18 632	2.6E -05	2.6E -05	3.1302 09134	0.0923 06441	0.067	0	0.4907 51522	0.4907 51522	0.0002 00926	0.0002 00926	0.0001 77079
3/6/0 5 3:00	24	24.8	24	1 10	0	0	0	32	0	0	0	2.44 434	2.44 98	3.1 3	2.98 392	0.17 87	0	2.9839 17477	0.0981 63728	0.067	0	0.5163 10378	0.5163 10378	0.0002 11227	0.0002 11227	0.0001 53628
3/6/0 5 6:00	28	28	24	0.9 99 92	0	0	0	30	0	0	0	2.43 489	3.7 8	3.7 8	2.98 392	0.21 96	2.8E -05	3.7799 02181	0.0678 12413	0.067	0.0512 13	0.3762 64857	0.4274 77857	0.0001 75563	0.0001 75563	0.0001 62214
3/6/0 5 9:00	33	33.2	29.1	0.7 49 87	0	0	0	12	0	1.06 667	71. 111	2.42 261	5.0 87	4.02 888	0.28 427	0.01 146	0.01 146	5.0753 97698	0.0245 98994	0.067	0.2378 889	0.1461 6284	0.3840 5174	0.0001 56528	0.3601 159	
3/6/0 5 12:00	30	32.4	29.9	0.6 11 13	0	0	0	13	0	1.33 333	88. 889	2.42 923	4.8 63	4.21 879	0.24 771	0.01 765	0.01 765	4.3237 41091	0.0488 89496	0.067	0.1897 1385	0.2800 18821	0.4697 32671	0.0001 93367	0.7670 72596	
3/6/0 5 15:00	27	30.4	27.6	0.6 49 9	0	0	0	13	0	1.06 667	71. 111	2.43 584	4.3 41	3.69 278	0.21 518	0.01 41	0.01 41	3.6786 81987	0.0714 81533	0.067	0.0868 8795	0.3945 20685	0.4814 08635	0.0001 97636	0.3510 09231	
3/6/0 5 18:00	24	26.8	24	0.9 39 93	0	0	0	80	0	0	0	2.44 434	2.44 98	3.5 24	2.98 392	0.17 87	0.00 197	2.9819 43494	0.0992 43733	0.067	0	0.5167 31182	0.5167 31182	0.0002 11399	0.0002 11399	0.0024 48562

Date/Time	TMP P (°C)	TMP max (°C)	TMP min (°C)	RH	RH (%)	solar radiation wati/m ²	St. solar radiation MJ/m ² /3hr	W ND (Deg)	Rai nfall (m)	Win d spe ed km/hr	U2 Win d spe ed m/sec	Lam da MJ/kg	e ^k P a	e ^m ax kPa	e ^m n kPa	Delt a kPa/°C	Db a kPa	e ^d point pressur e, kPa	Epsilon net emmisi vity	Gamma Psychro metric constan t	Sh, net shortw ave radiati on, MJ/m ² /3hr	Ln, Long wave radiatio n, MJ/m ² /3hr	Rn, net radiatio n, MJ/m ² /3hr	Rn, net radiatio n, mm/3hr	Ep, net evapor ation, mm/3hr
3/6/0 5	22.9	23.7	22.9	0.99	92	0	0	80.2	0	0	0	2.44	2.44	2.9	2.79	0.16	2.4E-05	2.7924	0.1060	0.067	0	0.5495	0.5495	0.0002	0.0001
21.00	22.5	22.5	22.1	1	10	0	0	80.2	0	0	0	2.44	2.44	2.7	2.66	0.16	0	2.6600	0.1116	0.067	0	0.5724	0.5724	0.0002	0.0001
3/7/0 5	22.1	22.1	21.7	1	10	0	0	75.5	0	0	0	2.44	2.44	2.6	2.59	0.15	0	2.5859	0.1144	0.067	0	0.5834	0.5834	0.0002	0.0001
3/7/0 3.00	29.5	21.7	21.7	0.99	94	0	0	80.2	0	0.53	35.556	2.43	2.43	4.1	2.59	0.23	0.00	4.1226	0.0557	0.067	0.0865	0.3154	0.4019	0.0001	0.0040
3/7/0 5	30.8	28	28	0.8	83	23	4	4.9	0	2.13	142.22	2.42	2.42	4.4	3.77	0.25	0.00	4.4351	0.0451	0.067	0.3376	0.2600	0.5977	0.0002	0.4474
3/7/0 9.00	32.4	31.2	31.2	0.6	66	14	4	8.1	0	1.86	124.44	2.42	2.42	4.8	4.54	0.26	0.01	4.6326	0.0386	0.067	0.3479	0.2250	0.5729	0.0002	0.9092
3/7/0 5	29.5	27.2	27.2	0.6	66	13	9	8.1	1.02	0.53	35.556	2.43	2.43	4.1	3.60	0.21	0.01	3.5943	0.0745	0.067	0.0432	0.4094	0.4526	0.0001	0.2651
3/7/0 15.00	26	24	24	0.9	91	0	0	9.4	0	0	0	2.44	2.44	3.3	2.98	0.17	0.00	2.9811	0.0982	0.067	0	0.5168	0.5168	0.0002	0.0033
3/7/0 18.00	24	24	23.7	0.9	97	0	0	9.4	0	0	0	2.44	2.44	2.9	2.93	0.17	9.9E-05	2.9838	0.0981	0.067	0	0.5163	0.5163	0.0002	0.0002
21.00	23.7	24	23.7	0.8	82	0	0	21	0	0	0	2.44	2.44	2.9	2.93	0.17	0.00	2.9255	0.1005	0.067	0	0.5266	0.5266	0.0002	0.0061
3/8/0 5	23.3	23.7	23.3	0.7	78	0	0	9.4	0	0	0	2.44	2.44	2.9	2.86	0.17	0.00	2.8544	0.1034	0.067	0	0.5390	0.5390	0.0002	0.0077
3/8/0 3.00	28.3	23.3	23.3	0.7	70	12	5	7.8	0	0.53	35.556	2.43	2.43	3.8	2.86	0.21	0.01	3.6827	0.0713	0.067	0.0641	0.3937	0.4578	0.0001	0.2015
3/8/0 6.00	31.2	27.6	27.6	0.5	52	19	6	8.1	0	2.13	142.22	2.42	2.42	4.5	3.69	0.25	0.01	4.5245	0.0422	0.067	0.2492	0.2443	0.4935	0.0002	1.3022
3/8/0 9.00	29.5	29.5	29.5	0.4	47	19	6	3.6	0	1.86	124.44	2.43	2.43	4.8	4.12	0.23	0.02	4.0994	0.0565	0.067	0.3202	0.3200	0.6402	0.0002	1.4667
12.00	26.4	29.1	26.4	0.4	49	88	35	35	7.87	1.33	88.889	2.43	2.43	4.0	3.44	0.20	0.01	3.5046	0.0779	0.067	0.0781	0.4254	0.5035	0.0002	0.9557
3/8/0 15.00	23.7	25.6	23.7	0.8	83	0	0	13	0	0	0	2.44	2.44	3.2	2.93	0.17	0.00	2.9253	0.1005	0.067	0	0.5267	0.5267	0.0002	0.0062
3/8/0 18.00	23.3	23.7	23.3	0.9	98	0	0	14	0	0	0	2.44	2.44	2.9	2.86	0.17	0.00	2.9300	0.1003	0.067	0	0.5257	0.5257	0.0002	0.0008
21.00	23.7	23.7	23.3	0.8	81	6.3	0	6.3	0	0	0	2.44	2.44	2.9	2.82	0.17	0.00	2.9300	0.1003	0.067	0	0.5257	0.5257	0.0002	0.0008
3/9/0 5	22.5	23.7	22.5	0.9	95	0	0	14	0	0	0	2.44	2.44	2.9	2.72	0.16	0.00	2.7243	0.1089	0.067	0	0.5614	0.5614	0.0002	0.0017

3/11	25	25	22	0.9	98.	115.6	0.0520	39.	0	0	0	2.44	3.	3.2	2.79	0.19	0.00	3.28246	0.08635	0.0	0.0447	0.46405	0.50882	0.00020	0.00049
/05	.6	.6	.9	9	98	833	575	37	0	0	0	056	28	83	249	421	031	2344	4082	67	6945	5297	4747	8487	0219
6.00	28	29	26	0.6	66.	342.1	0.1539	19	0	0	0	2.43	3.	4.0	3.36	0.21	0.01	3.76768	0.08825	0.0	0.1324	0.37870	0.51112	0.00020	0.01219
/05	.1	.1	.1	69	85	667	75	0.3	0	0	0	489	78	29	144	96	225	0902	2791	67	185	8346	6846	9918	7699
9.00	29	30	26	0.4	47.	375.4	0.1689	93	0	0	0	2.43	4.	4.3	3.52	0.24	0.02	4.19809	0.05315	0.0	0.1453	0.30242	0.44773	0.00018	0.01899
/05	.9	.4	.8	74	38	833	675	03	0	0	0	041	22	41	372	162	069	6602	0399	67	1205	3036	5086	4222	2071
12.0	0	23	29	0.5	51.	79.4	0.0357	19	16.	0.53	35.5	2.44	2.	4.2	2.93	0.17	0.01	2.91311	0.10105	0.0	0.0307	0.52934	0.56007	0.00022	0.41341
/05	.7	.9	.7	11	07	0	3	0.6	76	333	56	504	93	19	061	591	749	5186	0094	67	278	9007	6807	9066	0147
15.0	0	23	23	0.8	84.	0	0	24	0.2	0	0	2.44	2.	2.9	2.86	0.17	0.00	2.85644	0.10338	0.0	0	0.53867	0.53867	0.00022	0.00539
/05	.3	.7	.3	49	9	0	0	3.3	5	0	0	599	86	31	082	225	437	8601	5561	67	0	0599	0599	0226	9687
18.0	0	23	23	0.9	95.	0	0	24	0	0	0	2.44	2.	2.9	2.86	0.17	0.00	2.92921	0.10039	0.0	0	0.52589	0.52589	0.00021	0.00179
/05	.7	.7	.3	52	18	0	0	3.3	0	0	0	504	93	31	082	591	139	2606	0803	67	0	5327	5327	5086	8551
21.0	23	23	23	0.9	98.	0	0	24	0	0	0	2.44	2.	2.9	2.86	0.17	0.00	2.93025	0.10034	0.0	0	0.52567	0.52567	0.00021	0.00057
/05	.7	.7	.3	88	78	0	0	24	0	0	0	504	93	31	082	591	035	5063	8171	67	0	1997	1997	4995	0656
0.00	23	23	23	0.6	66.	134.3	0.0604	15	6.1	0.26	17.7	2.43	3.	3.7	3.36	0.21	0.01	3.76814	0.06823	0.0	0.0519	0.37861	0.43059	0.00017	0.12210
/05	.7	.7	.7	97	65	5	375	2.5	0	667	78	489	78	8	144	96	179	1152	6193	67	741	6253	0353	6942	8395
0.00	27	30	27	0.8	80.	449.0	0.2020	96.	1.0	0.8	53.3	2.43	4.	4.3	3.60	0.21	0.00	3.59667	0.07438	0.0	0.1737	0.40834	0.58211	0.00023	0.22179
/05	.2	.4	.2	06	6	167	575	33	2	0	0	678	61	41	739	084	771	7987	0557	67	6945	1698	1148	8885	6233
6.00	28	28	26	0.6	66.	134.3	0.0604	15	6.1	0.26	17.7	2.43	3.	3.7	3.36	0.21	0.01	3.76814	0.06823	0.0	0.0519	0.37861	0.43059	0.00017	0.12210
/05	.7	.7	.7	97	65	5	375	2.5	0	667	78	489	78	8	144	96	179	1152	6193	67	741	6253	0353	6942	8395
9.00	27	30	27	0.8	80.	449.0	0.2020	96.	1.0	0.8	53.3	2.43	4.	4.3	3.60	0.21	0.00	3.59667	0.07438	0.0	0.1737	0.40834	0.58211	0.00023	0.22179
/05	.2	.4	.2	06	6	167	575	33	2	0	0	678	61	41	739	084	771	7987	0557	67	6945	1698	1148	8885	6233
12.0	28	28	26	0.6	66.	134.3	0.0604	15	6.1	0.26	17.7	2.43	3.	3.7	3.36	0.21	0.01	3.76814	0.06823	0.0	0.0519	0.37861	0.43059	0.00017	0.12210
/05	.7	.7	.7	97	65	5	375	2.5	0	667	78	489	78	8	144	96	179	1152	6193	67	741	6253	0353	6942	8395
15.0	27	30	27	0.8	80.	449.0	0.2020	96.	1.0	0.8	53.3	2.43	4.	4.3	3.60	0.21	0.00	3.59667	0.07438	0.0	0.1737	0.40834	0.58211	0.00023	0.22179
/05	.2	.4	.2	06	6	167	575	33	2	0	0	678	61	41	739	084	771	7987	0557	67	6945	1698	1148	8885	6233
18.0	28	28	26	0.6	66.	134.3	0.0604	15	6.1	0.26	17.7	2.43	3.	3.7	3.36	0.21	0.01	3.76814	0.06823	0.0	0.0519	0.37861	0.43059	0.00017	0.12210
/05	.7	.7	.7	97	65	5	375	2.5	0	667	78	489	78	8	144	96	179	1152	6193	67	741	6253	0353	6942	8395
0	27	30	27	0.8	80.	449.0	0.2020	96.	1.0	0.8	53.3	2.43	4.	4.3	3.60	0.21	0.00	3.59667	0.07438	0.0	0.1737	0.40834	0.58211	0.00023	0.22179
/05	.2	.4	.2	06	6	167	575	33	2	0	0	678	61	41	739	084	771	7987	0557	67	6945	1698	1148	8885	6233
15.0	28	28	26	0.6	66.	134.3	0.0604	15	6.1	0.26	17.7	2.43	3.	3.7	3.36	0.21	0.01	3.76814	0.06823	0.0	0.0519	0.37861	0.43059	0.00017	0.12210
/05	.7	.7	.7	97	65	5	375	2.5	0	667	78	489	78	8	144	96	179	1152	6193	67	741	6253	0353	6942	8395
12.0	27	30	27	0.8	80.	449.0	0.2020	96.	1.0	0.8	53.3	2.43	4.	4.3	3.60	0.21	0.00	3.59667	0.07438	0.0	0.1737	0.40834	0.58211	0.00023	0.22179
/05	.2	.4	.2	06	6	167	575	33	2	0	0	678	61	41	739	084	771	7987	0557	67	6945	1698	1148	8885	6233
15.0	28	28	26	0.6	66.	134.3	0.0604	15	6.1	0.26	17.7	2.43	3.	3.7	3.36	0.21	0.01	3.76814	0.06823	0.0	0.0519	0.37861	0.43059	0.00017	0.12210
/05	.7	.7	.7	97	65	5	375	2.5	0	667	78	489	78	8	144	96	179	1152	6193	67	741	6253	0353	6942	8395
0	27	30	27	0.8	80.	449.0	0.2020	96.	1.0	0.8	53.3	2.43	4.	4.3	3.60	0.21	0.00	3.59667	0.07438	0.0	0.1737	0.40834	0.58211	0.00023	0.22179
/05	.2	.4	.2	06	6	167	575	33	2	0	0	678	61	41	739	084	771	7987	0557	67	6945	1698	1148	8885	6233
15.0	28	28	26	0.6	66.	134.3	0.0604	15	6.1	0.26	17.7	2.43	3.	3.7	3.36	0.21	0.01	3.76814	0.06823	0.0	0.0519	0.37861	0.43059	0.00017	0.12210
/05	.7	.7	.7	97	65	5	375	2.5	0	667	78	489	78	8	144	96	179	1152	6193	67	741	6253	0353	6942	8395
0	27	30	27	0.8	80.	449.0	0.2020	96.	1.0	0.8	53.3	2.43	4.	4.3	3.60	0.21	0.00	3.59667	0.07438	0.0	0.1737	0.40834	0.58211	0.00023	0.22179
/05	.2	.4	.2	06	6	167	575	33	2	0	0	678	61	41	739	084	771	7987	0557	67	6945	1698	1148	8885	6233
15.0	28	28	26	0.6	66.	134.3	0.0604	15	6.1	0.26	17.7	2.43	3.	3.7	3.36	0.21	0.01	3.76814	0.06823	0.0	0.0519	0.37861	0.43059	0.00017	0.12210
/05	.7	.7	.7	97	65	5	375	2.5	0	667	78	489	78	8	144	96	179	1152	6193	67	741	6253	0353	6942	8395
0	27	30	27	0.8	80.	449.0	0.2020	96.	1.0	0.8	53.3	2.43	4.	4.3	3.60	0.21	0.00	3.59667	0.07438	0.0	0.1737	0.40834	0.58211	0.00023	0.22179
/05	.2	.4	.2	06	6	167	575	33	2	0	0	678	61	41	739	084	771	7987	0557	67	6945	1698	1148	8885	6233
15.0	28	28	26	0.6	66.	134.3	0.0604	15	6.1	0.26	17.7	2.43	3.	3.7	3.36	0.21	0.01	3.76814	0.06823	0.0	0.0519	0.37861	0.43059	0.00017	0.12210
/05	.7	.7	.7	97	65	5	375	2.5	0	667	78	489	78	8	144	96	179	1152	6193	67	741	6253	0353	6942	8395
0	27	30	27	0.8	80.	449.0	0.2020	96.	1.0	0.8	53.3	2.43	4.	4.3	3.60	0.21	0.00	3.59667	0.07438	0.0	0.1737	0.40834	0.58211	0.00023	0.22179
/05	.2	.4	.2	06	6	167	575	33	2	0	0	678	61	41	739	084	771	7987	0557	67	6945	1698	1148	8885	6233
15.0	28	28	26	0.6	66.	134.3	0.0604	15	6.1	0.26	17.7	2.43	3.	3.7	3.36	0.21	0.01	3.76814	0.06823	0.0	0.0519	0.37861	0.43059	0.00017	0.12210
/05	.7	.7	.7	97	65	5	375	2.5	0	667	78	489	78	8	144	96	179	1152	6193	67	741	6253	0353	6942	8395
0	27	30	27	0.8	80.	449.0	0.2020	96.	1.0	0.8	53.3	2.43	4.	4.3	3.60	0.21	0.00	3.59667	0.07438	0.0	0.1737	0.40834	0.58211	0.00023	0.22179
/05	.2	.4	.2	06	6	167	575	33	2	0	0	678	61	41	739	084	771	7987	0557	67	6945	1698	1148	8885	6233
15.0	28	28	26	0.6	66.	134.3	0.0604	15	6.1	0.26	17.7	2.43	3.	3.7	3.36	0.21	0.01	3.76814	0.06823	0.0	0.0519	0.37861	0.43059	0.00017	0.12210
/05	.7	.7	.7	97	65	5	375	2.5	0	667	78	489	78	8	144	96	179	1152	6193	67	741	6253	0353	6942	8395
0	27	30																							

Date/Time	T M P (°C)	TMP max (°C)	TMP min (°C)	RH	RH (%)	solar radia tion watt/ m ²	St. solar radian MJ/m ² 2/3hr	W ND (D deg)	Rai nfall (m)	Win d spe ed km/ hr	U2. Win d spe ed m/s	Lam da MJ/ kg	e ^t k P a	e ^m ax kPa	e ^{mi} n kPa	Delt a kPa/ °C	Db a f kPa	e ^d dew point vapor pressur e, kPa	Epsilon net emissi vity	Gamma Psycho metric constan t	Sh, net shortw ave radiati on, MJ/m ² 2/3hr	Ln, Long wave radiatio n, MJ/m ² 2/3hr	Rn, net radiatio n, MJ/m ² 2/3hr	Rn, net radiatio n mm/3hr	Ep, net evapor ation, mm/3hr
3/13/ 05 12:00	32.8	32.8	30.8	0.65	64.98	742.15	0.3339 675	23 5.8	0	2.66 667	177 78	2.42 356	4.97 74	4.97 74	4.44 169	0.27 879	0.01 649	4.9575 06702	0.0282 83572	0.067	0.2872 1205	0.1671 80091	0.4543 92141	0.0001 8749	1.2844 3717
3/13/ 05 15:00	26.8	32.8	26.8	0.61	61.42	236.2667	0.1063 2	23 1.1	0	0.8	53. 333	2.43 773	3.52 74	3.52 74	3.52 372	0.20 658	0.01 639	3.5073 26091	0.0778 10009	0.067	0.0914 352	0.4248 98381	0.5163 33581	0.0002 1181	0.5008 19069
3/13/ 05 18:00	24	25.6	24	0.91	91.33	0	0	15 1.9	0	0	0	2.44 434	2.98 392	2.98 392	0.17 87	0.00 272	2.9812 01912	0.0982 73796	0.067	0	0.5168 89304	0.5168 89304	0.0002 11464	0.0033 10718	
3/13/ 05 21:00	24	24	23.7	0.99	99.4	0	0	15 1.9	0	0	0	2.44 434	2.93 392	2.93 392	0.17 87	0.00 018	2.9837 40041	0.0981 70918	0.067	0	0.5163 48197	0.5163 48197	0.0002 11243	0.0003 59913	
3/14/ 05 0:00	22	23.7	22.9	1	10	0	0	15 1.9	0	0	0	2.44 693	2.79 31	2.79 31	0.16 865	0	2.7924 89766	0.1060 49579	0.067	0	0.5495 75255	0.5495 75255	0.0002 24598	0.0001 60741	
3/14/ 05 3:00	22	22.5	22.1	1	10	0	0	15 1.9	0	0	0	2.44 882	2.7 26	2.7 26	0.16 165	0	2.6600 89335	0.1116 63076	0.067	0	0.5724 37354	0.5724 37354	0.0002 3376	0.0001 65263	
3/14/ 05 6:00	25	25.6	22.5	0.98	87	88.2	0.0397 125	11 1.6	0	0	0	2.44 056	2.72 83	2.72 83	0.19 421	0.00 039	3.2823 85633	0.0863 57026	0.067	0.0341 5275	0.4640 71224	0.4882 23974	0.0002 04143	0.0005 70254	
3/14/ 05 9:00	28	28	26	0.66	69.32	224.5	0.1010 25	21 0	0	0.26 667	17. 778	2.43 489	3.36 8	3.36 8	0.21 96	0.01 096	3.7689 74312	0.0682 06151	0.067	0.0868 815	0.3784 49558	0.4653 31058	0.0001 9111	0.1134 98334	
3/14/ 05 12:00	21	26.8	21	0.50	50.17	100	0.045	15 4.9	4.32	2.13 333	142 22	2.45 142	2.48 701	2.48 701	0.15 242	0.01 498	2.4720 28674	0.1198 8239	0.067	0.0387 67253	0.6054 67253	0.6441 67253	0.0002 62773	1.5370 74988	
3/14/ 05 15:00	21	21.3	21	0.53	53.45	76.4	0.0344 1	23 6.3	0	1.33 333	88. 889	2.45 071	2.5 33	2.5 33	0.15 489	0.01 168	2.5215 20442	0.1176 89855	0.067	0.0295 926	0.5968 21988	0.6264 14588	0.0002 55605	0.7451 67225	
3/14/ 05 18:00	21	21	21	0.87	74.42	0	0	81. 32	0	0	0	2.45 142	2.48 701	2.48 701	0.15 242	0.00 313	2.4838 75915	0.1193 55562	0.067	0	0.6028 06501	0.6028 06501	0.0002 45901	0.0043 29029	
3/14/ 05 21:00	21	21	20.6	0.98	82.15	0	0	20. 65	0.76	0	0	2.45 142	2.42 87	2.42 87	0.15 242	0.00 045	2.4865 50893	0.1192 36784	0.067	0	0.6022 06611	0.6022 06611	0.0002 45656	0.0007 74555	
3/15/ 05 0:00	20	21	20.6	0.99	99.65	0	0	16. 9	1.27	0	0	2.45 236	2.42 87	2.42 87	0.14 918	8.6E -05	2.4264 66325	0.1219 20336	0.067	0	0.6124 17944	0.6124 17944	0.0002 49726	0.0002 88692	
3/15/ 05 3:00	19	20.2	19.8	0.96	61.08	0	0	17 8.4	2.79	0	0	2.45 425	2.3 67	2.3 67	0.14 287	0.00 092	2.3085 72361	0.1272 84184	0.067	0	0.6324 25709	0.6324 25709	0.0002 57686	0.0014 61522	
3/15/ 05 6:00	22	22.5	19.8	0.9	61.12	117.	0.0529 425	22 2.4	0	0	0	2.44 788	2.7 949	2.7 949	0.16 512	0.00 098	2.7246 09963	0.1089 10504	0.067	0.0455 3055	0.5613 57664	0.6068 88214	0.0002 47924	0.0013 90445	
3/15/ 05 9:00	28	28	22.5	0.74	74.41	531. 3833	0.2391 225	17 3.9	0	1.06 667	71. 111	2.43 489	2.72 8	2.72 8	0.21 96	0.00 841	3.7715 16561	0.0681 14501	0.067	0.2056 4535	0.3779 41029	0.5835 86379	0.0002 39676	0.3235 82045	
3/15/ 05 12:00	28	28.3	27.6	0.56	56.63	543. 1333	0.2444 1	13 9.9	0	0.8	53. 333	2.43 418	3.8 46	3.8 46	0.22 296	0.01 649	3.8299 7556	0.0660 15473	0.067	0.2101 926	0.3677 55856	0.5779 48456	0.0002 3743	0.4736 91174	
3/15/ 15:00	24	28.3	24.8	0.4	49.95	130.	0.0586 8	13 1.5	0	0.53 333	35. 556	2.44 245	3.8 13	3.8 46	0.18 632	0.01 763	3.1126 01619	0.0930 04085	0.067	0.0504 648	0.4944 60474	0.5449 25274	0.0002 23106	0.3973 79707	

Date/Time	TMP P (°C)	TMP max (°C)	TMP min (°C)	RH (%)	RH (%)	solar radiation watt/m ²	St. solar radiation MJ/m ² /3hr	W ND (Deg)	Rainfall (mm)	Wind speed km/hr	U2 Wind speed m/sec	Lambda MJ/kg	Lat P a	e* m ax kPa	e* m n kPa	Delta a kPa/°C	Dbat kPa	e'd. point pressure, kPa	Epsilon net emissivity	Gamma Psychrometric constant	Sh. net shortwave radiation, MJ/m ² /3hr	Ln. Long wave radiation, MJ/m ² /3hr	Rn. net radiation MJ/m ² /3hr	Rn. net radiation mm/3hr	Ep. net evaporation, mm/3hr
3/15/18:00	23.7	24.8	23.7	86.67	72	0	0	18.04	0	0	0	2.44504	2.93061	3.103	0.17591	0.00403	2.926581965	0.100498421	0.067	0	0.526459078	0.526459078	0.000215317	0.004897146	
3/15/21:00	22.9	23.3	22.9	96.61	13	0	0	20.95	0	0	0	2.44693	2.79249	2.861	0.16865	0.00109	2.791396793	0.106095367	0.067	0	0.549812542	0.549812542	0.000224695	0.001494223	
3/16/0:00	22.9	22.9	22.9	99.96	62	0	0	20.95	0	0	0	2.44693	2.79249	2.792	0.16865	0.00109	2.792382721	0.106054063	0.067	0	0.549598493	0.549598493	0.000224607	0.000291342	
3/16/3:00	22.9	22.9	22.9	100	0	0	0	25.52	0.76	0	0	2.44882	2.66009	2.792	0.16165	0.001116	2.660089335	0.111663076	0.067	0	0.572437354	0.572437354	0.00023376	0.000165263	
3/16/6:00	26.4	26.4	22.1	97.75	47	147.0333	0.066165	21.89	0	0	0	2.43867	2.66009	3.442	0.20238	0.000803	3.440973535	0.080301942	0.067	0.0569019	0.436172094	0.436173994	0.00020219	0.000963093	
3/16/9:00	28.7	28.7	26.4	68.8	02	326.4833	0.1469175	17.53	0	0.26667	17.778	2.43324	3.94437	3.94437	0.22751	0.0118	3.924949045	0.062639045	0.067	0.12634905	0.350802089	0.477151139	0.000196097	0.118831261	
3/16/12:00	30	32	29.5	51.19	93	839.2333	0.377655	17.09	0	1.33333	88.889	2.42823	4.7289	4.7289	0.24771	0.02134	4.320054659	0.049013623	0.067	0.3247833	0.28071307	0.60551307	0.000249262	0.927301974	
3/16/15:00	25.2	31.6	25.2	53.33	27	294.1	0.132345	19.08	0	0.8333	53.333	2.4415	4.6571	4.6571	0.19023	0.01835	3.187359918	0.090055497	0.067	0.1138167	0.481360108	0.585176808	0.000243775	0.599645756	
3/16/18:00	22.1	24.4	22.1	86.66	63	0.983333	0.0004425	22.76	0	0	0	2.44882	3.0266	3.0266	0.16382	0.001118	2.656268873	0.111827105	0.067	0.00038055	0.573278246	0.573278246	0.000234259	0.004995603	
3/16/21:00	21.3	22.1	21.3	99.78	77	0	0	25.59	0	0	0	2.45071	2.65332	2.65332	0.15489	0.001172	2.532625063	0.117200872	0.067	0	0.594342289	0.594342289	0.000242518	0.000923392	
3/17/0:00	21.3	21.3	21	99.99	92	0	0	25.59	0	0	0	2.45071	2.53317	2.53317	0.15489	2.1E-05	2.533184064	0.117176286	0.067	0	0.594217606	0.594217606	0.000242467	0.000196672	
3/17/3:00	21.3	21.3	21	100	0	0	0	25.59	0	0	0	2.45071	2.53332	2.53332	0.15489	0	2.533204981	0.117175366	0.067	0	0.594212941	0.594212941	0.000242466	0.000169254	
3/17/6:00	24.4	24.4	21.3	99.49	88	69.58333	0.0313125	22.26	0	0	0	2.44339	3.0266	3.0266	0.18248	0.000953	3.054882668	0.095304883	0.067	0.02692875	0.503977852	0.503977852	0.000217283	0.001792768	
3/17/9:00	30.4	30.4	26.8	61.13	28	562.7333	0.25323	18.87	0	0.26667	17.778	2.43229	4.3372	4.3372	0.23213	0.01523	4.013658881	0.059522347	0.067	0.2177778	0.33511759	0.55289539	0.000227314	0.150888574	
3/17/12:00	31.6	31.6	30.4	42.28	78	559.8	0.25191	14.11	0	0.8333	53.333	2.4234	4.648	4.648	0.24771	0.02452	4.315672489	0.049161246	0.067	0.2166426	0.281517892	0.498217892	0.000205093	0.679864486	
3/17/15:00	32.4	32.4	27.6	46.68	78	272.55	0.1226475	28.03	0	0.53333	35.556	2.43584	4.8278	4.8278	0.21518	0.02277	3.670098012	0.071798012	0.067	0.10547685	0.396267395	0.501744245	0.000205994	0.456244696	
3/17/18:00	23.7	26	23.7	67.74	4	0.983333	0.0004425	20.11	0	0	0	2.44504	3.3293	3.3293	0.17591	0.01007	2.920351338	0.100753503	0.067	0.00038055	0.527795323	0.528175873	0.000216019	0.012236228	
3/17/21:00	23.7	23.7	23.7	89.99	87	0	0	19.13	0	0	0	2.44504	2.93061	2.93061	0.17591	0.001004	2.927637693	0.100455228	0.067	0	0.526232803	0.526232803	0.000215224	0.00365362	

Date/Time	T M P P P (°C)	TMP max (°C)	TMP min (°C)	RH	RH (%)	solar radia tion watt/ m ²	St. solar radian MJ/m ² 2/3hr	W ND (D eg)	Rai nfall (m m)	Win d spe ed km/ hr	U2 Win d spe ed m/s ec	Lam da MJ/ kg	e ^t k P a	e ^m ax kPa	e ^m n kPa	Delt a kPa/ °C	Db a f kPa	e ^d dew point vapor pressur e, kPa	Epsilon net emissi vity	Gamma Psychro metric constan t	Sh, net shortw ave radiati on, MJ/m ² 2/3hr	Ln, Long wave radiatio n, MJ/m ² 2/3hr	Rn, net radiatio n, MJ/m ² 2/3hr	Rn, net radiatio n mm/3hr	Ep, net evapor ation, mm/3hr
3/18/ 05 00.00	23 .3	23.7	23.3	0.9 82	15	0	0	10 0.5	0	0	0	2.44 599	2. 86	2.9 31	2.86 082	0.17 225	0.00 054	2.8602 85423	0.1032 26703	0.067	0	0.5378 42897	0.5378 42897	0.0002 19888	0.0008 00436
3/18/ 05 30.00	23 .7	23.7	22.9	1 0	0	0	0	86. 73	0	0	0	2.44 504	2.9 31	2.9 249	2.79 591	0.17 591	0	2.9306 07375	0.1003 33764	0.067	0	0.5255 96528	0.5255 96528	0.0002 14964	0.0001 55672
3/18/ 05 60.00	27 .6	27.6	23.3	0.9 32	15	9	05	96. 57	0	0.26 667	17. 778	2.43 584	3. 6	2.86 93	2.86 082	0.21 518	0.00 224	3.6905 37351	0.0710 49201	0.067	0.0405 963	0.3921 3456	0.4327 3086	0.0001 77652	0.0237 40011
3/18/ 05 90.00	31 .6	31.6	29.1	0.5 7	98	611. 7667	20 95	20 8.4	0	2.13 333	142 22	2.42 639	4. 6	4.6 48	4.02 888	0.26 287	0.01 866	4.6296 86395	0.0387 66115	0.067	0.2367 537	0.2255 67603	0.4623 21303	0.0001 90539	1.2296 50452
3/18/ 05 12.00	32 .4	32.4	32	0.4 74	4	607. 8333	17 25	17 2.3	0	1.33 333	88. 889	2.42 45	4. 8	4.8 63	4.75 478	0.27 339	0.02 53	4.8380 1563	0.0320 63146	0.067	0.2352 315	0.1885 31584	0.4237 63084	0.0001 74783	1.0185 34252
3/18/ 05 15.00	27 .2	30.8	27.2	0.4 65	53	85.2 8333	20 775	20 6.7	0	0	0	2.43 678	4. 4	3.60 42	3.60 739	0.21 084	0.02 152	3.5858 7043	0.0748 90475	0.067	0.0330 0465	0.4111 41095	0.4441 45745	0.0001 82267	0.0219 85613
3/18/ 05 18.00	24 .8	26	24.8	0.8 35	47	0	0	27 1.9	0.25	0	0	2.44 245	3. 3	3.13 024	0.18 632	0.00 537	0.00 537	3.1248 68768	0.0925 17823	0.067	0	0.4918 75344	0.4918 75344	0.0002 01386	0.0061 74963
3/18/ 05 21.00	23 .7	24.4	23.7	0.9 53	33	0	0	26 5.1	0	0.8	53. 333	2.44 504	2. 3	3.0 56	2.93 061	0.17 591	0.00 14	2.9292 10427	0.1003 90893	0.067	0	0.5258 95794	0.5258 95794	0.0002 15086	0.0488 36387
3/19/ 05 00.00	21 .3	22.5	21.3	0.9 92	18	0	0	15 7.8	44.7	2.13 333	142 22	2.45 071	2. 5	2.7 26	2.53 32	0.15 489	0.00 021	2.5329 90247	0.1171 8481	0.067	0	0.5942 60835	0.5942 60835	0.0002 42485	0.0219 06189
3/19/ 05 30.00	21 .3	21.3	21.3	1 0	0	0	0	11 7.4	8.63	0.53 333	35. 556	2.45 071	2. 5	2.5 33	2.53 32	0.15 489	0	2.5332 04981	0.1171 75366	0.067	0	0.5942 12941	0.5942 12941	0.0002 42486	0.0001 69264
3/19/ 05 60.00	21 .7	21.7	21.3	0.9 31	45	8.83 3333	0.0039 75	12 1.4	15.5	0	0	2.44 977	2. 5	2.5 96	2.53 32	0.15 824	0.00 177	2.5942 00429	0.1145 08695	0.067	0.0034 185	0.5838 51162	0.5872 69662	0.0002 39725	0.0024 46183
3/19/ 05 90.00	22 .5	22.5	22.1	0.6 09	85	101	5	55. 3	13.2	0	0	2.44 788	2. 7	2.6 26	2.66 009	0.16 512	0.01 054	2.7150 45144	0.1093 16483	0.067	0.0390 87	0.5634 50206	0.6025 37206	0.0002 46147	0.0132 67211
3/19/ 05 12.00	23 .7	23.7	22.9	0.4 5	45	194. 1167	0.0873 525	16 3.9	2.53	0.26 667	17. 778	2.44 504	2. 9	2.9 31	2.79 249	0.17 591	0.01 574	2.9148 68858	0.1009 78182	0.067	0.0751 2315	0.5289 72297	0.6040 95447	0.0002 47069	0.1953 54839
3/19/ 05 15.00	22 .5	24	22.5	0.4 93	3	105 8833	0.0476 475	15 4.9	0	0.53 333	35. 556	2.44 788	2. 9	2.9 84	2.72 559	0.16 512	0.01 447	2.7111 14011	0.1094 83548	0.067	0.0409 7685	0.5643 11308	0.6052 88158	0.0002 47271	0.3606 93879
3/19/ 05 18.00	20 .2	22.1	20.2	0.8 89	85	0	0	22. 23	0	0	0	2.45 331	2. 6	2.6 739	0.14 599	0.00 28	0.00 28	2.3645 84879	0.1247 19105	0.067	0	0.6230 71686	0.6230 71686	0.0002 53972	0.0040 37561
3/19/ 05 21.00	20 .2	20.2	19.8	0.9 95	45	0	0	14. 97	0	0	0	2.45 331	2. 3	2.3 949	0.14 599	0.00 013	0.00 013	2.3672 59083	0.1245 97405	0.067	0	0.6224 63694	0.6224 63694	0.0002 53724	0.0003 51197
3/20/ 05 00.00	20 .6	20.6	19.8	0.9 99	92	0	0	48. 5	0	0.26 667	17. 778	2.45 236	2. 4	2.4 27	2.30 949	0.14 918	2E- 05	2.4265 32579	0.1219 17358	0.067	0	0.6124 02989	0.6124 02989	0.0002 4972	0.0004 53495
3/20/ 3.00	20 .6	20.6	20.2	1 0	0	0	0	10 9.2	0	0.26 667	17. 778	2.45 236	2. 4	2.4 27	2.36 739	0.14 918	0	2.4265 52312	0.1219 16472	0.067	0	0.6123 98535	0.6123 98535	0.0002 49718	0.0001 72323

Date/Time	TMP P (°C)	TMP max (°C)	TMP min (°C)	RH (%)	RH (%)	solar radiation wati/m ²	St. solar radian MJ/m ² /3hr	W ND (Deg)	Rai nfall (m)	Win spe ed km/hr	U2. Win spe m/s	Lam da MJ/kg	e ^t k P a	e ^m ax kPa	e ^m n kPa	Delt a kPa/°C	Db a kPa	e ^d dew point pressur e, kPa	Epsilon net emmissi vity	Gamma Psychro metric constan t	Sh, net shortw ave radiati on, MJ/m ² /3hr	Ln, Long wave radiatio n, MJ/m ² /3hr	Rn, net radiatio n, MJ/m ² /3hr	Rn, net radiatio n, mm/3hr	Ep, net evapor ation, mm/3hr
3/20/05.00	21.7	21.7	20.6	99.93	99.28	58.83333	0.026475	20.1.1	0	0	0	2.44977	2.6	2.596	2.42655	0.15824	0.00018	2.595790021	0.114439621	0.067685	0.02279897	0.58349897	0.60626747	0.00024748	0.000405525
3/20/05.00	28	28	22.5	77.76	58.35	582.575	0.2620575	22.5.2	0	1.33333	88.889	2.43489	3.78	3.7	2.72559	0.2196	0.00729	3.772637763	0.06774055	0.0676945	0.377716608	0.603086058	0.000247685	0.348729422	
3/20/05.00	30.8	30.8	28.7	65.86	57.61	799.9833	0.3599925	17.0.2	0	0.53333	35.556	2.42828	4.44	4.4	3.93675	0.25268	0.01736	4.424333755	0.06722596	0.0679355	0.309511421	0.571704971	0.000235436	0.306397523	
3/20/05.00	26	31.6	26	61.61	56.45	376.45	0.1694025	25.3.6	0	0	0	2.43961	3.36	4.6144	3.36144	0.01758	0.0158341	3.343858341	0.06792923	0.0678615	0.14568865	0.599474815	0.000245725	0.018947925	
3/20/05.00	22	24.4	22.5	90.08	82.0	0	0	35.4.4	0	0	0	2.44788	2.73	3.056	2.72512	0.00265	0.000265	2.722932751	0.108981642	0.0672433	0.56172433	0.56172433	0.000229474	0.003460159	
3/20/05.00	22	22.5	22.1	99.95	53.0	0	0	35.4.4	0	0	0	2.44882	2.66	2.7209	0.16165	0.00013	0.00063669	2.659968469	0.0670.1116	0.0670.067	0.572465004	0.572465004	0.000233772	0.000324143	
3/21/00.00	21	22.5	21.3	10.1	0	0	0	94.2	0	0	0	2.45071	2.53	2.732	0.15489	0.0000	0.00004981	2.533204981	0.117175366	0.0670.067	0.594212941	0.594212941	0.000242466	0.000169254	
3/21/00.00	21	21.3	21	10.0	0	0	0	12.8.4	0	0	0	2.45071	2.53	2.732	0.15489	0.0000	0.00004981	2.533204981	0.117175366	0.0670.067	0.594212941	0.594212941	0.000242466	0.000169254	
3/21/00.00	26	26.4	21.3	98.84	43.0	226.4667	0.10191	10.1.2	0	0.53333	35.556	2.43867	3.44	3.4	2.532	0.20238	0.000047	3.441278397	0.080290438	0.0670.067	0.436109608	0.523752208	0.00021477	0.010014251	
3/21/00.00	30	30.4	27.2	70.01	08.0	667.65	0.3004425	22.6.9	0	1.6	106.67	2.42923	4.434	4.341	3.60739	0.24771	0.01189	4.329500589	0.06795672	0.0678055	0.278908675	0.537289225	0.000221177	0.618035477	
3/21/00.00	31	31.6	30.8	50.05	47.0	916.6667	0.412513	13.7.1	0	2.13333	142.22	2.42734	4.454	4.648	4.44169	0.25773	0.02251	4.521486586	0.042306975	0.0675	0.354781039	0.599631039	0.000247032	1.506117767	
3/21/00.00	27	30.4	27.6	51.15	47.0	213.7333	0.09618	66.33	0	0.26667	17.778	2.43584	3.69	4.341	3.69278	0.21518	0.0195	3.673285701	0.071678551	0.067148	0.082708067	0.478322867	0.000196369	0.205174411	
3/21/00.00	22	26.4	22.9	86.63	25.0	293.3333	0.00132	77.6	1.78	0.26667	17.778	2.44693	2.79	3.442	2.79249	0.16865	0.000429	2.788203729	0.106229187	0.067352	0.550506027	0.551641227	0.000225442	0.055215949	
3/21/00.00	22	22.9	22.5	99.43	25.0	0	0	81.35	0	0	0	2.44788	2.72	2.72	0.16512	0.000159	0.00027240	0.108901159	0.06736323	0.0670	0.561490745	0.561490745	0.000229379	0.002133293	
3/22/00.00	21	22.1	21.3	99.7	95.0	0	0	29.9.5	0	0	0	2.45071	2.53	2.632	0.15489	0.000079	0.00025324	0.117213004	0.067102	0.0670	0.594389592	0.594389592	0.000242538	0.001207352	
3/22/00.00	20	21.3	20.6	98.88	83.0	0	0	29.9.5	0.25	0	0	2.45236	2.53	2.4233	0.14918	0.00029	2.426262993	0.121929473	0.0670	0.612463842	0.612463842	0.000249744	0.000563688		
3/22/00.00	26	26.4	20.6	89.98	8.0	174.5	0.078525	23.4.6	0	0	0	2.43961	3.44	3.44	0.19826	0.000299	3.358446996	0.083435074	0.067315	0.067574775	0.450706275	0.518312454	0.000212454	0.003352965	
3/22/00.00	28	28.7	26.8	63.06	4.95	535.3	0.240885	21.1.4	0	1.06667	71.111	2.43324	3.3	3.937	3.52372	0.22345	0.01345	3.923306	0.062697282	0.067611	0.351128236	0.568289336	0.000229443	0.502662722	

Date/Time	TM P (°C)	TM P max (°C)	TM P min (°C)	RH (%)	RH (%)	solar radiation watt/m ²	Solar radiation MJ/m ² /23hr	Wind speed m/sec	U2, Wind speed m/sec	La m d a M J/ k g	e ^a kPa	e ^m kPa	e ^m kPa	e ^a kPa	Delta kPa/°C	D a r k P a	e ^d , dew point pressure, kPa	Ep, net emittance	Gamma, Psychrometric constant	S _n , net short wave radiation, MJ/m ² /hr	Ln, Long wave radiation, MJ/m ² /3hr	R _n , net radiation, MJ/m ² /hr	R _n , net radiation mm/3hr	Ep, net evaporation, mm/3hr
3/22/05 12:00	30.8	30.8	26	50.0	73.0	0.328	120.2	0.8	5	2.42828	4.4	4.4	3.36	0.0194	0.0194	0.0194	4.4	0.045593	0.0	0.28266	0.2	0.545184	0.0	0.507
				5	4	68			3			144	4	9	2	9	222	522	67	48	625	6	0.002	31496
				0					3			4	4		5		027				198		245	15
				1					3			2			6		8						15	
3/22/05 15:00	28	32	28	52.0	35.0	0.160	83.92	1.0666	7	2.43489	3.7	4.0	3.77	0.0204	0.0204	0.0204	3.7	0.068549	0.0	0.13773	0.3	0.518058	0.0	0.787
				5	9	155			1		8	7	993	8	2	8	594	633	67	33	803	706	0.002	19883
				2					1			5			1		541				554		127	3
				2					1			5			6		82				06		177	
3/22/05 18:00	22	26	22	86.0	2.933	0.0013	11	35.5	2.44	2.33	2.72	0.16	0.00	2.72158	2.72158	0.10903	0.0	0.0011	0.56201	0.56315	0.00023	0.00023	0.00985	
				85	333	2	9.4	56	788	73	61	512	512	4	4	5386	8805	67	352	8968	4168	0.0058	0.0058	3636
				94		0	0	0	2.44	2.27	2.66	0.16	0.00	2.72418	2.72418	0.10892	0.0	0	0.56145	0.56145	0.00022	0.00022	0.00190	
				8		0	0	0	788	73	26	009	512	14	14	7331	8427	67		0048	0048	9362	9362	2085
3/22/05 21:00	22	22	22	90.0	0	0	0	0	2.44	2.27	2.72	0.16	0.00	2.72297	2.72297	0.10897	0.0	0	0.56171	0.56171	0.00022	0.00022	0.00340	
				42		0	0	0	788	73	26	559	512	261	261	5585	9825	67		4964	4964	947	947	6963
				97		0	0	0	2.44	2.28	2.72	0.17	0.00	2.86019	2.86019	0.10323	0.0	0.0113	0.53786	0.54924	0.00022	0.00022	0.00091	
				75	667	375	7	0	599	86	61	559	225	063	063	2659	0542	67	8425	2902	7152	455	455	4984
3/23/05 00:00	22	22	22	90.0	0	0	0	0	2.43	3.34	2.93	0.20	0.00	3.44038	3.44038	0.08032	0.0	0.0963	0.43629	0.53266	0.53266	0.00021	0.00021	0.00159
				73	167	575	75	0	867	44	42	061	238	136	136	6999	4077	67	6945	2321	1771	8423	8423	0884
				73	167	575	75	0	867	44	42	061	238	136	136	6999	4077	67	6945	2321	1771	8423	8423	0884
3/23/05 03:00	23	23	23	69.0	342.1	0.1539	20	0	2.43	3.38	3.52	0.21	0.01	3.76880	3.76880	0.06821	0.0	0.1324	0.37848	0.51089	0.51089	0.00020	0.00020	0.01109
				8	5	675	9.5	0	489	78	46	372	96	113	113	1391	2386	67	1205	4153	6203	9823	9823	6585
				66	833	375	16	53.3	2.44	3.34	3.20	0.19	0.01	3.19463	3.19463	0.08977	0.0	0.0565	0.47983	0.53636	0.53636	0.00021	0.00021	0.36187
				68	833	375	5.7	33	15	21	42	571	023	107	107	8685	0269	67	3425	552	977	9688	9688	2277
3/23/05 06:00	23	24	23	89.0	2.933	0.0013	75	35.5	2.44	2.30	2.86	0.17	0.00	2.85765	2.85765	0.10333	0.0	0.0011	0.53841	0.53954	0.53954	0.00022	0.00022	0.07626
				3	333	2	93	56	599	86	56	082	225	317	317	5463	5581	67	352	0188	5388	0584	0584	8602
				93	333	2	93	56	599	86	56	082	225	317	317	5463	5581	67	352	0188	5388	0584	0584	8602
3/23/05 09:00	20	22	20	99.0	0	0	4	124	2.45	2.26	2.42	0.14	4.2E	2.42650	2.42650	0.12191	0.0	0	0.61240	0.61240	0.61240	0.00024	0.00024	0.00405
				83		0	83	44	236	43	6	655	918	-05	-05	9923	8377	67		8103	8103	9722	9722	5947
				83		0	83	44	236	43	6	655	918	-05	-05	9923	8377	67		8103	8103	9722	9722	5947

Date/Time	TMP P (°C)	TMP max (°C)	TMP min (°C)	RH	RH (%)	solar radiation wati/m ²	St. solar radian MJ/m ² /3hr	W ND (Deg)	Rai nfall (m)	Win d spe ed km/hr	U2. Win d spe ed m/s	Lam da MJ/kg	e ^t k P a	e ^m ax kPa	e ^m n kPa	Delt a kPa/°C	Db a kPa	e ^d . dew point pressur e, kPa	Epsilon net emmissi vity	Gamma Psychro metric constan t	Sh, net shortw ave radiati on, MJ/m ² /3hr	Ln, Long wave radiatio n, MJ/m ² /3hr	Rn, net radiatio n, MJ/m ² /3hr	Rn, net radiatio n, mm/3hr	Ep, net evapor ation, mm/3hr
3/26/05 0:00	22.5	22.5	22.1	1	10	0	0	17	0	0	0	2.44	2.7	2.7	2.66	0.16	0	2.7255	0.1088	0.067	0	0.5611	0.5611	0.0002	0.0001
3/26/05 3:00	22.5	22.5	22.1	0.99	99	0	0	17	0	0	0	2.44	2.7	2.66	0.16	4.5E-05	2.6600	0.1116	0.067	0	0.5724	0.5724	0.0002	0.0002	
3/26/05 6:00	24.4	24.4	22.1	1	10	82.3	0.0370	17	0	0	0	2.44	3.0	2.66	0.18	0	3.0663	0.0952	0.067	0.0318	0.5036	0.5355	0.0002	0.0001	
3/26/05 9:00	29.9	29.9	27.6	0.99	99	620	0.2792	21	0	0	0	2.43	4.2	3.69	0.23	3.3E-05	4.1228	0.0557	0.067	0.2401	0.3154	0.5556	0.0002	0.0002	
3/26/05 12:00	33.2	33.2	29.9	0.99	99	764	0.3441	17	0	0	0	2.42	5.0	4.21	0.28	0.00	5.0866	0.0242	0.067	0.2959	0.1440	0.4400	0.0001	0.0003	
3/26/05 15:00	32	32	28.7	0.96	96	287	0.1292	12	0	0	0	2.43	4.7	3.93	0.22	0.00	3.9350	0.0622	0.067	0.1111	0.3487	0.4599	0.0001	0.0017	
3/26/05 18:00	25.6	25.6	23.3	0.99	99	1.96	0.0008	49	0	0	0	2.44	3.2	2.86	0.17	0.00	2.8605	0.1032	0.067	0.0007	0.5377	0.5385	0.0002	0.0005	
3/26/05 21:00	22.9	22.9	22.1	1	10	0	0	49	0	0	0	2.44	2.7	2.66	0.16	0	2.6600	0.1116	0.067	0	0.5724	0.5724	0.0002	0.0001	
3/27/05 0:00	21.7	21.7	21.7	1	10	0	0	49	0	0	0	2.44	2.6	2.59	0.15	0	2.5959	0.1144	0.067	0	0.5834	0.5834	0.0002	0.0001	
3/27/05 3:00	21.3	21.3	21.3	1	10	0	0	49	0	0	0	2.45	2.5	2.53	0.15	0	2.5332	0.1171	0.067	0	0.5942	0.5942	0.0002	0.0001	
3/27/05 6:00	25.2	25.2	21.3	1	10	109	0.0494	49	0	0	0	2.44	3.2	2.53	0.19	0	3.2057	0.0893	0.067	0.0424	0.4775	0.5200	0.0002	0.0001	
3/27/05 9:00	32	32	28.7	0.94	95	756	0.3405	14	0	0.53	35	2.42	4.7	3.93	0.26	0.00	4.7521	0.0348	0.067	0.2929	0.2036	0.4965	0.0002	0.0444	
3/27/05 12:00	34.1	34.1	31.2	0.85	85	855	0.3851	12	0	1.6	106	2.42	5.3	4.54	0.29	0.00	5.3416	0.0164	0.067	0.3312	0.0987	0.4300	0.0001	0.3323	
3/27/05 15:00	34.1	34.1	30.4	0.86	86	439	0.1976	12	0	0.53	35	2.42	4.7	3.93	0.24	0.00	4.3349	0.0485	0.067	0.1699	0.2778	0.4478	0.0001	0.1150	
3/27/05 18:00	26.8	26.8	24	0.96	96	1.96	0.0008	12	0	0	0	2.44	3.5	2.98	0.17	0.00	2.9827	0.0992	0.067	0.0007	0.5165	0.5173	0.0002	0.0015	
3/27/05 21:00	23.3	23.3	23.3	1	10	0	0	12	0	0	0	2.44	2.9	2.86	0.17	0	2.8608	0.1032	0.067	0	0.5377	0.5377	0.0002	0.0001	
3/28/05 0:00	23.7	23.7	22.9	1	10	0	0	19	0	0	0	2.44	2.9	2.79	0.16	0	2.7924	0.1060	0.067	0	0.5495	0.5495	0.0002	0.0001	

Date/Time	TMP max (°C)	TMP min (°C)	RH	RH (%)	solar radiation w/m ²	St. solar radiation MJ/m ² /3hr	W ND (deg)	Rainfall (m)	Wind speed km/hr	U2 Wind speed m/sec	Lambda MJ/kg	ek Pa	e'm ax kPa	e'mi n kPa	Delta a °C	Delta f kPa	Dbair kPa	e'd point vapor pressure, kPa	Epsilon net emissivity	Gamma Psychrometric constant	Sh, net shortwave radiation, MJ/m ² /3hr	Ln, Long wave radiation, MJ/m ² /3hr	Rn, net radiatio n MJ/m ² /3hr	Rn, net radiatio n mm/3hr	Ep, net evaporation, mm/3hr
3/28/05 3:00	22.9	22.1	1	10	0	0	19.97	0	0	0	2.44882	2.6686	2.792	2.66009	0.16165	0	2.6800	0.1116	0.067	0	0.5724	0.5724	0.0002	0.0002	0.0001
3/28/05 6:00	24.4	22.1	1	10	39.2	0.0176475	22.55	0	0	0	2.44339	3.0339	3.05609	2.660248	0.18248	0	3.0563	0.0952	0.067	0.01517685	0.5036	0.5188	0.0002	0.0001	0.0001
3/28/05 9:00	28	25.2	0.8	83	324.5333	0.14604	18.92	0	0.53333	35.556	2.43489	3.73208	3.20571	3.20571	0.2196	0.00	3.7741	0.0680	0.067	0.1255944	0.3774	0.5029	0.0002	0.0002	0.1131
3/28/05 12:00	28.7	24.8	0.6	88	146.0667	0.06573	15.73	0.5	0.8333	53.333	2.44245	3.937	3.13024	3.13024	0.18632	0.01	3.1191	0.0927	0.067	0.0565278	0.4930	0.5495	0.0002	0.0002	0.3670
3/28/05 15:00	24	23.7	0.6	65	22.5667	0.010155	14.79	1.01	0	0	2.44434	2.984	2.93061	2.93061	0.1787	0.01	2.9735	0.0985	0.067	0.0087333	0.5185	0.5272	0.0002	0.0002	0.0121
3/28/05 18:00	24	22.9	0.9	92	2.93333	0.00132	64.7	0	0	0	2.44693	2.929	2.7984	2.7984	0.16865	0.15	2.7903	0.1061	0.067	0.0011352	0.5500	0.5511	0.0002	0.0002	0.0027
3/28/05 21:00	22.9	22.9	0.9	99	0	0	67.5	0	0	0	2.44693	2.729	2.7984	2.7984	0.16865	0.15	2.7903	0.1061	0.067	0	0.5495	0.5495	0.0002	0.0002	0.0002
3/29/05 0:00	22.9	22.5	1	10	0	0	29.27	0	0	0	2.44788	2.729	2.729	2.729	0.16512	0	2.7255	0.1088	0.067	0	0.5611	0.5611	0.0002	0.0002	0.0001
3/29/05 3:00	22.5	21.7	1	10	0	0	32.3	0	0	0	2.44882	2.729	2.729	2.729	0.16512	0	2.7255	0.1088	0.067	0	0.5724	0.5724	0.0002	0.0002	0.0001
3/29/05 6:00	24.8	22.5	0.9	99	81.3833	0.0366225	58.55	0	0	0	2.44245	3.131	3.131	3.131	0.18632	2.4E-05	3.1302	0.0923	0.067	0.03149535	0.4907	0.5222	0.0002	0.0001	0.0001
3/29/05 9:00	28.7	26.4	0.9	92	512.7667	0.230745	19.66	0	1.06667	71.111	2.43324	3.934	3.4437	3.44175	0.22751	0.00	3.9339	0.0623	0.067	0.1984407	0.3490	0.5474	0.0002	0.0002	0.1063
3/29/05 12:00	32.4	29.1	0.8	82	777.4333	0.349845	17.13	0	1.667	106.67	2.4245	4.863	4.02888	4.02888	0.27339	0.00	4.8554	0.0315	0.067	0.3006667	0.1852	0.4861	0.0002	0.0002	0.3765
3/29/05 15:00	32.8	27.2	0.6	64	295.1	0.132795	19.45	0	0.53333	35.556	2.43678	4.974	3.6074	3.6074	0.21084	0.01	3.5922	0.0746	0.067	0.1142037	0.4098	0.5240	0.0002	0.0002	0.3081
3/29/05 18:00	26	24	0.9	95	0.98333	0.0004425	14.35	0	0	0	2.44434	3.361	3.29861	3.29861	0.1787	0.00	2.9823	0.0982	0.067	0.00038055	0.5166	0.5170	0.0002	0.0002	0.0019
3/29/05 21:00	23.7	22.9	1	10	0	0	43.6	0	0	0	2.44693	2.929	2.929	2.929	0.16865	0	2.7924	0.1060	0.067	0	0.5495	0.5495	0.0002	0.0002	0.0001
3/30/05 0:00	22.9	22.5	1	10	0	0	43.6	0	0	0	2.44788	2.729	2.729	2.729	0.16512	0	2.7255	0.1088	0.067	0	0.5611	0.5611	0.0002	0.0002	0.0001
3/30/05 3:00	22.9	22.5	1	10	0	0	43.6	0.25	0	0	2.44693	2.729	2.729	2.729	0.16865	0	2.7924	0.1060	0.067	0	0.5495	0.5495	0.0002	0.0002	0.0001

Date/ Time	T M P (° C)	TMP max (° C)	TMP min (° C)	RH (%)	RH (%)	solar radia tion watt/ m ²	St. solar radian MJ/m ² 2/3hr	W ND (D eg)	Rai nfall (m m)	Win d spe ed, km/ hr	U2, Win d spe ed, m/s sec	Lam da MJ/ kg	e ^t k P a	e ^m ax, kPa	e ^m n, kPa	Delt a kPa/ °C	Db a kPa	e ^d , dew point vapor pressur e, kPa	Epsilon net emissi vity	Gamma Psychro metric constan t	Sh, net shortw ave radiati on, MJ/m ² 2/3hr	Ln, Long wave radiatio n, MJ/m ² 2/3hr	Rn, net radiatio n, MJ/m ² 2/3hr	Rn, net radiatio n mm/3hr	Ep, net evapor ation, mm/3hr
3/30/ 05 6:00	27 .6	27.6	22.9	0.9 87	0.9 72	122. 55	0.0551 475	12 2.4	0.51	0	0	2.43 584	3 69	3.6 93	2.79 249	0.21 518	0.00 042	3.6923 65622	0.0709 82584	0.067	0.0474 2685	0.3917 66886	0.4391 93736	0.0001 80305	0.0005 53127
3/30/ 05 9:00	29 .5	29.9	26.4	0.7 69	0.7 92	700. 9833	0.3154 425	16 1.7	0	1.33 333	88. 889	2.43 135	4. 12	4.2 19	3.44 175	0.23 684	0.00 884	4.1140 43935	0.0560 36514	0.067	0.2712 8055	0.3171 65097	0.5884 45647	0.0002 42024	0.3981 71424
3/30/ 05 12:00	26 .4	30.4	23.7	0.6 45	0.6 52	557. 8333	0.2510 25	10 8	15.2 4	1.33 333	88. 889	2.43 867	3. 44	4.3 41	2.93 061	0.20 238	0.01 29	3.4288 44698	0.0807 60042	0.067	0.2158 815	0.4386 6033	0.6545 4183	0.0002 68401	0.6588 92473
3/30/ 05 15:00	29 .9	30.4	28.3	0.9 83	0.9 28	406. 8667	0.1830 9	13 5.5	0	0	0	2.43 041	4. 22	4.3 41	3.84 646	0.24 162	0.00 07	4.2180 85606	0.0524 88301	0.067	0.1574 574	0.2985 41932	0.4559 99332	0.0001 87623	0.0007 87052
3/30/ 05 18:00	24 .8	26.8	24.4	1 0	1 0	4.9 05	0.0022 05	21 9.6	0	0	0	2.44 245	3. 13	3.5 24	3.05 631	0.18 632	0 0	3.1302 35219	0.0923 05409	0.067	0.0018 963	0.4907 46035	0.4926 42335	0.0002 017	0.0001 48353
3/30/ 05 21:00	24 .0	24.8	24	1 0	1 0	0 0	0 0	19 2.2	0	0	0	2.44 434	2. 98	3.1 3	2.98 392	0.17 87	0 0	2.9839 17477	0.0981 63728	0.067	0 0	0.5163 10378	0.5163 10378	0.0002 11227	0.0001 53628
3/31/ 05 0:00	24 .0	24.4	24	1 0	1 0	0 0	0 0	30 3.3	0	0	0	2.44 434	2. 98	3.0 56	2.98 392	0.17 87	0 0	2.9639 17477	0.0981 63728	0.067	0 0	0.5163 10378	0.5163 10378	0.0002 11227	0.0001 53628
3/31/ 05 3:00	23 .3	24	23.3	1 0	1 0	0 0	0 0	11 4.4	0	0.26 667	17. 778	2.44 599	2. 86	2.9 84	2.86 082	0.17 225	0 0	2.8608 2113	0.1032 04531	0.067	0 0	0.5377 27375	0.5377 27375	0.0002 1984	0.0001 58276
3/31/ 05 6:00	21 .3	21	0.9 72	0.9 18	0.9 18	3.933 333	0.0017 7	16 2.9	1.06 667	71.1 11	2.45 071	2. 53	2.6 6	2.53 32	0.15 489	0.00 073	0.00 073	2.53247 3592	0.11720 7535	0.0015 67	0.0015 222	0.59437 6076	0.59589 8276	0.00024 3153	0.03766 7274
3/31/ 05 9:00	22 .1	22	0.6 97	0.6 72	0.6 72	27.45 525	0.0123 8	12 8	0	0	0	2.44 882	2. 66	2.6 6	2.59 597	0.16 165	0.00 796	2.65213 0785	0.11200 4905	0.0	0.0106 2315	0.57418 9731	0.58481 2881	0.00023 8814	0.01023 0367
3/31/ 05 12:00	27 .6	27	0.5 59	0.5 93	0.5 66	441.1 667	0.1985 25	19 8.8	0.8 9	53.3 33	2.43 584	3. 69	3.6 93	2.72 559	0.21 518	0.01 414	0.00 414	3.67864 0153	0.07148 306	0.0	0.1707 315	0.39452 9112	0.56526 0612	0.00023 206	0.41807 7811
3/31/ 05 15:00	24 .8	24	0.5 26	0.5 57	0.5 57	230.3 833	0.1036 725	19 5.2	1.06 667	71.1 11	2.44 245	3. 13	3.6 07	3.13 024	0.18 632	0.01 598	0.00 598	3.11425 5622	0.09293 8441	0.0	0.0891 5635	0.49411 1577	0.58326 9927	0.00023 8806	0.70213 5674

Weather data for dry period

Date /Time	TMp (°C)	TMp max (°C)	TMn (°C)	RH	RH (%)	solar radiation MJ/m ² /3hr	St. solar radiation MJ/m ² /3hr	Wind Dir (Degr)	Wind speed km/hr	U2, Wind speed m/sec	Lamda (late n heat) MJ/kg	e*, vapor pressure kPa	e*max, kPa	e*min, kPa	Delta, Grnd ent, kPa/C	Dbar, kPa	e* d, dew point vapor pressure, kPa	Epstlon, n, net emmivty	Gamm, Psychrometric constant	Sh, net short wave radiation, MJ/m ² /3hr	Ln, Long wave radiation, MJ/m ² /3hr	Rn, net radiation, MJ/m ² /3hr	Rn, net radiation, mm/3 hr	Ep, net evaporation, mm/3 hr
9/5/04	21.6	21.7	21.3	1	100	0	0	13	0	0	2.44	2.585	2.595	2.533	0.157	0	2.585	0.114	0.067	0	0.585	0.58	0.000	0.000
9/5/00	33.3	33.3	33.3	5	5	0	0	5	0	0	9923	4157	9699	2049	6781	0	4157	8908		2699	5269	2388	1676	
9/5/04	21.1	21.3	21.1	1	100	0	0	13	0	0	2.45	2.502	2.533	2.487	0.153	0	2.502	0.118	0.067	0	0.599	0.59	0.000	0.000
9/5/00	67	67	67	7	7	0	0	5	0	0	1182	3227	2049	0053	2411	0	3227	5377		4905	9490	2445	1701	
9/5/04	22.3	24.2	21.1	1	97.4	15	0.056	15	0.26	17.7	2.44	2.703	3.130	2.487	0.163	0.000	2.702	0.109	0.067	0.04	0.61	0.61	0.000	0.009
9/5/00	67	67	67	7	7	3	488	3	7	78	8192	6001	2352	0053	9559	7115	8885	8335		8562	0947	3656	2506	
9/5/04	29.7	32.4	26.1	5	68	19	0.328	19	0.8	53.3	2.43	4.863	4.863	3.523	0.239	0.013	4.161	0.054	0.067	0.28	0.308	0.59	0.000	0.359
9/5/00	67	67	67	7	7	4	383	4	3	33	0838	5947	3111	7195	4168	2305	3642	4080		2658	8309	1489	3319	
9/5/04	33.2	34.4	32.1	3	53	2	0.432	2	1.6	106	2.42	5.091	5.348	4.863	0.284	0.023	5.068	0.024	0.067	0.37	0.147	0.51	0.000	1.097
9/5/00	67	67	67	7	7	3	960	3	3	67	2575	6035	9488	3111	5008	4967	1068	8256		1829	5414	9371	2143	
9/5/04	33.3	34.1	31.1	5	50	19	0.212	19	0.53	35.5	2.42	5.134	5.348	4.648	0.286	0.024	5.109	0.023	0.067	0.18	0.140	0.32	0.000	
9/5/00	67	67	67	7	7	3	64	3	3	56	2221	5306	9488	3496	5816	5433	9872	5260		2870	0921	2962	1333	
9/5/04	25.5	28.4	24.1	8	87	18	0.002	18	0	0	2.44	3.269	3.779	3.056	0.193	0.004	3.265	0.087	0.067	0.00	0.467	0.46	0.000	0.004
9/5/00	33	33	33	7	7	4	205	4	0	0	0715	8169	9303	3126	5439	3694	4474	0123		1896	1754	9071	1921	
9/5/04	23.3	23.7	22.1	3	91	9	0	9	0	0	2.44	2.872	2.930	2.725	0.172	0.002	2.869	0.102	0.067	0	0.536	0.53	0.000	0.003
9/5/00	67	67	67	7	7	3	0	3	0	0	5831	3504	6073	5876	8556	4557	8947	8293		0	2543	6254	2192	
9/6/04	22.4	22.9	21.1	8	92	16	0	16	0	0	2.44	2.714	2.792	2.595	0.164	0.001	2.712	0.109	0.067	0	0.563	0.56	0.000	0.002
9/6/00	33	33	33	7	8	9	0.035	9	0.53	35.5	8034	5744	4897	9699	5369	9398	6345	4189		4697	4697	3469	2301	
9/6/04	21.3	21.7	21.1	3	99.5	32	0	32	0	0	2.45	2.533	2.533	2.533	0.154	0.000	2.533	0.117	0.067	0	0.594	0.59	0.000	0.000
9/6/00	67	67	67	7	7	6	0	6	0	0	0710	2049	2049	2049	8925	1182	0867	1805		2393	4239	2424	3242	
9/6/04	22.5	23.1	21.1	5	95	85	0.035	85	0.53	35.5	2.44	2.728	2.930	2.487	0.165	0.001	2.727	0.108	0.067	0.03	0.560	0.59	0.000	0.028
9/6/00	67	67	67	7	7	7	288	7	3	56	7838	3469	6073	0053	2656	1512	1957	8008		0347	9190	1266	2415	
9/6/04	28.9	30.8	26.1	5	67	20	0.335	20	1.6	106	2.43	3.994	4.441	3.361	0.230	0.012	3.981	0.060	0.067	0.28	0.340	0.62	0.000	
9/6/00	5	5	5	5	5	6.7	745	6.7	0	0	2649	1178	6910	4388	3874	8556	2822	6565		8740	8262	9586	2587	
9/6/00	67	67	67	7	7	3	0	3	0	0	05	65	99	29	16	58	07	93		7	18	92	99	

Date /Time	TMP (°C)	TM Pmax (°C)	TM Pmin (°C)	RH (%)	RH (%)	solar radiation MJ/m ² /hr	St. solar radiation MJ/m ² /hr	Wind speed m/sec	U2, Wind speed m/sec	Lam da (late heat) MJ/kg	e*, vapor pressure kPa	e*max kPa	e*min kPa	Delta, Gradi ent, kPa/°C	Dbar, kPa	e'd, dew point pressure, kPa	Epsilo n, net emmiv ity	Gam ma, Psych rometr ic constan t	Sh, net wave radia tion, MJ/m ² /3hr	Ln, Long wave radia tion, MJ/m ² /3hr	Rn, net radia tion, MJ/m ² /hr	Rn, net radiation, MJ/m ² /hr	Rn, net radiation, mm/3 hr	Ep, net evapo ration mm/3 hr
9/6/04	31.7	32.4	30.4	55.7	55.7	786.283	0.353828	124.444	124.444	2.426077	4.6635926	4.8633111	4.3413906	0.2645964	0.0203884	4.6632041	0.0376776	0.067	0.304291	0.2196180	0.523909	0.0002159	1.1716537	
9/6/04	31.3	32.8	29.9	56.6	56.6	450.983	0.202943	106.666	106.666	2.427061	4.5742226	4.9739919	4.2187883	0.2592199	0.0199636	4.5542589	0.0412300	0.067	0.174530	0.2390137	0.413544	0.0001703	1.0015228	
9/6/04	24.4	28.3	22.1	77.3	77.3	2.93333	0.00132	71.111	71.111	2.443312	3.0624141	3.8464613	2.660893	0.1827944	0.0073578	3.0550563	0.0852979	0.067	0.001135	0.5041668	0.505302	0.0002068	0.3285126	
9/6/04	21.1	21.7	20.6	97.7	97.7	0	0	0	0	2.451182	2.5023227	2.5959699	2.4265523	0.1532411	0.0005650	2.5017577	0.1185627	0.067	0	0.5996170	0.599617	0.0002446	0.0009175	
9/7/00	20.6	21.2	20.2	99.6	99.6	0	0	0	0	2.452363	2.4265523	2.4870053	2.3673876	0.1491777	8.09066E-05	2.4264714	0.1219201	0.067	0	0.6124167	0.612416	0.0002497	0.0002818	
9/7/00	19.8	20.6	19.4	100	100	0	0	0	0	2.454094	2.3190512	2.3673876	2.2528310	0.1433831	0	2.3190512	0.1268019	0.067	0	0.6326033	0.632603	0.0002569	0.0001751	
9/7/00	20.9	24.8	19.9	94.7	94.7	124.5	0.056025	17.7777	17.7777	2.451576	2.4768394	3.1302352	2.1973933	0.1518764	0.0014073	2.4754320	0.1197309	0.067	0.048181	0.6041543	0.652335	0.0002660	0.0199338	
9/7/00	28.9	30.8	26.8	63.3	63.3	771.55	0.347198	124.444	124.444	2.432767	3.9825871	4.4416910	3.5237195	0.2298086	0.0145235	3.9680635	0.0612000	0.067	0.298589	0.3432028	0.641792	0.0002638	0.9320277	
9/7/00	31.8	32.4	31.4	51.7	51.7	866.65	0.389993	17.7777	17.7777	2.425762	4.7190674	4.8633111	4.5439985	0.2663365	0.0226872	4.6963801	0.0366041	0.067	0.335393	0.2137340	0.549127	0.0002263	1.8448343	
9/7/00	32.4	32.8	31.6	49.5	49.5	357.866	0.16104	53.3333	53.3333	2.424503	4.8633111	4.9739919	4.6483496	0.2733929	0.0242964	4.8390147	0.0320313	0.067	0.138494	0.1883446	0.326839	0.0001348	0.5950525	
9/7/00	25.0	27.6	23.7	84.5	84.5	3.91666	0.001763	0	0	2.441935	3.1709239	3.6927819	2.9306073	0.1884304	0.0051331	3.1657907	0.0909026	0.067	0.001515	0.4846951	0.486210	0.0001991	0.0058584	
9/7/00	22.5	23.3	22.1	96.3	96.3	0	0	0	0	2.447720	2.7366397	2.8608211	2.660893	0.1657042	0.0009569	2.7356828	0.1084414	0.067	0	0.5594440	0.559444	0.0002285	0.0013476	
9/8/00	21.4	22.1	21.1	99.6	99.6	0	0	0	0	2.450356	2.5565846	2.660893	2.4870053	0.1561408	9.86526E-05	2.5564860	0.1161537	0.067	0	0.5902333	0.590233	0.0002408	0.0002969	
9/8/00	20.8	21.6	20.6	100	100	0	0	0	0	2.451891	2.4566163	2.4870053	2.4265523	0.1507920	0	2.4566163	0.1205696	0.067	0	0.6072840	0.607284	0.0002476	0.00085	

Date /Time	TMP (°C)	TM Pmax (°C)	TM Pmin (°C)	RH (%)	RH (%)	St. solar radiation MJ/m ² /3hr	W N D Wind Dir (D eg)	Rai nfall (mm)	Win d speed (km/h)	U2, Wind speed (m/sec)	Lam da (late heat) MJ/kg	e*, vapor pressure, kPa	e*max, kPa	e*min, kPa	Delta, Gradi ent, kPa/°C	Dbar, kPa	e'd, dew point pressure, kPa	Epsilo n, net emmiv ity	Gam ma, Psych rometr ic consta nt	Sh, net short wave radiation, MJ/m ² /3hr	Ln, Long wave radiation, MJ/m ² /3hr	Rn, net radiation, MJ/m ² /hr	Rn, net radiation, mm/3 hr	Ep, net evapo ration, mm/3 hr
9/8/04	22.4	26.4	20.2	0.950	0.950	123.59	93.75	0	0.26	17.7	2.44	2.709	3.441	2.367	0.164	0.001	2.707	0.109	0.067	0.04	0.564	0.61	0.000	0.018
6:00				0.666	0.666	533.3	75		6.666	7777	8113	0.824	7464	3.876	2462	4329	6494	6308		7807	3067	2114	2500	9970
9/8/04	30.5	32.7	28.7	0.615	0.615	778.295	17.24	0	1.33	88.8	2.42	4.362	4.754	3.936	0.249	0.016	4.366	0.047	0.067	0.30	0.272	0.57	0.000	0.721
6:00				0.55	0.55	433.3	24.8		3.333	8888	8832	9406	7753	7535	7729	7094	2311	4626		1253	4435	3697	2362	5757
9/8/04	32.9	34.1	31.6	0.520	0.520	882.065	18.14	0	1.6	106.6	2.42	5.016	5.348	4.648	0.280	0.023	4.992	0.027	0.067	0.34	0.161	0.50	0.000	1.130
12:00				0.05	0.05	366.7	1.42			6666	3205	0.575	9488	3496	8330	9685	0.889	1982		1475	0.802	2556	2073	7574
9/8/04	29.7	34.1	24.4	0.627	0.627	330.673	17.10	3.5	1.06	71.1	2.43	4.186	5.348	3.056	0.240	0.015	4.170	0.054	0.067	0.12	0.307	0.43	0.000	0.560
15:00				0.666	0.666	383.3	8.8	6	6.666	1111	0.720	6074	9488	3126	0.158	6477	9596	0.790		7858	1657	5024	1789	5947
9/8/04	23.0	24.4	22.5	0.973	0.973	4.9	11.9	0	0	0	2.44	2.823	3.056	2.725	0.170	0.000	2.822	0.104	0.067	0.00	0.544	0.54	0.000	0.001
18:00				0.35	0.35	205.8	9.8				6500	6293	3126	5876	2936	7661	8632	7806		1896	3456	6241	2232	0.873
9/8/04	21.9	22.5	21.3	0.999	0.999	0	11.43	0	0	0	2.44	2.627	2.725	2.533	0.159	2.191	2.627	0.113	0.067	0	0.577	0.57	0.000	0.000
21:00				0.67	0.67	7	7				9294	8588	5876	2049	9370	16E-	8369	0.515		1475	9867	7986	2359	1942
9/9/04	21.2	21.7	21.1	1.00	1.00	0	11.39	0	0	0	2.45	2.528	2.595	2.487	0.154	0	2.528	0.117	0.067	0	0.595	0.59	0.000	0.000
6:00				0.999	0.999	0	0				0.789	0.349	9699	0.053	6162	0	0.349	4.028		0	0.971	5097	2428	1694
9/9/04	21.5	21.7	21.3	0.999	0.999	0	13.21	0	0	0	2.45	2.564	2.595	2.533	0.156	2.137	2.564	0.115	0.067	0	0.588	0.58	0.000	0.000
3:00				0.916	0.916	0	0.8				0.238	4.197	9699	2049	5588	16E-	3983	8076		0	0.874	8874	2403	1960
9/9/04	21.9	23.3	21.5	0.969	0.969	54.9	18.75	0.2	0	0	2.44	2.641	2.860	2.487	0.160	0.000	2.640	0.112	0.067	0.02	0.575	0.59	0.000	0.001
6:00				0.9	0.9	705.9	2.2	5			9097	2465	8211	0.053	6485	8289	4176	5089		1246	8626	7108	2438	2254
9/9/04	25.6	27.4	24.4	0.816	0.816	352.828	17.46	0	1.06	71.1	2.44	3.295	3.607	3.126	0.194	0.006	3.289	0.086	0.067	0.13	0.462	0.59	0.000	0.259
6:00				0.966	0.966	95.883	9.7		6.666	1111	0.401	7700	3883	3126	8823	1306	6394	0.769		6591	9789	9570	2456	7381
9/9/04	27.1	28.7	25.2	0.749	0.749	654.698	14.97	0	2.13	142.2	2.43	3.566	3.936	3.205	0.209	0.008	3.577	0.075	0.067	0.25	0.412	0.66	0.000	0.704
12:00				0.67	0.67	883.3	7.7		3.333	2222	7016	3105	7535	7122	7693	9399	3705	2048		3439	3175	5757	2731	1166
9/9/04	26.8	28.3	26.5	0.722	0.722	311.766	16.5	0	1.06	71.1	2.43	3.534	3.846	3.361	0.207	0.009	3.524	0.077	0.067	0.12	0.421	0.54	0.000	0.402
15:00				0.67	0.67	766.7	5.7		6.666	1111	7607	0.848	4613	4398	1060	9949	0.899	1841		0.653	7618	2415	2225	8898
9/9/04	26.8	28.3	26.5	0.67	0.67	766.7	5.7		6.666	1111	7607	0.848	4613	4398	1060	9949	0.899	1841		0.653	7618	2415	2225	8898
15:00				0.67	0.67	766.7	5.7		6.666	1111	7607	0.848	4613	4398	1060	9949	0.899	1841		0.653	7618	2415	2225	8898

Date /Time	TMP (°C)	TM Pmax (°C)	TM Pmin (°C)	RH (%)	RH (%)	St. solar radiation MJ/m ² /3hr	W D Wind Dir (Deg)	Rai fall (mm)	Win speed (km/hr)	U2, Wind speed (m/sec)	Lam da (late heat) MJ/kg	e*, vapor pressure, kPa	e*max, kPa	e*min, kPa	Delta, Grad ent, kPa/°C	Dbar, kPa	e'd, dew point vapor pressure, kPa	Epsilo n, net emmiv sivity	Gam ma, P-sychrometric constant	Sh, net short wave radiation, MJ/m ² /3hr	Ln, Long wave radiation, MJ/m ² /3hr	Rn, net radiation, MJ/m ² /3hr	Rn, net radiation, mm/3hr	Ep, net evaporation, mm/3hr
9/9/00	23.4	26	21.3	0.85	85	7.85	25	0	0	0	2.44	3.361	2.533	0.173	0.004	2.873	0.102	0.067	0.000	0.535	0.53	0.000	0.005	
9/9/00	20.5	21.3	19.8	0.965	96.5	0	35	0	0	0	2.45	2.533	2.309	0.148	0.000	2.413	0.122	0.067	0	0.614	0.61	0.000	0.001	
9/10/00	19.4	19.8	19.4	0.999	99.9	0	35	0	0	0	2.45	2.426	2.252	0.143	1.949	2.319	0.126	0.067	0	0.630	0.63	0.000	0.000	
9/10/00	20.2	21.3	19.8	0.999	99.9	0.029	18	0	0.26	17.7	2.45	2.533	2.252	0.146	1.994	2.374	0.124	0.067	0.02	0.621	0.64	0.000	0.000	
9/10/00	25.2	27.2	22.5	0.748	74.8	0.249	12	0	1.6	106.	2.44	3.692	2.725	0.190	0.008	3.200	0.089	0.067	0.21	0.479	0.69	0.000	0.517	
9/10/00	16.6	16.6	16.6	0.666	66.6	0.933	27	8.7	0.666	6666	1463	8912	7819	5876	3962	0.657	8255	5280	4372	6478	3020	2838	0.863	
9/10/00	28.9	29.5	28.3	0.611	61.1	0.319	17	0	1.6	106.	2.43	4.122	3.846	0.229	0.015	3.967	0.061	0.067	0.27	0.343	0.61	0.000	0.863	
9/10/00	28.3	29.5	26.8	0.649	64.9	0.131	13	0	0	0	2.43	4.028	3.523	0.223	0.013	3.840	0.065	0.067	0.11	0.365	0.47	0.000	0.013	
9/10/00	22.5	24.8	21.3	0.939	93.9	0.001	11	0	0	0	2.44	3.130	2.533	0.165	0.001	2.732	0.108	0.067	0.00	0.560	0.56	0.000	0.002	
9/10/00	20.4	21.3	20.4	0.999	99.9	0	11	0	0	0	2.45	2.487	2.367	0.148	2.022	2.406	0.122	0.067	0	0.615	0.61	0.000	0.000	
9/11/00	20.0	21.3	19.8	1	100	0	11	0	0	0	2.45	2.487	2.309	0.144	0	2.347	0.125	0.067	0	0.625	0.62	0.000	0.000	
9/11/00	20.5	20.6	20.2	1	100	0	11	0	0	0	2.45	2.426	2.367	0.148	0	2.416	0.122	0.067	0	0.614	0.61	0.000	0.000	
9/11/00	20.8	22.5	19.8	0.993	99.3	0.034	58	0	0	0	2.45	2.792	2.309	0.151	0.000	2.461	0.120	0.067	0.02	0.606	0.63	0.000	0.000	
9/11/00	33.3	33.3	33.3	0.666	66.6	0.833	418	8	0.8	3333	1812	6565	4897	4882	0.625	1615	4969	3517	9599	4617	6060	2594	3960	
9/11/00	25.5	28.3	22.5	0.839	83.9	0.193	15	0	0.8	53.3	2.44	3.779	2.792	0.193	0.005	3.271	0.086	0.067	0.16	0.466	0.63	0.000	0.169	
9/11/00	66.6	67	66.6	0.833	83.3	0.433	245	4.7	0.8	3333	0.637	9303	4897	8778	2634	0.005	0.250	0.067	6190	2239	2414	2591	4616	
9/11/00	67	67	66.6	0.833	83.3	0.433	245	4.7	0.8	3333	0.637	9303	4897	8778	2634	0.005	0.250	0.067	6190	2239	2414	2591	4616	

Date /Time	TMP (°C)	TM Pmax (°C)	TM Pmin (°C)	RH (%)	RH (%)	St. solar radiation MJ/m ² /3hr	W N D Wind Dir (D eg)	Rai nfall (mm)	Win d speed, km/hr	U2, Wind speed, m/sec	Lam da nt heat) MJ/kg	e*, vapor pressure, kPa	e*max, kPa	e*min, kPa	Delta, Gradi ent, kPa/m C	Dbar, kPa	e'd, dew point pressure, kPa	Epsilo n, net emmivivity	Gam ma, Psychrometric constant	Sh, net wave radiation, MJ/m ² /3hr	Ln, Long wave radiation, MJ/m ² /3hr	Rn, net radiation, MJ/m ² /hr	Rn, net radiation, mm/3 hr	Ep, net evaporation, mm/3 hr
9/11/04 12:00	28.9	29.9	28	0.665	66.333	489.220	20.78	0	1.6	106.666	2.43	4.001	4.218	3.779	0.230	0.013	3.888	0.060	0.067	0.339	5624.01	0.52	0.000	0.735
9/11/04 15:00	28.1	29.1	26	0.663	66.333	307.833	11.78	0	1.33	88.888	2.43	3.813	4.028	3.441	0.221	0.012	3.800	0.067	0.067	0.372	8986.05	0.49	0.000	0.597
9/11/04 18:00	22.6	24.8	21	0.914	91.166	0.002	35.72	0	0	0	2.44	2.744	3.130	2.533	0.166	0.002	2.742	0.108	0.067	0.558	3286.45	0.56	0.000	0.003
9/11/04 21:00	20.9	21.7	20	0.996	66.666	0	35.72	0	0	0	2.45	2.481	2.595	2.426	0.152	8.370	2.481	0.119	0.067	0.602	9912.49	0.60	0.000	0.000
9/12/00 00:00	21.2	22.1	20	0.829	82.67	0	19.73	0	0.26	17.777	2.45	2.517	2.660	2.367	0.154	0.004	2.513	0.118	0.067	0.597	8207.24	0.59	0.000	0.059
9/12/00 03:00	19.4	20.2	18	0.781	78.166	0	20.86	0	1.33	88.888	2.45	2.255	2.367	2.156	0.139	0.004	2.250	0.129	0.067	0.642	9458.31	0.64	0.000	0.344
9/12/00 06:00	18.8	19.4	18	0.700	70.67	0.024	12.7	0	2.66	17.777	2.45	2.179	2.252	2.156	0.135	0.006	2.172	0.133	0.067	0.655	6095.55	0.67	0.000	0.933
9/12/00 09:00	22.1	22.9	20	0.527	52.333	0.189	15.67	0	3.2	213.333	2.44	2.662	2.792	2.426	0.161	0.012	2.650	0.112	0.067	0.574	73.03	0.73	0.000	1.797
9/12/00 12:00	24.8	26.3	23	0.479	47.9	0.263	24.14	0	1.86	124.444	2.44	3.145	3.361	2.930	0.187	0.016	3.129	0.092	0.067	0.491	4627.28	0.71	0.000	1.242
9/12/00 15:00	24.8	26.3	23	0.490	49.05	0.133	20.06	0	0.53	35.555	2.44	3.145	3.361	2.860	0.187	0.015	3.129	0.092	0.067	0.491	4627.28	0.71	0.000	0.355
9/12/00 18:00	18.2	16.6	16	0.832	83.333	0.002	30.23	0	0	0	2.45	2.092	2.487	1.913	0.131	0.003	2.088	0.137	0.067	0.669	3761.72	0.67	0.000	0.005
9/12/00 21:00	16.6	16.6	16	0.980	98.333	0	30.35	0	0	0	2.46	1.889	1.913	1.865	0.119	0.000	1.888	0.147	0.067	0.701	1819.81	0.70	0.000	0.000
9/13/00 00:00	17.2	17.5	17	0.955	95.666	0	26.55	0	0.26	17.777	2.46	1.966	1.999	1.950	0.124	0.000	1.965	0.143	0.067	0.689	3729.5	0.68	0.000	0.014
9/13/00 03:00	16.0	17.1	15	0.867	86.666	0	32.46	0	0	0	2.46	1.824	1.950	1.727	0.116	0.002	1.821	0.151	0.067	0.712	7864.87	0.71	0.000	0.004

Date /Time	TMp (°C)	TM Pmax (°C)	TM Pmin (°C)	RH (%)	RH (%)	solar radiation MJ/m ² /hr	St. solar radiation MJ/m ² /3hr	Wind speed (m/s)	Rainfall (mm)	Wind speed (km/hr)	U2, Wind speed (m/sec)	Lambda (late heat) MJ/kg	e ^s , vapor pressure, kPa	e ^{max} , kPa	e ^{min} , kPa	Delta, Gradient, kPa/°C	Dbar, kPa	e ^d , dew point pressure, kPa	Epsilon, net emissivity	Gamm, Psychrometric constant	Sh, short wave radiation, MJ/m ² /3hr	Ln, Long wave radiation, MJ/m ² /3hr	Rn, net radiation, MJ/m ² /hr	Rn, net radiation, mm ³ /hr	Ep, net evaporation, mm ³ /hr
9/13/04	15.8	17.0	14.0	87.5	87.0	71.5	0.032	19	0	0.26	17.7	2.46	1.799	2.051	1.640	0.114	0.002	1.796	0.152	0.067	0.02	0.716	0.74	0.000	0.041
9/13/04	33.3	39.0	27.0	51.6	51.6	66.6	0.205	1.5	0	6.666	7.777	3.617	0.200	0.472	5.784	8.033	3.041	7.158	3.417	0.067	0.22	7.623	4.458	3.021	3.869
9/13/04	22.2	24.0	19.0	46.6	46.6	61.9	0.278	2.0	0	2.4	1.60	2.44	2.654	2.983	2.197	0.162	0.013	2.670	0.111	0.067	0.23	0.571	0.81	0.000	1.503
9/13/04	26.3	27.0	25.0	30.3	30.3	74.7	0.336	1.5	0	1.06	71.1	2.43	3.428	3.607	3.205	0.201	0.023	3.404	0.081	0.067	0.28	0.443	0.73	0.000	0.969
9/13/04	33.3	33.0	33.0	83.3	83.3	0.66	0.18	7.2	8	6.666	11.1	8.827	2.470	3.883	7.122	6.919	5.449	7.021	6.743	0.067	0.28	2.315	23.46	3.002	5.214
9/13/04	25.8	26.0	24.0	38.4	38.4	31.2	0.140	2.5	0	0.26	17.7	2.44	3.321	3.523	2.983	0.196	0.020	3.301	0.085	0.067	0.12	0.461	0.58	0.000	0.227
9/13/04	17.9	21.0	16.0	82.7	82.7	3.91	0.001	3.5	0	0	0	2.45	2.053	2.487	1.865	0.128	0.003	2.049	0.139	0.067	0.00	0.675	0.87	0.000	0.005
9/13/04	16.6	16.0	16.0	16.6	16.6	7.16	0.666	7.2	0	0	0	8.698	1.992	0.053	2.661	8.932	7.610	4.381	5.779	0.067	0.00	0.891	7.364	2.754	9.531
9/13/04	15.8	16.0	15.0	96.5	96.5	0	0	3.5	0	0	0	2.46	1.795	1.865	1.727	0.114	0.000	1.794	0.152	0.067	0	0.716	0.71	0.000	0.001
9/14/00	14.8	15.0	14.0	99.7	99.7	0	0	7.2	0	0	0	5.899	1.690	1.727	1.683	0.108	5.116	1.690	0.157	0.067	0	0.733	0.73	0.000	0.000
9/14/04	6.66	6.0	6.0	6.66	6.66	7.623	0	8	0	0	0	6.62	6.62	4.288	5.115	7.237	4.11E-05	7.111	9.617	0.067	0	3.114	3.11	2.973	2.751
9/14/04	14.2	14.0	13.0	100	100	0	0	3.5	0	0	0	2.46	1.624	1.683	1.567	0.104	0	1.624	0.161	0.067	0	0.743	0.74	0.000	0.000
9/14/04	15.4	18.0	13.0	98.9	98.9	86.2	0.038	2.9	0	0	0	4.483	1.757	2.156	1.567	0.112	0.000	1.757	0.154	0.067	0.03	0.722	0.75	0.000	0.000
9/14/04	6.66	7.0	6.0	83.3	83.3	6.66	0.82	9.5	0	0	0	2.44	2.855	3.607	2.252	0.171	0.008	2.855	0.103	0.067	0.23	0.540	0.77	0.000	5.196
9/14/04	23.2	27.0	19.0	70.5	70.5	60.3	0.271	1.9	0	1.33	88.8	6.067	0.716	3.883	8.310	9.477	7.756	2.959	8.064	0.067	0.23	6.202	4.342	3.165	6.679
9/14/04	6.66	6.0	6.0	5.0	5.0	9.33	0.77	8.0	0	3.333	8.888	4.4	4.38	0.03	0.02	0.14	0.78	0.59	0.34	0.067	0.29	0.93	0.49	0.66	0.34
9/14/04	29.1	30.0	27.0	42.0	42.0	77.2	0.347	1.5	0	1.6	10.6	2.43	4.036	4.441	3.607	0.232	0.023	4.013	0.069	0.067	0.29	0.335	0.63	0.000	1.273
9/14/04	33.3	33.0	33.0	83.3	83.3	5.5	0.648	0	0	6.666	6.666	2.216	6.459	6.910	3.883	5.201	3.087	3.371	5.335	0.067	0.29	3.287	4.305	2.607	2.971
9/14/04	28.8	30.0	26.0	42.0	42.0	3.38	0.152	1.0	0	0.26	17.7	2.43	3.974	4.341	3.361	0.229	0.021	3.952	0.061	0.067	0.13	0.346	0.47	0.000	0.219
9/14/04	6.66	6.0	6.0	95.5	95.5	2.5	2.13	2.8	8	6.666	7.777	2.845	9.161	3.906	4.398	4.234	9.723	9.438	6.518	0.067	0.13	0.364	0.939	1.960	6.815
9/14/04	20.3	23.0	18.0	82.1	82.1	3.91	0.001	2.7	0	0	0	2.45	2.394	2.860	2.156	0.147	0.004	2.389	0.123	0.067	0.00	0.618	0.62	0.000	0.006
9/14/04	33.3	33.0	33.0	1	1	6.66	0.763	9.8	0	0	0	2.874	3.463	8.211	6.019	4.454	4.905	8.557	5.717	0.067	0.00	8.843	0.400	2.529	3.117
9/14/04	18.1	18.0	17.0	95.5	95.5	0	0	2.7	0	0	0	2.45	2.085	2.103	2.051	0.130	0.000	2.084	0.137	0.067	0	0.669	0.66	0.000	0.001
9/14/04	6.66	6.0	6.0	35	35	0	0	9.8	0	0	0	8.108	7.180	2.450	0.472	6.785	9.658	7.522	8.586	0.067	0	8.197	9.819	2.724	6.448
9/14/04	6.66	6.0	6.0	5	5	0	0	9.8	0	0	0	8.108	7.180	2.450	0.472	6.785	9.658	7.522	8.586	0.067	0	8.197	9.819	2.724	6.448

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9/15 /04 0:00	17.2	17.	17.	0.993	99.	0	28 0.5	0	0	0	2.46 0312	1.966 9869	1.999 9869	1.950 0432	0.124 1185	0.000 1283	1.866 4400	0.143 6782	0.067 0	0.689 1940	0.68 9194	0.000 2801	0.000 3855	
9/15 /04 3:00	16.5	17.	16.	1	100	0	28 1.3	0	0	0	2.46 1846	1.887 1950	1.950 0432	1.865 2661	0.119 7169	0	1.887 1514	0.147 6769	0.067 0	0.702 0544	0.70 2054	0.000 2851	0.000 1828	
9/15 /04 6:00	17.9	21	16.	0.989	98.	86.2	29 3.9	0	0	0	2.45 8698	2.053 1992	2.487 0053	1.885 2661	0.128 8932	0.000 2212	2.052 9780	0.139 4049	0.067 0	0.675 0113	0.70 8396	0.000 2881	0.000 5290	
9/15 /04 9:00	26.0	29.	22.	0.668	66.	57.3	10 6.1	0	0.53 3333	35.5 5555	3.374 9456	4.028 8844	4.028 8844	0.198 9444	0.011 3064	0.067 4033	0.363 2458	0.067 0	0.450 1533	0.67 2117	0.000 2755	0.000 0.241		
9/15 /04 12:00	30.5	31.	29.	0.473	47.	729.	16 4.3	0	1.6 6666	106. 67	2.42 8792	4.387 1145	4.543 9995	4.122 8854	0.249 9796	0.022 8011	4.364 3134	0.047 5288	0.067 0	0.272 8722	0.55 5150	0.000 2285	1.176 6313	
9/15 /04 15:00	30.5	31.	28.	0.510	51.	345.	24 0.0	0	0.26 6666	17.7 7777	2.42 8832	4.382 9406	4.648 3496	3.936 7535	0.249 7729	0.021 0048	4.361 9357	0.047 6065	0.067 0	0.273 2697	0.40 6829	0.000 1675	0.196 4124	
9/15 /04 18:00	22.8	26	21.	0.849	84.	4.9	35 0.2	0	0	0	2.44 7169	3.361 4398	3.361 4398	2.533 2049	0.167 7637	0.004 4504	2.771 1807	0.106 9439	0.067 0	0.553 4615	0.55 5357	0.000 2269	0.005 6157	
9/15 /04 21:00	20.2	21	19.	0.951	95.	0	35 0.2	0	0	0	2.45 3150	2.377 1599	2.487 0053	2.309 4882	0.146 5197	0.001 1551	2.376 0048	0.124 1998	0.067 0	0.621 0418	0.62 1041	0.000 2531	0.001 7611	
9/16 /04 0:00	19.1	19.	18.	0.987	98.	0	35 0.2	0	0	0	2.45 5786	2.218 0409	2.252 6310	2.156 6019	0.137 9053	0.000 2682	2.217 7727	0.131 5093	0.067 0	0.647 6399	0.64 7064	0.000 2637	0.000 5657	
9/16 /04 3:00	18.6	19	18.	1	100	0	35 0.2	0	0	0	2.45 6888	2.154 3933	2.197 3933	2.103 2450	0.134 4346	0	2.154 3553	0.134 5118	0.067 0	0.658 2069	0.65 8206	0.000 2679	0.000 1787	
9/16 /04 6:00	19.3	21	18.	0.996	99.	64.7	32 6.7	0	0.26 6666	17.7 7777	2.45 5393	2.241 1816	2.487 0053	2.103 2450	0.139 1632	8.032 94E-05	2.241 1013	0.130 4156	0.067 0	0.643 7198	0.66 8765	0.000 2723	0.001 3985	
9/16 /04 9:00	25.2	27.	23.	0.806	80.	373.	14 2.0	0	0	0	2.44 1424	3.212 7819	3.692 8211	2.860 8211	0.190 5608	0.006 3569	3.205 7160	0.089 3368	0.067 0	0.477 7320	0.62 2282	0.000 2548	0.007 1968	
9/16 /04 12:00	28.2	29.	27.	0.669	66.	453.	13 7.3	0	0	0	2.43 4223	3.842 7386	4.122 8854	3.607 3883	0.222 7698	0.012 9772	3.829 9772	0.066 0154	0.067 0	0.367 6742	0.54 3339	0.000 2232	0.012 5684	
9/16 /04 15:00	29.5	30.	28.	0.618	61.	301.	19 6.4	0	0	0	2.43 1232	4.134 7686	4.441 6910	3.779 9303	0.237 4290	0.015 7032	4.119 0653	0.065 8632	0.067 0	0.316 3935	0.43 3254	0.000 1782	0.014 6412	
9/16 /04 18:00	23.2	26	22.	0.905	90.	3.91	12 5.2	0	0	0	2.44 6067	2.855 0716	3.361 4398	2.660 0893	0.171 9477	0.002 8602	2.852 2114	0.103 5611	0.067 0	0.539 3427	0.54 0858	0.000 2211	0.003 5925	

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9/16 /04 21:0 0	21.0 333 33	21. 7	20. 6	0.987 7	98. 7	0	11 3.7 2	0	0	0	2.45 1340 3	2.482 1020 53	2.595 9699 94	2.426 5523 12	0.152 6940 23	0.000 3264 64	2.491 7755 89	0.119 0049 74	0.067	0	0.601 3082 91	0.60 1308 29	0.000 2452 98	0.000 6036 11
9/17 /04 0:00	20.1 333 33	20. 6	19. 4	0.992 333 33	99. 33 3	0	22 0.1 2	0	0	0	2.45 3465 2	2.357 6505 55	2.426 5523 12	2.252 8310 02	0.145 4678 39	0.000 1793 76	2.357 4711 79	0.125 0431 79	0.067	0	0.624 1231 13	0.62 4123 11	0.000 2543 84	0.000 4221 86
9/17 /04 3:00	18.8 1666 5	19. 7	18. 7	1 333 33	100 33 3	0	26 0.2 3	0	0	0	2.45 6495 15	2.176 9140 53	2.197 3933 24	2.156 6019 8	0.135 6655 79	0 0	2.176 9140 53	0.133 4388 34	0.067	0	0.654 4487 93	0.65 4448 79	0.000 2664 16	0.000 1783 4
9/17 /04 6:00	20.1 1666 67	22. 1	19. 1	0.992 333 33	99. 33 3	23 8.6 3	23 0.2 3	0	0	0	2.45 3504 55	2.355 2217 48	2.660 0893 35	2.197 3933 24	0.145 3367 98	0.000 1862 04	2.355 0355 45	0.125 1542 45	0.067	0.02 1626 85	0.624 5355 35	0.64 6162 38	0.000 2633 63	0.000 4379 21
9/17 /04 9:00	22.6 8333 33	26. 3	21. 3	0.940 333 33	94. 33 3	16 6.4 5	16 0.2 7	0.26 6666 7	17.7 78	2.44 7444 65	2.756 0753 1	3.361 4398 29	2.533 2049 81	2.166 7313 15	0.166 7585 69	0.001 001 41	2.754 3167 41	0.107 6541 2	0.067	0.09 2570 4	0.556 2592 63	0.64 8829 66	0.000 2651 05	0.022 9961 31
9/17 /04 12:0 0	29.5 1666 5	31. 2	27. 6	0.649 833 33	64. 33 3	13 4.3 3	13 0.16 3	1.6 6666 67	106 67	2.43 1232 45	4.134 7686 7	4.543 9995 87	3.692 7819 6	0.237 4290 82	0.237 4290 82	0.014 4212 32	4.120 3474 39	0.065 8190 54	0.067	0.27 3550 95	0.316 1430 76	0.58 9694 03	0.000 2425 49	0.774 9577 5
9/17 /04 15:0 0	30.3 6666 67	31. 2	28. 3	0.614 1666 67	61. 416 67	82. 96 7	82. 96 7	0.26 6666 7	17.7 78	2.42 9304 3	4.333 1218 64	4.543 9995 87	3.846 4613 72	3.846 4613 72	0.247 3030 27	0.016 1865 98	4.316 9352 66	0.049 1186 99	0.067	0.12 0663 7	0.281 2080 67	0.40 1861 77	0.000 1654 23	0.152 5650 96
9/17 /04 18:0 0	23.8 1666 67	26. 4	22. 1	0.913 333 33	91. 33 3	94. 2	94. 2	0	0	0	2.44 4808 2	3.441 7464 35	2.660 0893 35	2.660 0893 35	0.176 8368 33	0.002 6441 29	2.945 6401 76	0.099 7198 56	0.067	0.00 1515 75	0.523 0847 19	0.52 4600 47	0.000 2145 77	0.003 2563 7
9/17 /04 21:0 0	21.5 1666 67	21. 7	21. 7	0.994 4	99. 4	0	94. 2	0	0	0	2.45 0199 15	2.567 0360 53	2.595 9699 94	2.487 0053 97	0.156 6884 14	0.000 1524 89	2.566 8635 64	0.115 6990 46	0.067	0 0	0.588 4548 63	0.58 8454 86	0.000 2401 66	0.000 3661 49
9/18 /04 0:00	20.7 3333 33	21. 6	20. 6	1 333 33	100 33 3	0	94. 2	0	0	0	2.45 2048 6	2.446 5590 16	2.487 0053 97	2.426 5523 12	0.150 2523 18	0 0	2.446 5590 16	0.121 0192 21	0.067	0 0	0.608 9960 94	0.60 8996 09	0.000 2483 62	0.000 1717 68
9/18 /04 3:00	20.2 6666 67	20. 6	20. 2	1 333 33	100 33 3	0	95. 6	0	0	0	2.45 3150 4	2.377 1599 83	2.426 5523 12	2.367 3876 98	0.146 5197 63	0 0	2.377 1599 83	0.124 1474 21	0.067	0 0	0.620 7795 64	0.62 0779 56	0.000 2530 54	0.000 1736 49
9/18 /04 6:00	21.2 1666 67	24. 8	19. 8	0.987 1666 67	98. 716 67	12 3.7 3	12 0.3 3	0	0	0	2.45 0907 45	2.520 2971 5	2.983 9174 77	2.309 4882 49	0.154 2026 24	0.000 3396 6	2.519 9574 9	0.117 7587 84	0.067	0.04 0602 75	0.596 4958 1	0.63 7098 56	0.000 2599 44	0.000 6280 83
9/18 /04 9:00	29.0 3333 5	32. 6	25. 4	0.693 1666 67	69. 316 67	17 4.8 5	17 4.8 5	1.33 3333 3	88.8 89	2.43 888 95	4.017 2664 32	4.754 7753 96	3.282 7711 7	3.282 7711 7	0.231 5486 98	0.012 3309 36	4.004 9354 96	0.059 8273 11	0.067	0.25 9135 2	0.336 6117 81	0.59 5746 98	0.000 2449 2	0.565 2401 21
9/18 /04 12:0 0	33.6 3333 33	34. 9	32. 4	0.501 6666 67	50. 166 67	12 8.9 2	12 8.9 2	1.86 6666 7	124 44	2.42 1591 7	5.211 6214 01	5.591 6786 68	4.863 3111 98	0.290 3120 68	0.290 3120 68	0.026 0503 5	5.185 5710 52	0.021 1941 15	0.067	0.30 2388 9	0.126 6455 75	0.42 9034 48	0.000 1771 7	1.394 6840 55
9/18 /04 15:0 0	33.1 6666 67	34. 9	31. 6	0.534 5	53. 45	15 7.9 7	15 7.9 7	0.53 3333 3	35.5 56	2.42 2693 5	5.077 3638 97	5.591 6786 68	4.648 3496 8	0.283 8101 37	0.023 8336 66	5.053 5302 31	0.025 2791 83	0.067	0.14 7214 8	0.150 1390 54	0.29 7353 85	0.000 1227 37	0.384 6325 14	

Date /Time	TMP (°C)	TM Pmax (°C)	TM Pmin (°C)	RH (%)	RH (%)	St. solar radiation MJ/m ² /3hr	W N D Wind Dir (D eg)	Rainfall (mm)	Wind speed (km/hr)	U2, Wind speed (m/sec)	Lambda (late heat) MJ/kg	e*, vapor pressure, kPa	e*max, kPa	e*min, kPa	Delta, Gradient, kPa/C	Dbar, kPa	e'd, dew point pressure, kPa	Epsilon, net emissivity	Gamm, Psychrometric constant	Sh, net short wave radiation, MJ/m ² /3hr	Ln, Long wave radiation, MJ/m ² /3hr	Rn, net radiation, MJ/m ² /hr	Rn, net radiation, mm/3 hr	Ep, net evaporation, mm/3 hr
9/18/00	25.4	28.3	24	0.874	87.166667	4.9	26	0	0	0	2.44	3.253	3.846	2.983	0.192	0.004	3.249	0.087	0.067	0.00	0.469	0.47	0.000	0.004
9/18/00	18.0	18.0	18.0	416	7.2	205	7.2	0	0	0	0.912	4.613	4.613	9.174	7.114	2974	3894	6351	0.067	1896	9945	1890	1933	8377
9/18/00	23.5	24.5	22	0.981	98.15	0	30	0	0	0	2.44	2.904	2.983	2.792	0.174	0.000	2.903	0.101	0.067	0	0.530	0.53	0.000	0.000
9/18/00	21.0	21.0	21.0	9.4	9.4	0	9.4	0	0	0	5.398	2.653	9.174	4.897	5.306	5343	7310	4352	0.067	2937	2937	0.293	2168	7901
9/19/00	23.1	24.5	22	0.996	99.65	0	26	0	0.26	17.7	2.44	2.835	2.983	2.792	0.170	0.000	2.834	0.104	0.067	0	0.542	0.54	0.000	0.001
9/19/00	21.6	23.3	21	0.960	96.833333	0	24	3.8	0.53	35.5	2.45	2.580	2.860	2.487	0.157	0.001	2.579	0.115	0.067	0	0.586	0.58	0.000	0.027
9/19/00	22.3	24.4	21	0.961	96.67	109	27	0	0	0	2.44	2.706	3.056	2.487	0.164	0.001	2.705	0.109	0.067	0.04	0.564	0.60	0.000	0.001
9/19/00	8.333	8.333	6	116	8.333333	8	9.3	0	1.6	106	8.152	3.400	3.126	0.053	10.10	0.763	2637	7323	0.067	2492	7018	7194	2480	5197
9/19/00	28.4	30.4	26	0.741	74.133333	632	15	0	1.06	71.1	2.43	3.868	4.341	3.441	0.224	0.010	3.858	0.064	0.067	0.24	0.362	0.60	0.000	0.380
9/19/00	32.8	33.6	31	0.562	56.666667	724	19	0	1.6	106	2.42	4.973	5.201	4.648	0.278	0.021	4.952	0.028	0.067	0.28	0.168	0.44	0.000	1.021
9/19/00	33.4	34.5	31	0.494	49.45	396	16	0	1.06	71.1	2.42	5.158	5.469	4.648	0.287	0.025	5.132	0.022	0.067	0.15	0.136	0.28	0.000	0.796
9/19/00	18.0	18.0	18.0	86	7.166667	4.9	16	0	0	0	0.991	2.543	3.779	2.930	0.192	0.004	3.242	0.087	0.067	0.00	0.471	0.47	0.000	0.005
9/19/00	25.4	28.7	23	0.867	86.833333	205	3.1	0	0	0	2.44	3.247	3.779	3.033	0.192	0.004	3.242	0.087	0.067	1896	1577	3054	1937	0.005
9/19/00	24.0	24.3	23	0.961	96.133333	0	12	0.7	0.8	53.3	2.44	2.998	3.056	2.930	0.179	0.001	2.997	0.097	0.067	0	0.513	0.51	0.000	0.039
9/19/00	8.333	8.333	7	133	8.333333	0	8.9	6	0	33	4.139	8.751	3.126	6.073	4.815	15.74	7176	6051	0.067	0	9484	3948	2102	8208
9/20/00	22.1	22.1	21	0.996	99.67	0	68	0.2	0	0	2.44	2.660	2.725	2.595	0.161	0.000	2.659	0.111	0.067	0	0.572	0.57	0.000	0.000
9/20/00	18.0	18.0	18.0	616	6.166667	155	41	5	0	0	8.821	0.893	5.876	6.969	6.491	10.19	9873	6674	0.067	0	4.592	2.459	2337	2942
9/20/00	21.1	21.3	21	100	100	0	71	0	0	0	2.45	2.510	2.533	2.487	0.153	0	2.510	0.118	0.067	0	0.598	0.59	0.000	0.000
9/20/00	22.2	25.6	21	0.974	97.666667	148	77	0	0	0	2.44	2.676	3.282	2.487	0.162	0.000	2.675	0.110	0.067	0.06	0.569	0.63	0.000	0.001
9/20/00	29.7	32.8	26	0.680	68.016667	701	18	0	1.6	106	2.43	4.186	4.754	3.523	0.240	0.013	4.173	0.063	0.067	0.27	0.306	0.57	0.000	0.705
9/20/00	6.666	6.666	8	116	9.666667	885	0.7	0	0	66.66	0.720	6.074	7.753	7.195	0.158	2.386	3687	9964	0.067	1661	6967	8387	2379	3774
9/20/00	33.5	34.1	32	0.519	51.933333	777	14	0	1.86	124	2.42	5.192	5.348	4.973	0.289	0.024	5.167	0.021	0.067	0.30	0.129	0.43	0.000	1.331
9/20/00	6.666	6.666	8	8.6	8.633333	45	8.6	0	0.666667	44.44	1.749	2.551	9.488	9.919	3.756	80.94	4456	7517	0.067	15	28	0.08	1778	5012
9/20/00	12.0	12.0	12.0	33	33	52	87	93	7	44	1	52	87	93	67	68	85	71		15	28	0.08	62	3

Date /Time	TMP (°C)	TM Pmax (°C)	TM Pmin (°C)	RH (%)	RH (%)	St. solar radiation MJ/m ² /3hr	Wind speed m/sec	U2, Wind speed m/sec	Lam da (late nit heat) MJ/kg	e*, vapor pressure kPa	e*ma x kPa	e*min , kPa	Delta, Gradi ent, kPa/r C	Dbar, kPa	e'd, dew point vapor pressure, kPa	Epsilo n, net emmi sivity	Gam ma, Psychrometric constant	Sh, net short wave radiation, MJ/m ² /3hr	Ln, Long wave radiation, MJ/m ² /3hr	Rn, net radiation, MJ/m ² /hr	Rn, net radiation, mm/3 hr	Ep, net evaporation, mm/3 hr
9/20 /04 15:00	33.2	34.5	30.4	53.2	66.6	360.173	3.33	3.33	2.42	5.101	5.469	4.341	0.284	0.022	5.078	0.024	0.067	0.14	0.145	0.29	0.000	0.543
9/20 /04 18:00	25.9	28.3	24.8	86.3	33.3	648.333	0	0	2.43	3.358	3.846	3.130	0.198	0.004	3.353	0.083	0.067	0.00	0.451	0.45	0.000	0.005
9/20 /04 21:00	23.6	24.4	23.3	97.6	66.6	97.766	0	0	2.44	2.924	3.056	2.860	0.175	0.000	2.924	0.100	0.067	0	0.526	0.52	0.000	0.000
9/21 /04 00:00	23.1	23.3	22.9	99.9	166.6	916.67	0	0	2.44	2.826	2.860	2.792	0.170	2.355	2.826	0.104	0.067	0	0.543	0.54	0.000	0.000
9/21 /04 03:00	22.3	22.5	22.1	100	67	7	0	0	2.44	2.692	2.725	2.660	0.163	0	2.692	0.110	0.067	0	0.566	0.56	0.000	0.000
9/21 /04 06:00	23.8	28.3	21.7	94.8	83.3	131.383	0	0	2.44	2.957	3.846	2.595	0.177	0.001	2.955	0.099	0.067	0.05	0.521	0.57	0.000	0.002
9/21 /04 09:00	31.4	33.6	29.1	61.2	61.2	728.433	1.86	1.86	2.42	4.604	5.201	4.028	0.260	0.017	4.586	0.040	0.067	0.28	0.233	0.51	0.000	1.038
9/21 /04 12:00	35.9	37.1	34.9	42.8	42.8	918.633	1.86	1.86	2.41	5.913	6.309	5.591	0.323	0.034	5.879	0.000	0.067	0.35	0.003	0.35	0.000	1.679
9/21 /04 15:00	34.0	36.6	29.1	46.8	46.8	374.516	1.06	1.06	2.42	5.324	6.139	4.028	0.295	0.027	5.297	0.017	0.067	0.14	0.106	0.25	0.000	0.825
9/21 /04 18:00	25.0	27.6	23.7	67.4	67.4	0.98.333	1.33	1.33	2.44	3.174	3.692	2.930	0.188	0.010	3.163	0.091	0.067	0.00	0.485	0.48	0.000	0.584
9/21 /04 21:00	22.5	22.9	22.1	89.8	66.6	0	0	0	2.44	2.736	2.792	2.660	0.165	0.002	2.733	0.108	0.067	0	0.559	0.55	0.000	0.003
9/22 /04 00:00	21.9	22.6	21.3	98.1	66.6	0	0	0	2.44	2.638	2.725	2.533	0.160	0.000	2.638	0.112	0.067	0	0.576	0.57	0.000	0.000
9/22 /04 03:00	21.1	21.7	20.6	100	67	0	0	0	2.45	2.510	2.595	2.426	0.153	0	2.510	0.118	0.067	0	0.598	0.59	0.000	0.000
9/22 /04 06:00	22.8	26.8	20.6	93.1	66.6	147.18	0	0	2.44	2.784	3.523	2.426	0.168	0.002	2.782	0.106	0.067	0.05	0.551	0.60	0.000	0.002
9/22 /04 09:00	31.3	33.2	28.2	56.9	56.9	734.333	1.6	1.6	2.42	4.578	5.086	3.779	0.259	0.019	4.559	0.041	0.067	0.28	0.238	0.52	0.000	0.956
9/22 /04 12:00	33.3	33.3	33.3	98.3	83.3	45.333	0	0	2.42	5.544	6.139	4.028	0.323	0.034	5.544	0.000	0.067	0.35	0.003	0.35	0.000	1.679
9/22 /04 15:00	33.2	34.5	30.4	53.2	66.6	360.173	3.33	3.33	2.42	5.101	5.469	4.341	0.284	0.022	5.078	0.024	0.067	0.14	0.145	0.29	0.000	0.543
9/22 /04 18:00	25.9	28.3	24.8	86.3	33.3	648.333	0	0	2.43	3.358	3.846	3.130	0.198	0.004	3.353	0.083	0.067	0.00	0.451	0.45	0.000	0.005
9/22 /04 21:00	23.6	24.4	23.3	97.6	66.6	97.766	0	0	2.44	2.924	3.056	2.860	0.175	0.000	2.924	0.100	0.067	0	0.526	0.52	0.000	0.000
9/23 /04 00:00	23.1	23.3	22.9	99.9	166.6	916.67	0	0	2.44	2.826	2.860	2.792	0.170	2.355	2.826	0.104	0.067	0	0.543	0.54	0.000	0.000
9/23 /04 03:00	22.3	22.5	22.1	100	67	7	0	0	2.44	2.692	2.725	2.660	0.163	0	2.692	0.110	0.067	0	0.566	0.56	0.000	0.000
9/23 /04 06:00	23.8	28.3	21.7	94.8	83.3	131.383	0	0	2.44	2.957	3.846	2.595	0.177	0.001	2.955	0.099	0.067	0.05	0.521	0.57	0.000	0.002
9/23 /04 09:00	31.4	33.6	29.1	61.2	61.2	728.433	1.86	1.86	2.42	4.604	5.201	4.028	0.260	0.017	4.586	0.040	0.067	0.28	0.233	0.51	0.000	1.038
9/23 /04 12:00	35.9	37.1	34.9	42.8	42.8	918.633	1.86	1.86	2.41	5.913	6.309	5.591	0.323	0.034	5.879	0.000	0.067	0.35	0.003	0.35	0.000	1.679
9/23 /04 15:00	34.0	36.6	29.1	46.8	46.8	374.516	1.06	1.06	2.42	5.324	6.139	4.028	0.295	0.027	5.297	0.017	0.067	0.14	0.106	0.25	0.000	0.825
9/23 /04 18:00	25.0	27.6	23.7	67.4	67.4	0.98.333	1.33	1.33	2.44	3.174	3.692	2.930	0.188	0.010	3.163	0.091	0.067	0.00	0.485	0.48	0.000	0.584
9/23 /04 21:00	22.5	22.9	22.1	89.8	66.6	0	0	0	2.44	2.736	2.792	2.660	0.165	0.002	2.733	0.108	0.067	0	0.559	0.55	0.000	0.003
9/24 /04 00:00	21.9	22.6	21.3	98.1	66.6	0	0	0	2.44	2.638	2.725	2.533	0.160	0.000	2.638	0.112	0.067	0	0.576	0.57	0.000	0.000
9/24 /04 03:00	21.1	21.7	20.6	100	67	0	0	0	2.45	2.510	2.595	2.426	0.153	0	2.510	0.118	0.067	0	0.598	0.59	0.000	0.000
9/24 /04 06:00	22.8	26.8	20.6	93.1	66.6	147.18	0	0	2.44	2.784	3.523	2.426	0.168	0.002	2.782	0.106	0.067	0.05	0.551	0.60	0.000	0.002
9/24 /04 09:00	31.3	33.2	28.2	56.9	56.9	734.333	1.6	1.6	2.42	4.578	5.086	3.779	0.259	0.019	4.559	0.041	0.067	0.28	0.238	0.52	0.000	0.956
9/24 /04 12:00	33.3	33.3	33.3	98.3	83.3	45.333	0	0	2.42	5.544	6.139	4.028	0.323	0.034	5.544	0.000	0.067	0.35	0.003	0.35	0.000	1.679

Date /Time	TMP (°C)	TM Pmax (°C)	TM Pmin (°C)	RH (%)	RH (%)	solar radiation MJ/m ² /hr	St. solar radiation MJ/m ² /3hr	Wind Dir (D)	Wind speed (m/sec)	U2, Wind speed (m/sec)	Lam da (late heat) MJ/kg	e*, vapor pressure, kPa	e*max, kPa	e*min, kPa	Delta, Gradi ent, kPa/°C	Dbar, kPa	e'd, dew point pressure, kPa	Epsilo n, net emmiv ity	Gam ma, Psychr ometr ic consta nt	Sh, net wave radiation, MJ/m ² /3hr	Ln, Long wave radiation, MJ/m ² /3hr	Rn, net radiation, MJ/m ² /hr	Rn, net radiation, mm/3 hr	Ep, net evapo ration, mm/3 hr
9/22/04 12:00	35.4	36.2	34.9	47.4	47.4	893.7	0.401903	0.1	1.6	106.666667	2.417420	5.7481868	6.0065013	5.5916786	0.3160859	0.0305032	5.7176836	0.0052365	0.06715	0.340176	0.0320176	0.377653	0.0001562	1.3168780
9/22/04 15:00	34.8	36.2	32	46.333333	46.333333	422.55	0.190148	79.7	1.0666667	71.111111	2.418837	5.5608244	6.0065013	4.7547753	0.3071137	0.0287684	5.5320559	0.0107154	0.06765	0.0650098	0.228536	9.4482E-05	0.8530985	
9/22/04 18:00	26.4	29.1	24.8	83.666667	83.666667	4.9	0.002205	14.1	0	0	2.438551	3.4519013	4.0288844	3.1302352	0.2029039	0.0059182	3.4459831	0.0801129	0.0673	0.00435	0.434362	0.0001793	0.0063332	
9/22/04 21:00	23.9	24.4	23.7	95.333333	95.333333	0	0	14.1	0	0	2.444532	2.9690249	3.0563126	2.9306073	0.1779218	0.0013969	2.9676279	0.0988247	0.06771	0	0.5192043	0.0002123	0.0017841	
9/23/04 00:00	23.3	23.7	22.9	99.833333	99.833333	0	0	14.1	0	0	2.445988	2.8608211	2.9306073	2.7924897	0.1722499	0.0002336	2.8605874	0.1032142	0.06703	0	0.5377777	0.0002198	0.0004384	
9/23/04 03:00	22.7	22.9	22.5	100	100	0	0	16.8	0	0	2.447247	2.7704897	2.7924897	2.7255876	0.1674682	0	2.7700315	0.1069922	0.06737	0	0.5534623	0.0002261	0.0001615	
9/23/04 06:00	23.8	27.2	22.1	93.931	93.931	129.416	0.058238	24.8	0.2666667	17.777778	2.444650	2.9601205	3.6073883	2.6600893	0.1774561	0.0021622	2.9579882	0.0992179	0.06725	0.0520984	0.579195	0.0002335	0.0267901	
9/23/04 09:00	31.1	33.2	28.3	60.85	60.85	705.9	0.317665	16.7	1.6	106.666667	2.427415	4.5353963	5.0864613	3.8464613	0.2573070	0.0174869	4.5179094	0.0424247	0.0673183	0.274552	0.518638	0.0002136	0.8823749	
9/23/04 12:00	35.4	35.8	34.9	45	45	831.366	0.374115	13.5	1.6	106.666667	2.417381	5.7534685	5.8761139	5.5916786	0.3163177	0.0315364	5.7219321	0.0051121	0.0679	0.0312641	0.353003	0.0001460	1.3606699	
9/23/04 15:00	34.3	36.2	32.4	49.3	49.3	339.216	0.152648	11.5	0.5333333	35.555556	2.419860	5.4288225	6.0065013	4.8633111	0.3007807	0.0275549	5.4012675	0.0146312	0.06785	0.0882677	0.219544	9.07262E-05	0.4256063	
9/23/04 18:00	22.8	27.6	21.7	88.85	88.85	2.93333	0.00132	18.2	1.6	106.666667	2.447129	2.7784348	3.6927819	2.5959699	0.1679117	0.0035059	2.7749288	0.1067863	0.0672	0.00552	0.5527706	0.0002263	0.2499035	
9/23/04 21:00	21.5	21.7	21.3	99.545	99.545	0	0	27.9	0	0	2.450081	2.5748990	2.5959699	2.5332049	0.1571176	0.0001410	2.5747579	0.115352	0.0670	0.5871046	0.0002396	0.00027	0.0003506	
9/24/04 00:00	21.1	21.7	20.6	99.67	99.67	0	0	15.3	0	0	2.451064	2.5100123	2.5959699	2.4265523	0.1536525	2.03272E-05	2.5099913	0.1181986	0.0670	0.5981819	0.0002440	0.0002440	0.0001975	
9/24/04 03:00	20.7	21.3	20.6	100	100	0	0	15.6	0	0	2.452048	2.448590	2.4870053	2.4265523	0.1502523	0	2.4465590	0.1210192	0.0670	0	0.6089960	0.0002483	0.0001717	

Date /Time	TMP (°C)	TM Pmax (°C)	TM Pmin (°C)	RH (%)	RH (%)	St. solar radiation MJ/m ² /3hr	W N D Wind Dir (D eg)	Rai fall (mm)	Win d speed, km/hr	U2, Wind speed, m/sec	Lam da (late heat) MJ/kg	e*, vapor pressure, kPa	e*max, kPa	e*min, kPa	Delta, Gradi ent, kPa/°C	Dbar, kPa	e'd, dew point pressure, kPa	Epsilo n, net emmiv ity	Gam ma, Psych rometr ic consta nt	Sh, net short wave radiation, MJ/m ² /3hr	Ln, Long wave radiation, MJ/m ² /3hr	Rn, net radiation, MJ/m ² /hr	Rn, net radiation, mm/3 hr	Ep, net evapo ration, mm/3 hr
9/24 /04	21.4	22.	21.	0.992	99.	55.8	16	0.2	0	0	2.45	2.561	2.725	2.487	0.156	0.000	2.561	0.115	0.067	0.02	0.589	0.61	0.000	0.000
6:00	8333	5		8333	283	833	8.9	5			0.277	8057	5876	0053	4194	1867	6189	9291		1626	3586	0985	2493	4173
9:00	26.0	29.	22.	0.775	77.	521.	20	0	0.8	53.3	2.43	3.374	4.122	2.792	0.198	0.007	3.366	0.083	0.067	0.20	0.449	0.65	0.000	0.244
9:00	6666	5	9	8333	583	55	6.7		33	3333	9456	8854	4897	9444	7509	9687	1101		1839	4196	1259	2669	2687	69
9:00	67	32	29.	0.585	58.	811.	13	0	1.6	106.	2.42	4.471	4.754	4.028	0.254	0.018	4.453	0.044	0.067	0.31	0.256	0.57	0.000	0.927
12:0	1666	67	1	6666	566	75	5.4			6666	8005	3221	7753	8844	1449	1968	1253	5659		4147	9975	1144	2352	0620
12:0	67	32	29.	0.561	56.	355.	12	0	0	0	2.42	4.626	4.863	4.122	0.261	0.019	4.606	0.039	0.067	0.13	0.229	0.36	0.000	0.016
9/24 /04	31.5	32.	29.	0.561	56.	883	16	0	0	0	6589	4400	3111	8854	7891	7247	7153	5143		7726	6700	7396	1514	9991
15:0	1666	4	5		1	3	5				15	47	98	69	64	02	45	58		85	49	9	05	
9/24 /04	24.7	27.	23.	0.908	90.	4.9	70.	0	0	0	2.44	3.111	3.607	2.860	0.185	0.002	3.108	0.083	0.067	0.00	0.494	0.49	0.000	0.003
18:0	6666	2	3	1666	816	205	3				2683	6099	3883	8211	3530	9699	6399	1613		1896	6319	6528	2032	4991
18:0	67	7	7	67	7	11	03				3	11	03	3	23	86	25	03		3	4	24	72	2
9/24 /04	22.9	23.	22.	0.995	99.	0	70.	0	0	0	2.44	2.803	2.860	2.792	0.169	0.000	2.803	0.105	0.067	0	0.547	0.54	0.000	0.000
6:00	6666	3	9	3333	533	0	3				6775	7783	8211	4897	2480	1319	6464	5826		0	6487	7648	2238	3208
6:00	67	7	7	33	3	88	3				7	88	3	66	58	11	77	99		0	7	7	25	03
9/25 /04	22.3	22.	22.	1	100	0	0	0	0	0	2.44	2.692	2.725	2.660	0.163	0	2.692	0.110	0.067	0	0.566	0.56	0.000	0.000
6:00	6666	5	1			6645	0				8349	5876	5876	0893	3766	0	6645	2692		0	8248	6824	2315	1641
9/25 /04	22.3	22.	22.	1	100	0	70.	0	0	0	2.44	2.703	2.725	2.660	0.163	0	2.703	0.109	0.067	0	0.564	0.56	0.000	0.000
3:00	6666	5	1			6001	3				8192	5876	5876	0893	9559	0	6001	8032		0	9388	4938	2307	1638
3:00	67	7	7	33	3	02	07				3	02	07	35	41	02	02	1		0	53	85	58	15
9/25 /04	23	26	21.	0.984	98.	118.	11	0	0	0	2.44	2.809	3.361	2.533	0.169	0.000	2.808	0.105	0.067	0.04	0.546	0.59	0.000	0.000
6:00	6666	3	3	3333	433	385	7.4				6697	4376	4398	2049	5462	4617	9758	3600		5911	7396	2650	2422	7344
9/25 /04	30.4	32.	27.	0.700	70.	649.	14	0	0.8	53.3	2.42	4.349	4.863	3.607	0.248	0.012	4.337	0.048	0.067	0.25	0.277	0.52	0.000	0.334
9:00	3333	4	2	8333	083	016	6.9				9146	3111	3111	3883	1240	6707	0023	4434		1169	5856	8755	2176	6123
9:00	33	33	33	33	3	7	5				9	26	98	03	39	55	71	08		45	86	14	71	22
9/25 /04	33.6	34.	32.	0.504	50.	854.	16	0	1.6	106.	2.42	5.216	5.469	4.973	0.290	0.025	5.190	0.021	0.067	0.33	0.125	0.45	0.000	1.189
6:00	6666	5	8	6666	466	883	1.9				1552	4727	1459	9919	5465	8641	6085	0393		0839	7477	6587	1885	1272
12:0	67	7	7	67	7	3	5				35	46	03	93	63	72	75	75		85	99	65	52	55
9/25 /04	33.2	34.	30.	0.514	51.	383.	22	0	0.26	17.7	2.42	5.096	5.469	4.441	0.284	0.024	5.072	0.024	0.067	0.14	0.146	0.29	0.000	0.203
6:00	6666	5	8	6666	466	35	6.4				2536	3577	1459	6910	7314	0502	3074	6950		8356	7973	5153	1218	2853
15:0	33	33	33	67	7	7	2				1	75	03	99	58	98	77	26		45	12	76	37	98
9/25 /04	25.8	28.	24.	0.862	86.	2.93	24	0	0	0	2.43	3.331	3.936	3.056	0.196	0.004	3.326	0.084	0.067	0.00	0.456	0.45	0.000	0.005
6:00	6666	7	4	5	25	333	1.9				9968	7486	7535	3126	7354	8077	9409	6413		1135	3755	7510	1875	3035
18:0	67	7	7	67	7	3	2				15	59	03	53	37	33	26	46		2	61	76	07	31
9/25 /04	23.7	24.	22.	0.942	94.	0	24	0	0	0	2.44	2.933	3.056	2.792	0.176	0.001	2.931	0.100	0.067	0	0.525	0.52	0.000	0.002
6:00	6666	4	9	5	25	91	1.9				5004	5470	3126	4897	0652	6815	8655	2823		0	4450	5445	2149	1347
21:0	67	7	7	67	7	53	66				95	53	53	66	7	31	6	22		0	19	02	06	71

Date /Time	TMP (°C)	TM Pmax (°C)	TM Pmin (°C)	RH (%)	RH (%)	St. solar radiation MJ/m ² /3hr	W N D Wind Dir (D eg)	Rai fall (mm)	Win speed, km/hr	U2, Wind speed, m/sec	Lam da (late heat) MJ/kg	e ^s , vapor pressure, kPa	e ^m ax, kPa	e ^r min, kPa	Delta, Gradi ent, kPa/°C	Dbar, kPa	e ^d , dew point pressure, kPa	Epsilo n, net emmiv sivity	Gam ma, Psychrometric constant	Sh, net wave radiation, MJ/m ² /3hr	Ln, Long wave radiation, MJ/m ² /3hr	Rn, net radiation, MJ/m ² /hr	Rn, net radiation, mm/3 hr	Ep, net evapo ration, mm/3 hr
9/26 /04 0:00	21.7	22	21	0.969	96	0	24	0	0	0	2.44	2.606	2.725	2.533	0.158	0.000	2.605	0.114	0.067	0	0.581	0.58	0.000	0.001
9/26 /04 0:00	666	5	3	5	95	0	19	0	0	0	9608	5678	5876	2049	8042	8019	7598	0068	0	12	1818	2375	1962	
9/26 /04 3:00	21.3	21	21	0.988	98	0	33	0	0	0	2.45	2.546	2.595	2.487	0.155	0.000	2.545	0.116	0.067	0	0.592	0.59	0.000	0.000
9/26 /04 3:00	833	7	7	333	833	0	23	0	0	0	0513	1705	9699	0053	5949	2965	8740	6188	0	08	0605	2060	5560	
9/26 /04 6:00	22.9	26	21	0.898	89	0	23	0	0.8	53.3	2.44	2.803	3.361	2.487	0.169	0.002	2.800	0.105	0.067	0.05	0.548	0.59	0.000	0.107
9/26 /04 6:00	666	6	2	5	95	0	29	0	0	33	675	7783	4398	0053	2480	9827	7956	7019	0	25	2670	2445	5200	
9/26 /04 9:00	29.7	31	27	0.639	63	0	694	0	1.6	106	2.43	4.170	4.648	3.607	0.239	0.014	4.155	0.054	0.067	0.26	0.309	0.57	0.000	0.794
9/26 /04 9:00	338	34	33	5	50	0	353	0	0	666	0878	5971	3496	3883	2174	8809	7162	6019	0	71	8486	2379	9392	
9/26 /04 12:0	33.8	35	31	0.500	50	0	837	0	1.6	106	2.42	5.270	5.469	5.086	0.293	0.026	5.243	0.019	0.067	0.32	0.44	0.44	0.000	1.203
9/26 /04 12:0	333	5	2	5	05	0	21	0	0	666	1119	0967	1459	8531	1364	3636	7331	4112	0	64	0310	1818	9992	
9/26 /04 15:0	33	3	3	67	7	0	0	0	0	67	5	33	03	41	81	08	25	15	0	31	0.44	0.44	0.000	9
9/26 /04 15:0	33	3	3	67	7	0	0	0	0	67	5	33	03	41	81	08	25	15	0	31	0.44	0.44	0.000	9
9/26 /04 18:0	33.4	35	31	0.520	52	0	348	0	0.26	17.7	2.42	5.153	5.716	4.648	0.287	0.024	5.128	0.022	0.067	0.13	0.136	0.27	0.000	0.208
9/26 /04 18:0	333	3	6	1666	016	0	033	0	6666	7777	2063	7099	5849	3496	5104	8672	8427	9427	0	98	7372	1426	6392	
9/26 /04 18:0	33	3	3	67	7	0	0	0	0	67	5	33	03	41	81	08	25	15	0	31	0.44	0.44	0.000	9
9/26 /04 18:0	33	3	3	67	7	0	0	0	0	67	5	33	03	41	81	08	25	15	0	31	0.44	0.44	0.000	9
9/26 /04 21:0	26.4	29	24	0.868	86	0	5.88	0	0	0	2.43	3.451	4.028	3.130	0.202	0.004	3.447	0.080	0.067	0.00	0.435	0.43	0.000	0.005
9/26 /04 21:0	5	1	8	5	85	0	333	0	0	0	8551	9013	8844	2352	9039	7071	1942	0673	0	9	1880	7464	1793	0648
9/26 /04 21:0	33	3	3	67	7	0	0	0	0	67	5	33	03	41	81	08	25	15	0	31	0.44	0.44	0.000	9
9/26 /04 21:0	33	3	3	67	7	0	0	0	0	67	5	33	03	41	81	08	25	15	0	31	0.44	0.44	0.000	9
9/26 /04 24:0	24.4	24	24	0.948	94	0	0	0	0	0	2.44	3.056	3.056	3.056	0.182	0.001	3.054	0.095	0.067	0	0.504	0.50	0.000	0.001
9/26 /04 24:0	4	4	4	8	8	0	16	0	0	0	3391	3126	3126	3126	4767	5892	7233	3112	0	9	0115	4011	2062	9667
9/26 /04 24:0	4	4	4	8	8	0	16	0	0	0	3391	3126	3126	3126	4767	5892	7233	3112	0	9	0115	4011	2062	9667
9/26 /04 24:0	4	4	4	8	8	0	16	0	0	0	3391	3126	3126	3126	4767	5892	7233	3112	0	9	0115	4011	2062	9667
9/26 /04 24:0	4	4	4	8	8	0	16	0	0	0	3391	3126	3126	3126	4767	5892	7233	3112	0	9	0115	4011	2062	9667
9/26 /04 24:0	4	4	4	8	8	0	16	0	0	0	3391	3126	3126	3126	4767	5892	7233	3112	0	9	0115	4011	2062	9667
9/26 /04 24:0	4	4	4	8	8	0	16	0	0	0	3391	3126	3126	3126	4767	5892	7233	3112	0	9	0115	4011	2062	9667
9/26 /04 24:0	4	4	4	8	8	0	16	0	0	0	3391	3126	3126	3126	4767	5892	7233	3112	0	9	0115	4011	2062	9667
9/26 /04 24:0	4	4	4	8	8	0	16	0	0	0	3391	3126	3126	3126	4767	5892	7233	3112	0	9	0115	4011	2062	9667
9/26 /04 24:0	4	4	4	8	8	0	16	0	0	0	3391	3126	3126	3126	4767	5892	7233	3112	0	9	0115	4011	2062	9667
9/26 /04 24:0	4	4	4	8	8	0	16	0	0	0	3391	3126	3126	3126	4767	5892	7233	3112	0	9	0115	4011	2062	9667
9/26 /04 24:0	4	4	4	8	8	0	16	0	0	0	3391	3126	3126	3126	4767	5892	7233	3112	0	9	0115	4011	2062	9667
9/26 /04 24:0	4	4	4	8	8	0	16	0	0	0	3391	3126	3126	3126	4767	5892	7233	3112	0	9	0115	4011	2062	9667
9/26 /04 24:0	4	4	4	8	8	0	16	0	0	0	3391	3126	3126	3126	4767	5892	7233	3112	0	9	0115	4011	2062	9667
9/26 /04 24:0	4	4	4	8	8	0	16	0	0	0	3391	3126	3126	3126	4767	5892	7233	3112	0	9	0115	4011	2062	9667
9/26 /04 24:0	4	4	4	8	8	0	16	0	0	0	3391	3126	3126	3126	4767	5892	7233	3112	0	9	0115	4011	2062	9667
9/26 /04 24:0	4	4	4	8	8	0	16	0	0	0	3391	3126	3126	3126	4767	5892	7233	3112	0	9	0115	4011	2062	9667
9/26 /04 24:0	4	4	4	8	8	0	16	0	0	0	3391	3126	3126	3126	4767	5892	7233	3112	0	9	0115	4011	2062	9667
9/26 /04 24:0	4	4	4	8	8	0	16	0	0	0	3391	3126	3126	3126	4767	5892	7233	3112	0	9	0115	4011	2062	9667
9/26 /04 24:0	4	4	4	8	8	0	16	0	0	0	3391	3126	3126	3126	4767	5892	7233	3112	0	9	0115	4011	2062	9667
9/26 /04 24:0	4	4	4	8	8	0	16	0	0	0	3391	3126	3126	3126	4767	5892	7233	3112	0	9	0115	4011	2062	9667
9/26 /04 24:0	4	4	4	8	8	0	16	0	0	0	3391	3126	3126	3126	4767	5892	7233	3112	0	9	0115	4011	2062	9667
9/26 /04 24:0	4	4	4	8	8	0	16	0	0	0	3391	3126	3126	3126	4767	5892	7233	3112	0	9	0115	4011	2062	9667
9/26 /04 24:0	4	4	4	8	8	0	16	0	0	0	3391	3126	3126	3126	4767	5892	7233	3112	0	9	0115	4011	2062	9667
9/26 /04 24:0	4	4	4	8	8	0	16	0	0	0	3391	3126	3126	3126	4767	5892	7233	3112	0	9	0115	4011	2062	9667
9/26 /04 24:0	4	4	4	8	8	0	16	0	0	0	3391	3126	3126	3126	4767	5892	7233	3112	0	9	0115	4011	2062	9667
9/26 /04 24:0	4	4	4	8	8	0	16	0	0	0	3391	3126	3126	3126	4767	5892	7233	3112	0	9	0115	4011	2062	9667
9/26 /04 24:0	4	4	4	8	8	0	16	0	0	0	3391	3126	3126	3126	4767	5892	7233	3112	0	9	0115	4011	2062	9667
9/26 /04 24:0	4	4	4	8	8	0	16	0	0	0	3391	3126	3126	3126	4767	5892	7233	3112	0	9	0115	4011	2062	9667
9/26 /04 24:0	4	4	4	8	8	0	16	0	0	0	3391	3126	3126	3126	4767	5892	7233	3112	0	9	0115	4011	2062	9667
9/26 /04 24:0	4	4	4	8	8	0	16	0	0	0	3391	3126	3126	3126	4767	5892	7233	3112	0	9	0115	4011	2062	9667
9/26 /04 24:0	4	4	4	8	8	0	16	0	0	0	3391	3126	312											

Date /Time	TMP (°C)	TM Pmax (°C)	TM Pmin (°C)	RH (%)	RH (%)	solar radiation MJ/m ² /hr	St. solar radiation MJ/m ² /3hr	Wind speed m/sec	Wind speed km/hr	Rainfall (mm)	W. N. Wind Dir (Deg)	W. N. Wind Dir (Deg)	Lambda (late heat) MJ/kg	e* vapor pressure kPa	e*max kPa	e*min kPa	Delta, Gradi ent, kPa/C	Dbar, kPa	e'd, dew point pressure, kPa	Epsilon, net emmissivity	Gamma, Psychrometric constant	Sh, net wave radiation, MJ/m ² /3hr	Ln, Long wave radiation, MJ/m ² /3hr	Rn, net radiation, MJ/m ² /hr	Rn, net radiation, mm/3hr	Ep, net evaporation, mm/3hr
9/27/04 21:00	21.5 6666 67	22.1 1 3	21.3 3333 33	99.8333	99.8333	0	0	0	0	0	83	83	2.450081	2.574899047	2.660089335	2.533204981	0.157117679	4.32775E-05	2.57485577	0.115351	0.067	0	0.587082909	0.587082909	0.000239618	0.000224027
9/28/04 00:00	21.2 6666 67	21.7 7	21.1	100	100	0	0	0	0	0	83	83	2.450789	2.5280349	2.5959699	2.4870053	0.15461624	0	2.5280349	0.117402865	0.067	0	0.595097116	0.595097116	0.000242819	0.000169409
9/28/04 3:00	20.8 5	21.7	20.2	100	100	0	0	0	0	0	83	83	2.451773	2.4641830	2.5959699	2.3673876	0.1511979	0	2.4641830	0.1202319	0.067	0	0.605995348	0.605995348	0.000247117	0.000171271
9/28/04 6:00	22.0 5	24.8	20.6	98.6666	98.6666	110.853	0.049853	0	0	0	15	8.8	2.448939	2.6519995	3.1302352	2.4265523	0.1612196	0.0005093	2.6519995	0.1120324	0.067	0.042873	0.573942024	0.6106815	0.000251882	0.000823342
9/28/04 9:00	29.4 5	30.8	26.8	70.8166	70.8166	750.943	0.337943	106.6666	1.6	0	11	7	2.431468	4.1110319	4.4418910	3.5237195	0.2362430	0.0116228	4.0994091	0.0565420	0.067	0.290630	0.3198149	0.610445	0.000251065	0.000096511
9/28/04 12:00	33.0 1666 67	34.1	31.6	49.8333	49.8333	520.566	0.234255	106.6666	1.6	0	17	3	2.423047	5.0348521	5.3489488	4.6483496	0.2817462	0.0253014	5.0095506	0.0266516	0.067	0.201459	0.157980636	0.359439	0.000148342	0.000643021
9/28/04 15:00	32.2 5	34.5	29.5	53.6666	53.6666	328.433	0.147795	53.3333	0.8	0	16	3	2.424975	4.8087773	5.4691459	4.1228854	0.2707286	0.0223174	4.7864599	0.0337082	0.067	0.127103	0.197686672	0.324790	0.000133936	0.000505019
9/28/04 18:00	24.8 3333 33	27.2	23.7	86.1666	86.1666	1.96666	0.000885	2.442368	0	0	26	4.4	2.445	3.1364652	3.6073883	2.9306073	0.1866435	0.0045384	3.1319267	0.0922384	0.067	0.000761	0.49060972	0.491370	0.000201186	0.000237719
9/28/04 21:00	23.1 6666 67	23.3	22.9	96.0333	96.0333	0	0	0	0	0	28	9.7	2.446303	2.8378836	2.8608211	2.7924897	0.1710438	0.0011212	2.8367623	0.1042023	0.067	0	0.54195026	0.54195026	0.000221538	0.000511069
9/29/04 00:00	22.4 3333 33	22.5	22.1	99.2333	99.2333	0	0	0	0	0	31	5	2.448034	2.7145744	2.7255876	2.6600893	0.1645369	0.0002064	2.7143679	0.1093452	0.067	0	0.563090406	0.563090406	0.000230017	0.000420617
9/29/04 3:00	22.0 33	22.1	21.7	99.8333	99.8333	0	0	0	0	0	18	2.3	2.448979	2.6493076	2.6600893	2.5959699	0.1610767	0.0001095	2.6491981	0.1121309	0.067	0	0.574317194	0.574317194	0.000234513	0.000304473
9/29/04 6:00	23.4	26.8	21.3	94.1666	94.1666	111.766	0.050295	177.7777	0.26	0	16	3	2.445752	2.8781302	3.5237195	2.5332049	0.1731591	0.0015697	2.8765605	0.1025540	0.067	0.043253	0.535059315	0.578313	0.000236456	0.000894605
9/29/04 9:00	29.6 8333 33	31.2	28.1	63.1666	63.1666	654.9705	0.294705	195.5555	2.93	0	15	8.9	2.430917	4.1666029	4.5439995	3.7799303	0.2390181	0.0150593	4.1515435	0.0547452	0.067	0.253446	0.31040541	0.564054	0.000232034	0.000146448
9/29/04 12:00	32.7	34.1	30.8	52.1666	52.1666	763.716	0.343673	142.2222	2.13	0	17	2.0	2.423795	4.9461187	5.3489488	4.4416910	0.2774304	0.0232935	4.9228252	0.0293758	0.067	0.295558	0.173409412	0.468967	0.000193485	0.000472444
9/29/04 15:00	28.9 3333 33	34.5	23.3	66.8	66.8	335.283	0.150878	106.6666	1.6	3.3	16	9	2.432688	3.9902710	5.4691459	2.8608211	0.2301943	0.0138277	3.9764433	0.0608257	0.067	0.129754	0.341701025	0.471455	0.000193868	0.000446353

Date /Time	TMP (°C)	TM Pmax (°C)	TM Pmin (°C)	RH	RH (%)	RH	solar radiation watt/m ²	solar radiation MJ/m ² /3hr	WN Dir (Deg)	Rainfall (mm)	Wind speed (km/hr)	U2, Wind speed (m/sec)	Lambda (late heat) MJ/kg	e*, vapor pressure, kPa	e*max, kPa	e*min, kPa	Delta, Gradi ent, kPa/°C	Dbar, kPa	e'd, dew point vapor pressure, kPa	Epsilon, net emissivity	Gamm, Psychrometric constant	Sh, net short wave radiation, MJ/m ² /3hr	Ln, Long wave radiation, MJ/m ² /3hr	Rn, net radiation, MJ/m ² /hr	Rn, net radiation, mm/3 hr	Ep, net evaporation, mm/3 hr
9/29/04 18:00	23.0	24	22.5	0.983	98.333	333	10.7833	0.004853	26.02	0	0.267	17.777	2.4465	2.81277	2.98377	2.72507	0.1696955	0.00018	2.8118094	0.1052416	0.06715	0.54624	0.5577	0.0002249	0.00069	
9/29/04 21:00	22.0	22.5	21.7	1	100		0	0	0.26	0	0	0	2.448979	2.6493076	2.7255876	2.5959699	0.1610767	0	2.6493076	0.1121282	0.067	0.5742930	0.5742930	0.0002345	0.0001656	
9/30/04 0:00	22.1	22.5	21.7	1	100		0	0	0	0	0	2.448821	2.6608893	2.7255876	2.5959699	0.1610767	0	2.6608893	0.1116630	0.067	0.5724373	0.5724373	0.0002337	0.0001652		
9/30/04 3:00	21.8	22.5	21.7	0.998	99.333	333	0	0	1.867	7.8	1.867	124.444	2.449412	2.6198547	2.7255876	2.4870053	0.1595114	4.34383E-05	2.6198112	0.1133963	0.067	0.5793671	0.5793671	0.0002365	0.0009265	
9/30/04 6:00	20.9	21	20.6	1	100		10.7666	0.004845	12.17	11.17	1.33888	88.888	2.451576	2.4768394	2.4260053	2.426523	0.1518764	0	2.4768394	0.1196683	0.067	0.6038384	0.6038384	0.0002480	0.0001720	
9/30/04 9:00	20.6	20.6	20.6	0.999	99.67	1666	54.97	0.024705	20.13	12.7	1.867	124.444	2.452363	2.4265523	2.4265523	2.4265523	0.1491777	2.02213E-05	2.4265520	0.1219173	0.067	0.6124030	0.633649	0.0002583	0.000309	
9/30/04 12:00	21.1	21.7	20.6	0.995	99.833	583	143.133	0.06441	18.02	7.36	1.66666	106.666	2.451064	2.5100123	2.5959699	2.4265523	0.1536525	0.0001046	2.5099076	0.1182023	0.067	0.5982007	0.653593	0.0002666	0.0002185	
9/30/04 15:00	22.1	22.5	21.7	0.961	96.15	1666	165.666	0.07455	22.61	0.25	0.53333	35.5555	2.448821	2.6608893	2.7255876	2.5959699	0.1610767	0.0010244	2.6590649	0.1117070	0.067	0.5726627	0.636775	0.0002600	0.0001604	
9/30/04 18:00	20.7	21.7	20.2	0.990	99.666	666	4.97	0.002205	35.58	0	0	0	2.452087	2.4440503	2.5959699	2.3673876	0.1501176	0.0002316	2.4438186	0.1211419	0.067	0.6094751	0.611371	0.0002493	0.0004841	

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ABSTRACT

A GIS STUDY OF LANDSLIDES IN THE LOWER LOS AMIGOS FORELAND OF PERU

by Suresh P. Khanal, MS, 2006
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A GIS study of landslides in the lower Los Amigos sub-basin in Peru, where human influence on drainage is nearly non-existent, was performed to determine environmental variables controlling landslides. GIS layers consisted of slope, landslides (381 digitized), Soils, and elevation.

I applied Ripley's K-function to estimate spatial extent of correlation between the landslides. The MIKE-SHE hydrologic model was used to determine the unsaturated soil-water pressure in the soil profile. Spatial regressions were performed between landslide counts in a 1X1 km grid and environmental variables: slope, aspect, distance of landslide from nearest river, and soil-water pressure. My conclusions are that landslides were spatially correlated at about 2km lengths, and variations of pore-water pressure in the soils significantly controlled landslide occurrence. Landslides along river meander paths may be an important factor that controls the evolution of foreland basins.